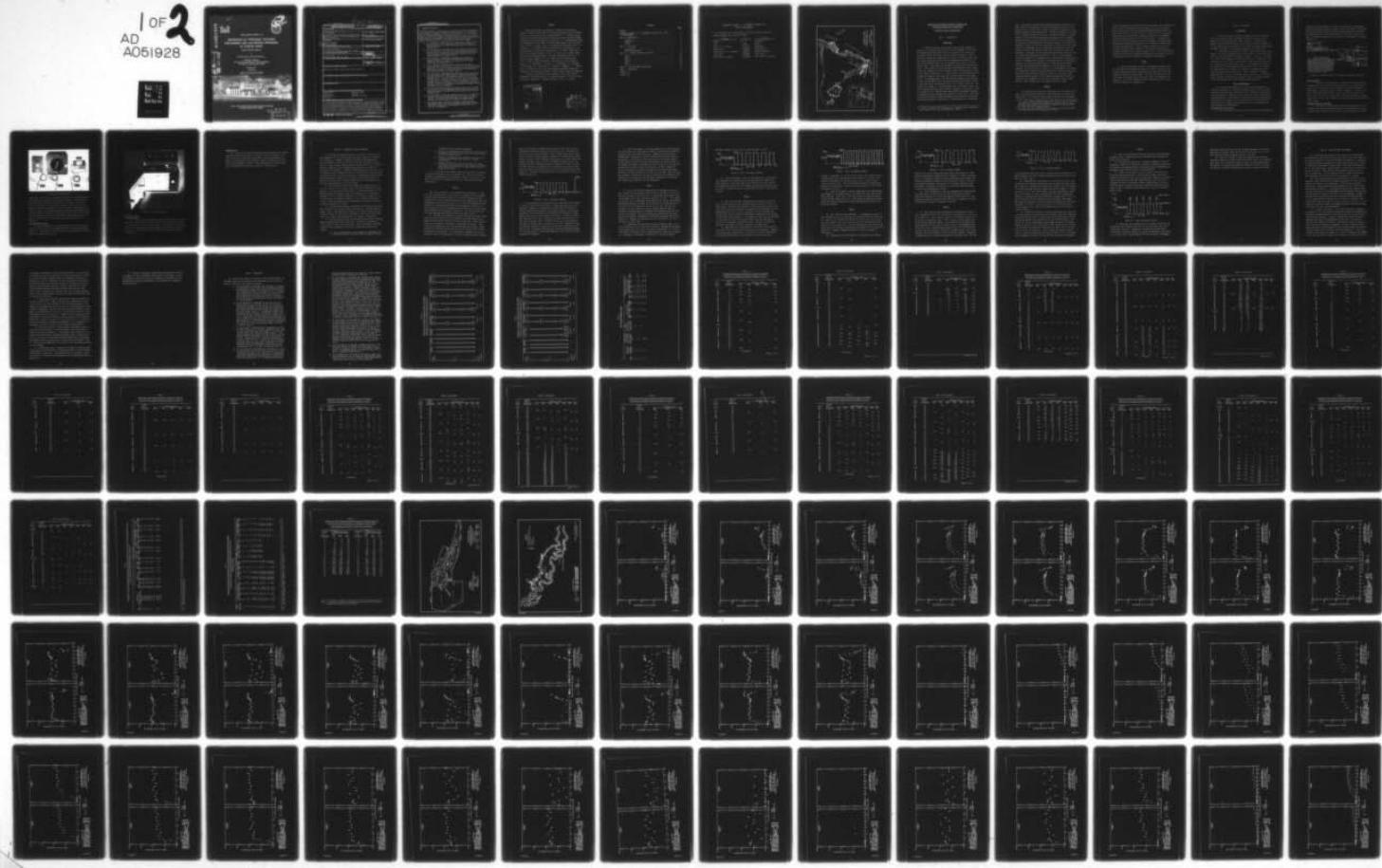


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DISPERSION OF PROPOSED EFFLUENT DISCHARGES AND SALTWATER INTRUSION IN COOPER RIVER

Hydraulic Model Investigation

by

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November 1977

Final Report

Approved For Public Release; Distribution Unlimited



Prepared for State of South Carolina Water Resources Commission
Columbia, South Carolina 29240

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20. ABSTRACT (Continued).

to critical locations, it was desired to determine the maximum concentrations of the effluents in Cooper River and Back River Reservoir. It was desired to know the rates of increases of effluent concentrations at critical locations should the freshwater discharge from Pinopolis reduce to zero. It was also desired to know if there would be saltwater intrusion into Back River Reservoir during operation of the Schedule C and Schedule E hydrographs. Based on the results of the model tests, the following conclusions were reached:

- a. For the Schedule C hydrograph and continuous dye release at Cooper River mile 37 (sta 37C), measurable concentrations reached the Back River Reservoir (sta BR1) within four tidal cycles after the release (Test 1).
- b. For the Schedule C hydrograph and the dye released at Cooper River mile 37 (sta 37C) at the rate of 30 cfs during each ebb phase of the tide and 0 cfs during each flood phase, measurable dye concentrations reached the Back River Reservoir (sta BR1) within four tidal cycles after the release (Test 2).
- c. For the Schedule C hydrograph and continuous dye release at Cooper River mile 33 (sta 33C), measurable dye concentrations reached the Back River Reservoir (sta BR1) within five tidal cycles after the release (Test 3).
- d. For the Schedule C hydrograph and continuous dye released at Cooper River mile 33 (sta 33C) at the rate of 30 cfs during each ebb phase of the tide and 0 cfs during each flood phase, measurable dye concentrations reached the Back River Reservoir (sta BR1) within five tidal cycles after the release (Test 4).
- e. For the Schedule C hydrograph and continuous dye release at Cooper River mile 30 (sta 30C), measurable dye concentrations reached the Back River Reservoir (sta BR1) within 25 tidal cycles after the release (Test 5). During the period of zero flow (cycles 56-68), dye moved into the Back River Reservoir with maximum concentrations of about 0.09 to 0.13 percent of initial concentration. After resuming the Schedule C hydrograph, the dye was flushed from sta BR1 with about 0.02 to 0.05 percent still remaining at sta BR2, BR3, and BR4 when the test was terminated.
- f. For the Schedule E hydrograph and continuous dye release at Cooper River mile 37 (sta 37C), measurable dye concentrations reached the Back River Reservoir (sta BR1) within three tidal cycles after the release (Test 6).
- g. For the Schedule C hydrograph, maximum salinities in the Back River Reservoir varied from 15 ppm total salt at sta BR1 to 46 ppm at sta BR2. For the Schedule E hydrograph, the maximum salinities varied from 10 ppm at sta BR1 to 15 ppm at sta BR2 and BR3.
- h. The upstream limit of intrusion (100 ppm) of ocean salt water (high-water slack, bottom) was approximately Cooper River mile 43 (sta 43C) for Schedule C and approximately Cooper River mile 41 (sta 41C) for Schedule E.

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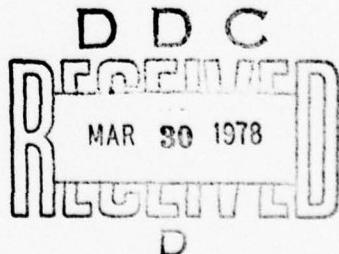
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PREFACE

This report presents the results of dispersion and salinity studies requested by the State of South Carolina Water Resources Commission for the Cooper River Water Users Association. The study was performed in the existing Charleston Harbor model during the period August to November 1975 by the Hydraulics Laboratory, U. S. Army Engineer Waterways Experiment Station (WES), Vicksburg, Mississippi, under the direction of Mr. H. B. Simmons, Chief of the Hydraulics Laboratory; Mr. F. A. Herrmann, Jr., Assistant Chief of the Hydraulics Laboratory; Mr. R. A. Sager, Chief of the Estuaries Division; Mr. W. H. Bobb, former Chief of the Interior Channel Branch; and Mr. R. A. Boland, Jr., present Chief of the Interior Channel Branch. The study was conducted by Mr. M. J. Trawle, Project Manager; Mr. H. A. Benson, Project Engineer; and Mr. H. R. Smith, Senior Technician. Technical help was provided by Messrs. C. R. Herrington, J. Cessna, J. T. Cartwright, T. W. McGough, D. M. Stewart, E. S. Jefferson, M. S. Taylor, D. Marzette, J. S. Ashley, and H. P. Townsley. This report was prepared by Messrs. Benson and Boland with the assistance of Messrs. Smith, Trawle, Sager, and Herrmann.

Directors of WES during the performance of this study and the preparation and publication of this report were COL G. H. Hilt, CE, and COL John L. Cannon, CE. Technical Director was Mr. F. R. Brown.

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CONVERSION FACTORS, U. S. CUSTOMARY TO METRIC (SI)

UNITS OF MEASUREMENT

U. S. customary units of measurement used in this report can be converted to metric (SI) units as follows:

| Multiply | By | To Obtain |
|------------------------------|------------|-------------------------|
| inches | 25.4 | millimetres |
| feet | 0.3048 | metres |
| miles (U. S. statute) | 1.609344 | kilometres |
| square feet | 0.09290304 | square metres |
| square miles (U. S. statute) | 2.589988 | square kilometres |
| cubic yards | 0.7645549 | cubic metres |
| cubic feet per second | 0.02831685 | cubic metres per second |

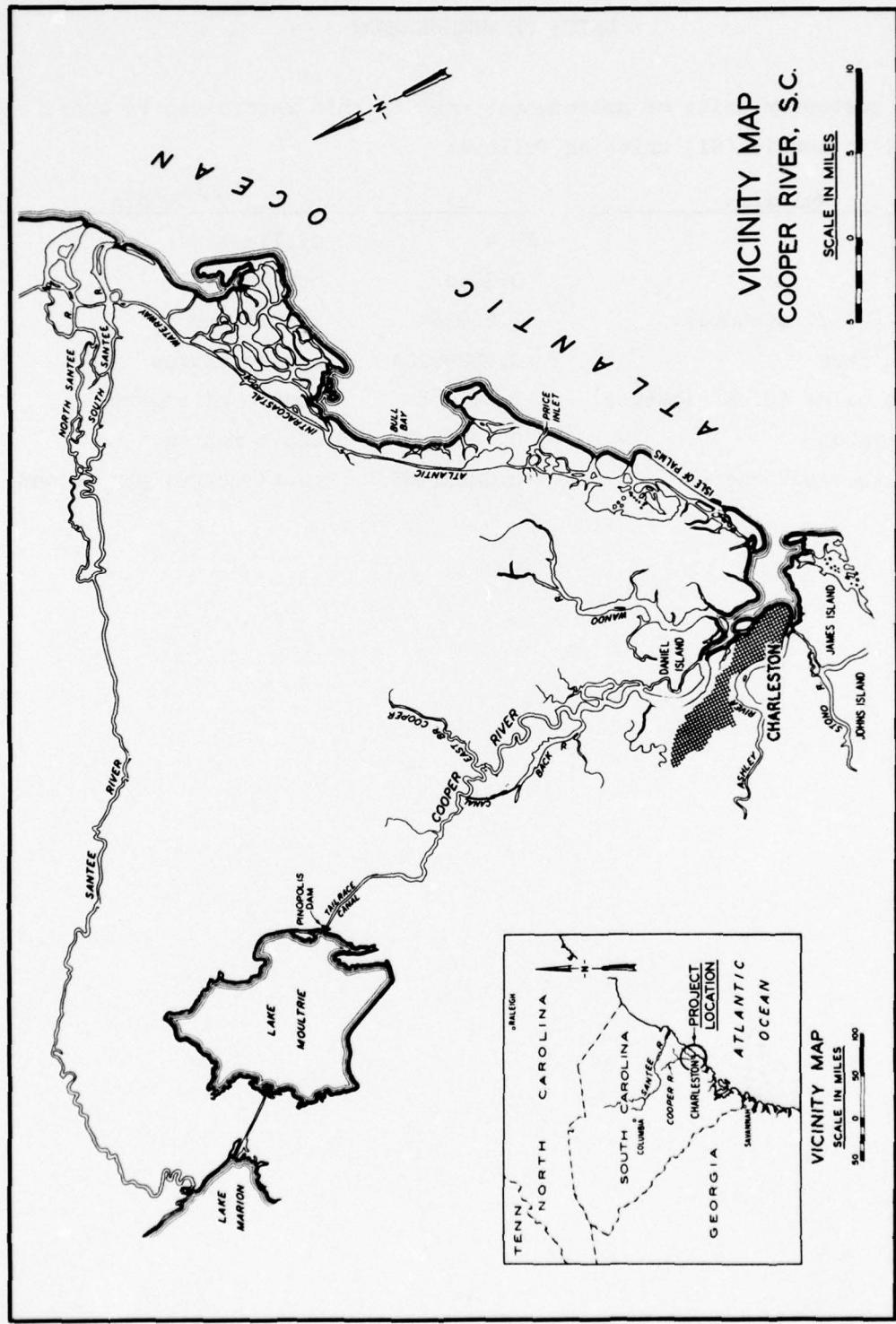


Figure 1. Location map

DISPERSION OF PROPOSED EFFLUENT DISCHARGES AND
SALTWATER INTRUSION IN COOPER RIVER

Hydraulic Model Investigation

PART I: INTRODUCTION

Background

1. Charleston Harbor, an important South Carolina seaport, is located on the Atlantic coast about 110 miles* southwest of the North Carolina-South Carolina State line and is formed by the junction of the Ashley, Wando, and Cooper Rivers as shown in Figure 1. Prior to 1940, the estuary had a drainage area of about 1,400 square miles, and the average freshwater inflow from all tributaries was about 415 cfs (261 cfs from Ashley River, 82 cfs from Wando River, and 72 cfs from Cooper River). The estuary was homogeneous, being almost entirely salt water. Construction of the Santee-Cooper Hydroelectric Project, begun in 1940 and completed in 1942, included a dam in the West Branch of the Cooper River at Pinopolis, S. C., and diversion of the Santee River flow through the Pinopolis power plant into the West Branch of the Cooper River. The drainage area of the Charleston Estuary was thus increased to about 16,000 square miles, and the average annual freshwater inflow of the Cooper River was increased from 72 cfs to about 15,600 cfs. The estuary was changed to a partially mixed type, and density currents became a controlling factor with respect to shoaling in the harbor. Prior to completion of the Santee-Cooper power project, maintenance dredging in Charleston Harbor averaged about 180,000 cu yd per year. Since completion of the project, annual maintenance requirements in the navigation channels steadily increased up to 10,000,000 cu yd at the present

* A table of factors for converting U. S. customary units of measurement to metric (SI) units is presented on page 3.

time. The results of previous studies* indicated that rediversion of a major portion of the Santee River flow from Cooper River back to the Santee River is the best way to obtain a substantial reduction in maintenance dredging in Charleston Harbor. However, continuation of as much flow as possible through Pinopolis was considered desirable to minimize change to the Cooper River and harbor environment and to accommodate downstream needs of Bushy Park Reservoir at mile 43 and the Jefferies Stream Electric Generating Plant just below Pinopolis. The Bushy Park Reservoir, which fills from the Cooper River at mile 43, has been established as a freshwater source for municipal and industrial uses; and salinity intrusion (80 ppm total salt) into the reservoir cannot be tolerated. Discharges from the municipal and industrial areas are into the Cooper River downstream from mile 43. The U. S. Army Engineer District, Charleston, is developing a monitoring system to determine the effect of freshwater flow changes in the Cooper River on the hydraulic, salinity, and shoaling characteristics in Charleston Harbor during both pre- and post-redirection conditions. The optimum inflow at Pinopolis to best satisfy all interests will be determined. The existing Cooper River Federal navigation channel and the portion maintained by the Navy are maintained at project depths of -35 ft mlw.** The Federal navigation channel and the portion maintained by the Navy are scheduled to be deepened to -40 ft mlw in the Cooper River to about mile 23. This condition was in the model during this study.

Purpose

2. The Bushy Park industrial development site is bounded on the west by the Back River Reservoir for fresh water and on the east by Cooper River. The industrial water supply scheme for the development

* U. S. Army Engineer Waterways Experiment Station, CE, "Investigation for Reduction of Maintenance Dredging in Charleston Harbor, South Carolina; Summary Report of Model Investigation," Technical Report No. 2-444, Apr 1957, Vicksburg, Miss.

** In this report, mlw refers to mean low water for the Custom House tide gage located on the Charleston waterfront.

involves withdrawals from the reservoir and discharges into Cooper River. It was desired to determine in what quantity, if any, the effluents would be transported from three proposed discharge points (located between miles 30 and 37 on Cooper River) to the mouth of the freshwater intake canal for the reservoir (located at mile 43) and subsequently through the intake canal into the reservoir proper. In addition to travel times of the effluents to critical locations, it was desired to determine the maximum concentrations of the effluents in Cooper River and Back River Reservoir. It was desired to know the rates of increases of effluent concentrations at critical locations should the freshwater discharge from Pinopolis reduce to zero. It was also desired to know if there would be saltwater intrusion into Back River Reservoir during operation of the Schedule C and Schedule E hydrographs.

Scope

3. The testing program consisted of measuring salinities and dye concentrations throughout the model for various locations of dye release simulating wastewater discharges from Bushy Park and for two different freshwater inflow schemes. The first five tests were conducted with an average weekly flow rate of 3000 cfs (Schedule C) at Pinopolis. Test 6 was conducted with an average weekly flow rate of 3500 cfs (Schedule E) at Pinopolis.

PART II: THE MODEL

Description

4. The Charleston Harbor model reproduced the entire tidal portions of the Ashley, Cooper, and Wando Rivers and a portion of the Atlantic Ocean within the limits shown in Plate 1. The Ashley and Wando Rivers and the East Branch of the Cooper River were reproduced to correct lengths and cross sections but, in order to conserve space, were realigned to conform to the general alignment of the Cooper River.

5. The model was constructed to linear scale ratios, model to prototype, of 1:2,000 horizontally and 1:100 vertically. These scale ratios fixed the following model-to-prototype relations: slope 20:1, velocity 1:10, time 1:200, discharge 1:2,000,000, and volume 1:400,000,000. The salinity scale ratio was 1:1, and the model ocean supply was maintained at a salinity of 30,000 ppm total salts. One prototype tidal cycle of 12 hr and 25 min was reproduced in the model in 3.725 min. The model was approximately 137 ft long, 46 ft wide at the widest point, and covered an area of about 3,600 sq ft. Depths of water in the model range from about 1/2 in. in the marsh areas to about 5 in. in the navigation channel. The model was constructed within a shelter to protect it from the weather and to permit uninterrupted operation.

Model Appurtenances

6. The model was equipped with the necessary appurtenances to reproduce and measure all pertinent phenomena such as tidal elevations, saltwater concentrations, current velocities, freshwater inflows, and dye concentrations. Apparatus used in connection with the reproduction and measurement of these phenomena included an automatic tide generator and recorder, tide gages, current velocity meters, freshwater inflow measuring devices, skimming and measuring weirs, and fluorometers for dye concentration determinations.

Tide generator and recorder

7. The reproduction of tidal action in the model was accomplished

by means of a tide generator, located in the model ocean, which maintained a differential between a pumped inflow of salt water to the model and a gravity return flow to the supply sump as required to reproduce all characteristics of the prototype tides at the ocean control tide gage. A schematic drawing of the operation of this system is presented in Figure 2.

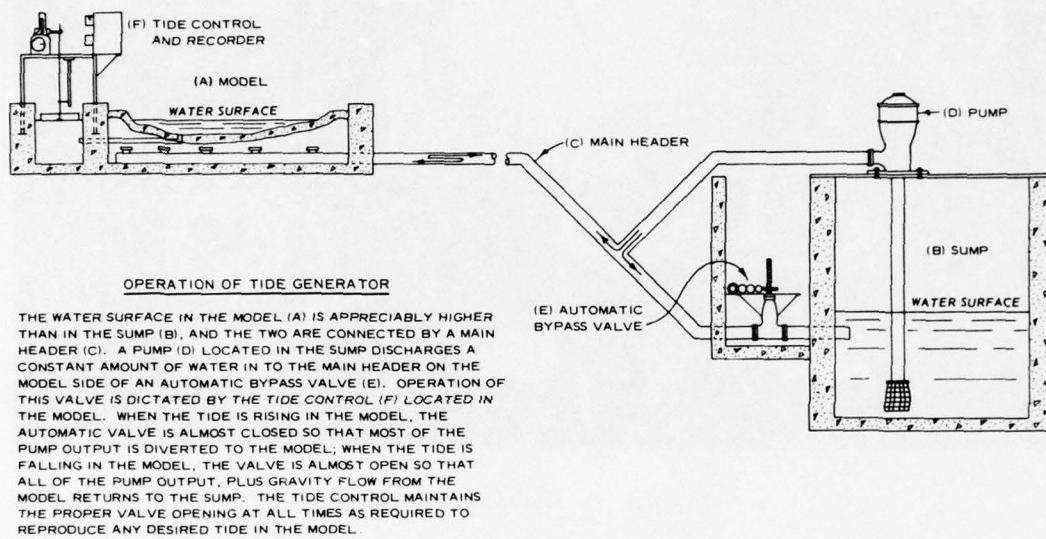


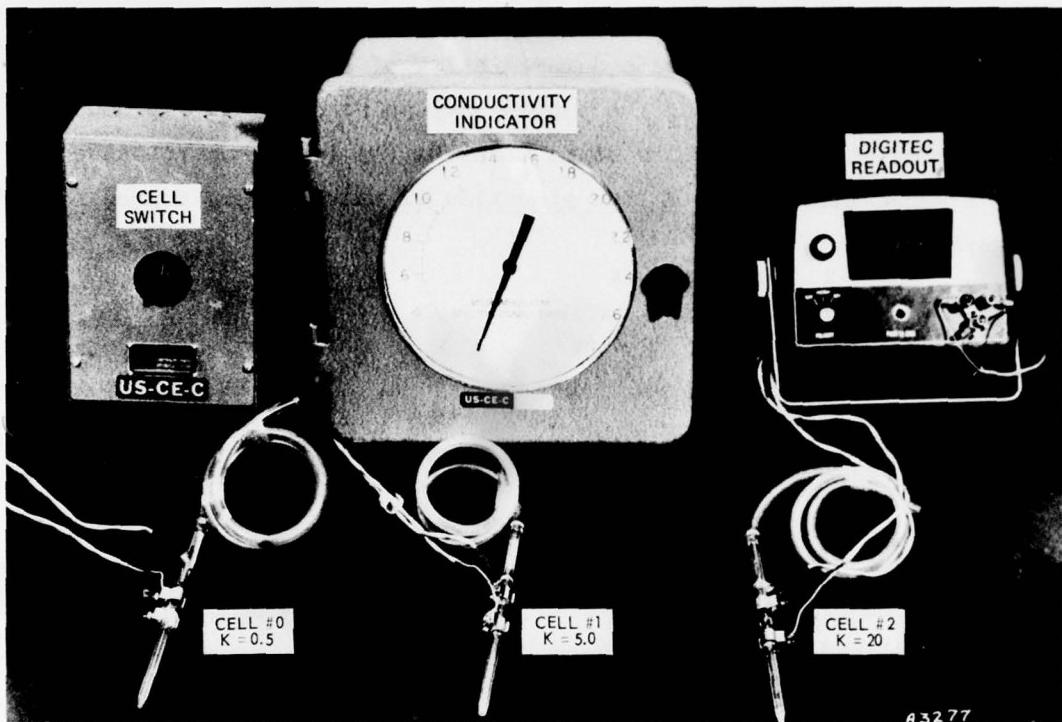
Figure 2. Schematic diagram of a typical tide generating system

Salinity meters

8. All salinity concentrations of samples taken from the model throughout the various tests were determined by use of salinity meters consisting of conductivity cells especially built and calibrated for this purpose. The salinity meter is shown in Figure 3. One cell was used for salinities below about 1.0 ppt; a second cell covered the range from 1.0 to about 5.0 ppt; while a third cell was used for values greater than 5.0 ppt. The accuracy of the salinity meter was ± 2 percent of full range.

Chemical titration equipment

9. This method of determining salinity concentrations was used primarily for periodic calibration checks of the salinity meters, and to ensure that a constant source salinity was maintained in the ocean



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Figure 3. Salinity meter

supply sump. The titration equipment consisted of a graduated burette for measuring the volume of silver nitrate required to precipitate the salt, pipettes for measuring the volume of each sample, sample jars in which to perform the titration, a supply of silver nitrate, and a quantity of potassium chromate for use as an end-point indicator in the titration process. The method consisted of adding a known concentration of silver nitrate solution to a known volume of the model salinity sample; the amount of silver nitrate required to precipitate the salt contained in the sample was then converted to salinity in parts per thousand.

Dye concentration meter

10. Dye concentrations of samples taken from the model throughout the various tests were determined by means of a Turner fluorometer (Figure 4). The accuracy of the fluorometer is about ± 3 percent for the range of concentrations measured.

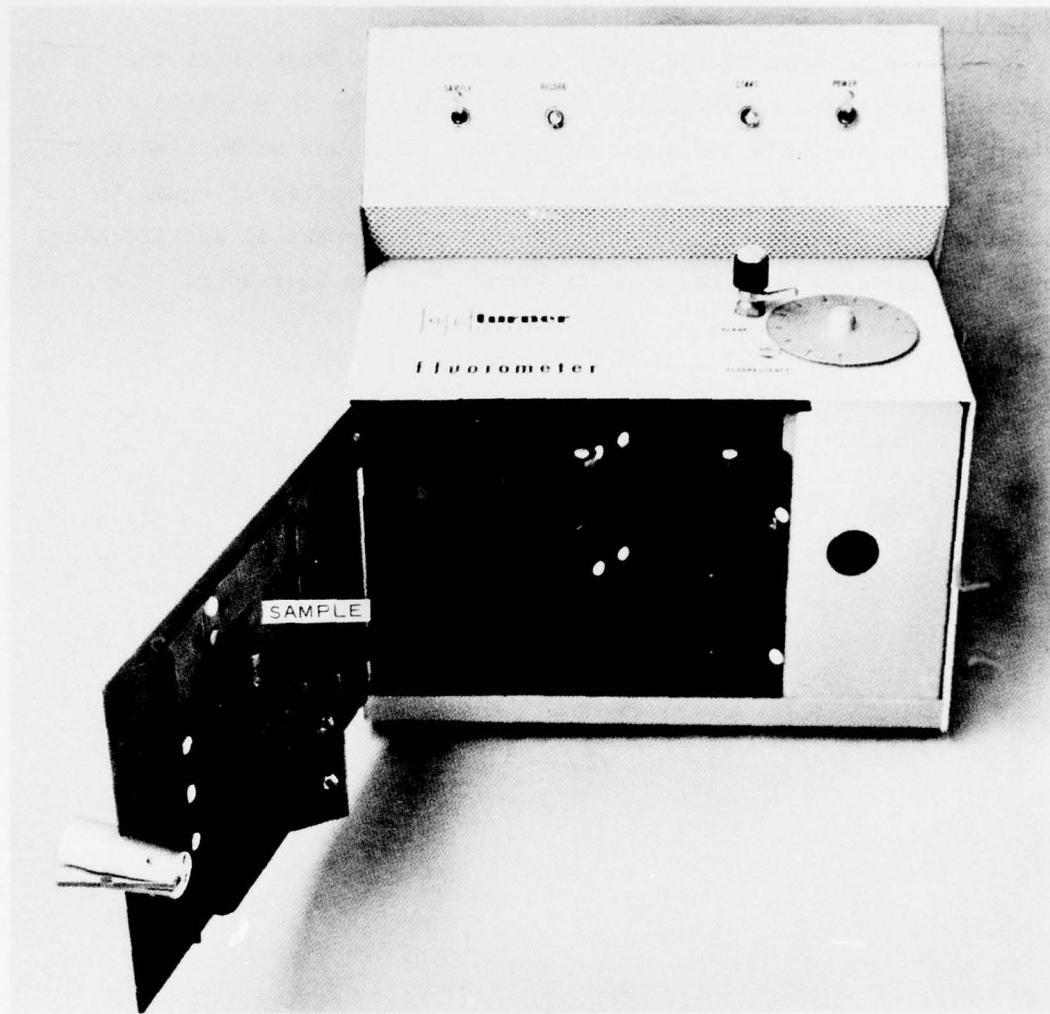


Figure 4. Turner fluorometer

Freshwater inflow
measuring devices

11. All rivers with freshwater inflows were equipped with a constant head tank and either Brooks rotometers or Van Leer weirs for precise measurements of the respective flows. The Cooper River control at Pinopolis was equipped with a quick-opening valve to make it possible to simulate the flow changes dictated by the power-generating schedule being tested.

Skimming weir

12. A portion of the mixed salt water and fresh water that accumulated in the model ocean had to be wasted in order to maintain a constant volume in the model and sump system. This was accomplished by means of a skimming weir that removed a quantity of water equal to the total of the freshwater inflows. Precise measurement of the discharge over the skimming weir was made by means of a Van Leer weir.

PART III: DISPERSION TESTS AND RESULTS

13. The testing program consisted of six tests. The first five were conducted with an average weekly flow rate of 3,000 cfs (Schedule C) at Pinopolis. Schedule C simulated a possible power-generating station operation at Pinopolis with zero flow for 3 days and 5,250-cfs flow for 4 days, giving a weekly average discharge of 3,000 cfs (Table 1). Test 6 was conducted with an average weekly flow rate of 3,500 cfs (Schedule E) at Pinopolis. Schedule E simulated 69 hr of zero flow, 3 hr of 28,500-cfs flow, followed by 4 days of 5,250-cfs flow, giving an average weekly flow rate of 3,500 cfs (Table 2). Transparent overlays of the operating schedules (Figures 5-10) for each test are provided in the pocket on the back cover to readily compare the dye concentration results and the freshwater inflow fluctuations.

14. The Cooper River navigation channel was deepened from 35 ft to 40 ft to mile 23 in the model, since the proposed deepening has been approved. All tests were conducted with a continuous reproduction of an average spring tide having an ocean tide range of 5.4 ft (high-water elevation = 5.8 ft; low-water elevation = 0.4 ft) and a range of 6.0 ft at Custom House (high-water elevation = 6.3 ft; low-water elevation = 0.3 ft). The ocean supply sump was maintained at a constant salinity of 30,000 ppm throughout all tests.

15. Salinity and dye samples were taken in the Cooper River, Back River Reservoir, and entrance canal to Back River at locations shown in Plates 1 and 2. The samples were taken at the times of local high- and low-water slacks at surface and bottom depths at the tidal cycles indicated on the salinity and dye plots for the duration of each test.

16. All dye dispersion data were processed and plotted by computer using a standard WES program, the results of which are presented in Plates 3-115 for Tests 1-6, respectively. The data analysis steps that resulted in the time/percent of initial concentration plots were as follows:

- a. The dye concentration of each sample was determined from Pontacyl Brilliant Pink dye calibration equations for the

fluorometer used in sample measurement.

- b. The dye concentrations were corrected by subtracting the background concentration (dye detected at each location prior to starting a test).
- c. The dye concentrations were divided by the initial concentration to determine the percent of initial concentration.
- d. Graphs were plotted of the log of percent of initial concentration as a function of time, expressed in tidal cycles after initiation of the dye release, for each observation station.

17. To include all dye samples taken, values below 0.01 percent (10 ppb) were plotted on the 0.01 percent line. For all tests, the initial dye concentration was 100,000 ppb. Values of 0.01, 0.10, 1.00, and 10.00 percent are equivalent to 10, 100, 1,000, and 10,000 ppb, respectively.

Test 1

18. Test 1 involved: (a) a continuous dye discharge at a rate of 15 cfs in Cooper River at mile 37 with a companion 15-cfs withdrawal from Back River Reservoir wasted; (b) a 750-cfs withdrawal from the reservoir at the South Carolina Electric and Gas (SCE&G) plant (BR1) and discharged in Cooper River at mile 33; (c) a 185-cfs withdrawal from the reservoir at the Verona plant (BR2) and discharged in Cooper River at mile 29; and (d) a 200-cfs withdrawal from the reservoir in Foster Creek and discharged off the battery at Charleston. The dye injection location and withdrawal and discharge points are shown in Plate 2.

19. The model was operated to salinity stability (69 tidal cycles) using a constant 3,000-cfs flow at Pinopolis and simulating all withdrawals and discharges except the 15-cfs dye discharge. After salinity stability was achieved, the Schedule C hydrograph was started. After 1 week of the hydrograph, the 15-cfs dye discharge was started. About 3 weeks after the dye injection was started, dye stability was achieved throughout the problem area. It was desired to determine the rates of increases of waste concentrations at critical locations should a disaster

reduce the freshwater discharge from Pinopolis to zero until the next dye-salinity plateau was reached in the problem area. Therefore, the flow rate at Pinopolis was reduced to zero 4 weeks after the dye injection was started. Model operation continued for an additional 19 tidal cycles, at which time the salinity concentration at sta BRL (SCE&G) had reached 1,340 ppm. Then, in order to determine flushing time in the problem area with a freshwater release at Pinopolis of 28,500 cfs, the Pinopolis flow rate was changed from 0 to 28,500 cfs (75 tidal cycles after dye release started) and continued for 12 additional tidal cycles (Figure 5). Time-dye concentration plots for each station of Test 1 are shown in Plates 3-19.

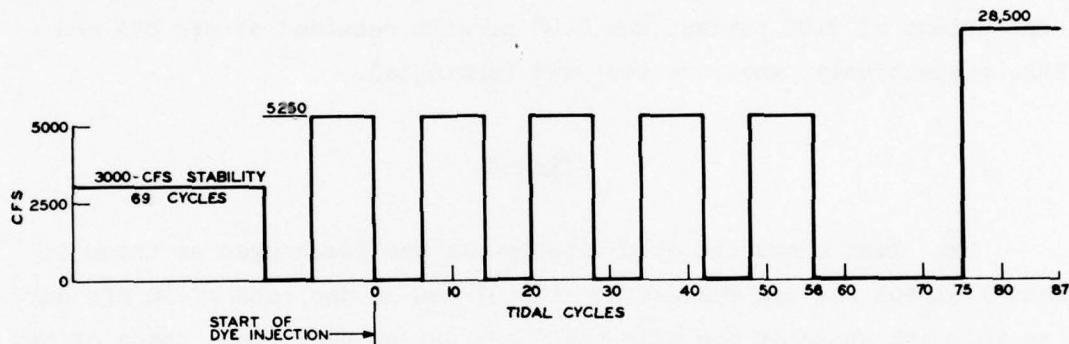


Figure 5. Test 1 discharge schedule

20. Measurable dye concentrations were indicated at the entrance to Back River Canal (sta 43C, Plate 14) within one tidal cycle after injection. Maximum dye concentrations reached about 0.5 percent of initial concentration after dye stability was obtained. A noticeable fluctuation of dye concentrations was caused by the Schedule C hydrograph as the flow went from 3 days of zero flow to 4 days of 5,250-cfs flow and back to zero flow. During the 19 cycles (cycles 56-75) of zero flow following 4 days of 5,250-cfs flow, the dye concentrations increased to slightly above 1.0 percent at sta 43C. Immediately after the flow was increased to 28,500 cfs, the dye was flushed downstream from sta 43C. Measurable concentrations of dye were detected upstream in the Cooper River to sta 50C and downstream to sta 00C during normal operations of Schedule C.

21. Plate 17 and Table 3 show that significant dye concentrations were observed in the intake canal (sta BRC) of the Back River Reservoir within one tidal cycle after injection. Maximum dye concentrations reached about 0.9 percent of initial concentration after dye stability was obtained. After three or four tidal cycles, the dye had reached sta BR1 and BR2 located in the Back River Reservoir (Plates 18 and 19). The maximum concentrations varied from about 0.4 percent of initial concentration at sta BR1 to about 0.6 percent at sta BR2. During the period of sustained zero flow (cycles 56-75), dye concentrations were increased to about 1.0 percent at sta BRC, BR1, and BR2. After the flow was increased to 28,500 cfs, the dye was flushed from sta BRC while concentrations of 0.02 percent and 0.08 percent remained at sta BR1 and BR2, respectively, when the test was terminated.

Test 2

22. Test 2 had the same withdrawals and discharges as those in Test 1 except the dye release at mile 37 was at the rate of 30 cfs during each ebb phase of the tide and 0 cfs during each flood phase of the tide instead of the 15-cfs continuous release as in Test 1. The purpose of this test was to investigate the possibility of the dye being flushed downstream during the ebb phase of the tide and not moving upstream as far as sta 43C if released only during the ebb tide. The model was operated to salinity stability using a constant 3000-cfs flow at Pinopolis and simulating all withdrawals and discharges except for the 30-cfs dye discharge. The dye discharge was started after the first week of the Schedule C hydrograph and continued through 60 tidal cycles (Figure 6). Time-dye concentration plots for each station for Test 2 are shown in Plates 20-36.

23. Measurable dye concentrations were indicated (Plate 31) at sta 43C within two tidal cycles after injection. Maximum dye concentrations reached about 0.5 percent of initial concentration. As in Test 1, a noticeable fluctuation of dye concentrations was caused by the Schedule C hydrograph. Measurable concentrations of dye were detected

upstream in Cooper River to sta 50C and downstream to sta 00C.

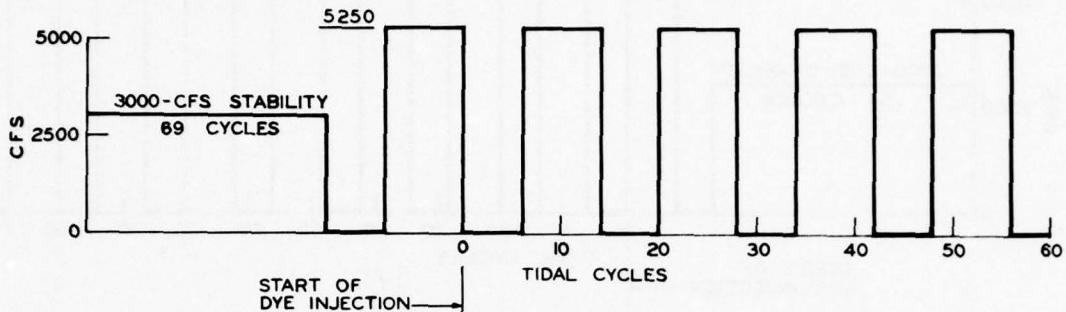


Figure 6. Test 2 discharge schedule

24. Plate 34 and Table 3 show that measurable dye concentrations were observed in the intake canal at sta BRC within one tidal cycle after injection. After five tidal cycles (Plates 35 and 36), the dye had reached sta BR1 and BR2. The maximum concentration observed at BR1 was about 0.5 percent of initial concentration and about 0.3 percent at sta BR2.

Test 3

25. Test 3 had the same withdrawals and discharges as those in Test 1 except that the 15-cfs continuous dye release was at mile 33 in Cooper River. The model was operated to salinity stability using a constant 3000-cfs flow at Pinopolis and simulating all withdrawals and discharges except for the 15-cfs dye discharge. The dye discharge was started after the first week of the Schedule C hydrograph and continued for 100 tidal cycles (Figure 7). The duration of this test was increased to 100 cycles to ensure that stability had really been achieved by 60 cycles, as assumed in the previous tests. Time-dye concentration plots for each station for Test 3 are shown in Plates 37-55.

26. Measurable dye concentrations (0.06 percent) were detected (Plate 48) at sta 43C within two tidal cycles after injection. Maximum dye concentrations reached about 0.2 percent of initial concentration. A noticeable fluctuation of dye concentrations was caused by the

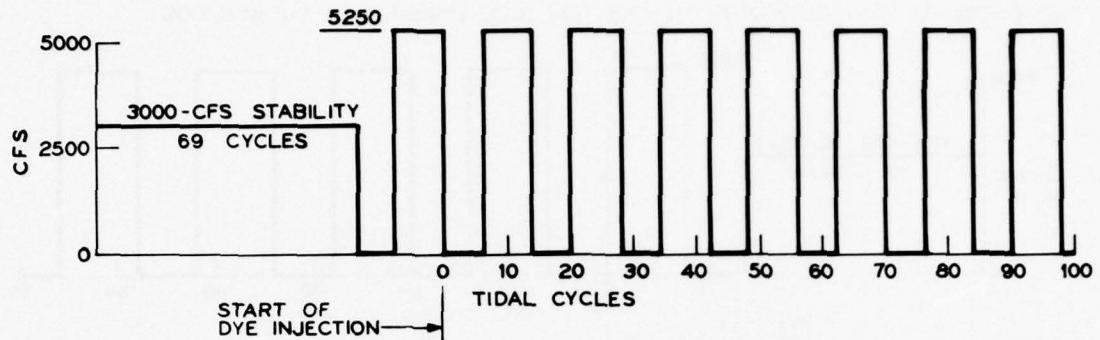


Figure 7. Test 3 discharge schedule

Schedule C hydrograph. At the end of the 3 days of zero flow, the dye concentrations during the high-water slack portion of the tidal cycle reached the maximum of 0.2 percent and fell off to 0 percent after 4 days of 5250-cfs flow. This was repeated throughout the hydrograph. Measurable concentrations of dye were detected upstream to sta 45C and downstream to sta 00C.

27. Plate 51 and Table 3 show that measurable dye concentrations were observed in the intake canal at sta BRC within three tidal cycles after injection. After five or six tidal cycles, the dye had reached sta BR1 and BR2 (Plates 52 and 53). The maximum concentration observed at BR1 was about 0.09 percent of initial concentration and about 0.05 percent at sta BR2.

Test 4

28. Test 4 had the same withdrawals and discharges as those in Test 1 except that the dye discharge was at Cooper River mile 33 and was at a rate of 30 cfs during the ebb phase of the tide and 0 cfs during each flood phase of the tide instead of the 15-cfs continuous dye discharge as in the previous test. The dye discharge was started after the first week of the Schedule C hydrograph and continued for 60 tidal cycles (Figure 8). Time-dye concentration plots for Test 4 are shown in Plates 56-72.

29. Measurable dye concentrations (0.03 percent) were detected

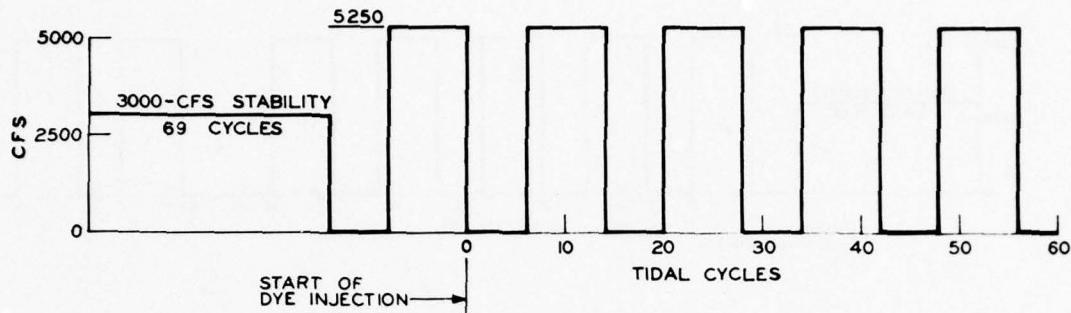


Figure 8. Test 4 discharge schedule

(Plate 67) at sta 43C within four tidal cycles after injection. Maximum dye concentrations reached about 0.15 percent of initial concentration. A noticeable fluctuation of dye concentrations was caused by the Schedule C hydrograph, varying from zero percent of initial concentration during the 5250-cfs flow period to 0.15 percent during the zero flow period. Measurable concentrations of dye were detected upstream to sta 45C and downstream to sta 00C.

30. Plate 70 and Table 3 show that measurable dye concentrations were observed at sta BRC within four tidal cycles after injection. After five tidal cycles, the dye had reached sta BR1 (Plate 71). The maximum concentration observed at BR1 was about 0.11 percent of initial concentration and about 0.08 percent at sta BR2.

Test 5

31. Test 5 had the same withdrawals and discharges as those in Test 1 except that the 15-cfs continuous dye discharge was at mile 30 in the Cooper River. After salinity stability was achieved, simulation of the Schedule C hydrograph began. After 1 week of the hydrograph, the 15-cfs dye discharge was started. At the request of the sponsors who were observing the test, after 56 tidal cycles of the hydrograph simulation, the flow at Pinopolis was reduced to zero for 12 tidal cycles, by which time the salinity at sta BR1 had reached 410 ppm. The flow at Pinopolis was then increased to 5250 cfs and the Schedule C hydrograph resumed (Figure 9) to determine flushing in the problem area. The test

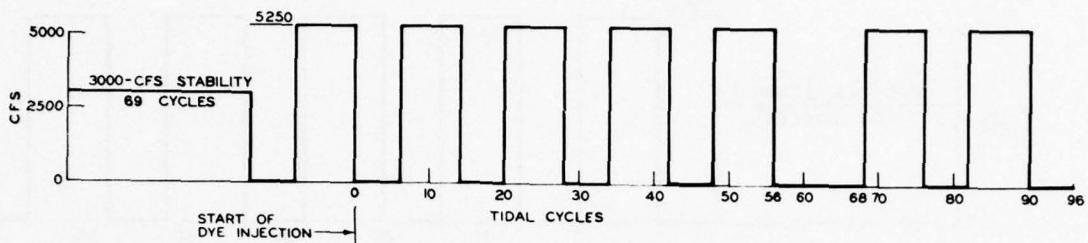


Figure 9. Test 5 discharge schedule

was concluded after 96 tidal cycles, by which time the salinity at sta BRL had dropped to 20 ppm. Time-dye concentration plots for Test 5 are shown in Plates 73-92.

32. Measurable dye concentrations (0.03 percent of initial concentration) were detected (Plate 85) at sta 43C within six tidal cycles after injection. Maximum dye concentrations reached about 0.07 percent of initial concentration during normal operation of Schedule C. During the period of zero flow (cycles 56-68), the peak concentration reached about 0.25 percent of initial concentration, and after resuming the Schedule C hydrograph, the peak concentration dropped back to 0.07 percent. During the initial operation with the Schedule C hydrograph, measurable concentrations of dye were detected upstream to sta 43C and downstream to sta 00C. During the period of no flow (cycles 56-68), the dye moved up to sta 45C but was flushed back to sta 43C after resuming Schedule C.

33. Plates 88-92 and Table 3 show that measurable dye concentrations were observed at sta BRC within five tidal cycles after injection (Plate 88) and after about 25 tidal cycles the dye had reached sta BRL. The maximum concentration observed at sta BRL and BR2 was about 0.02 percent of initial concentration during normal operation of Schedule C. During the period of zero flow (cycles 56-68), dye moved into the Back River Reservoir with maximum concentrations of about 0.09 to 0.13 percent of initial concentration. After resuming the Schedule C hydrograph, the dye was flushed from sta BRL with about 0.02 to 0.05 percent still remaining at sta BR2, BR3, and BR4 when the test was terminated.

Test 6

34. Test 6 was operated for the same withdrawals and discharges as those in Test 1 including the 15-cfs continuous dye discharge into Cooper River at mile 37.

35. The model was operated at a constant freshwater flow from Pinopolis of 3500 cfs for 69 cycles, followed by continuous operation of the Schedule E hydrograph (Table 2) and simulating all withdrawals and discharges except the continuous 15-cfs dye release.

36. After 1 weeks operation of the Schedule E hydrograph, the 15-cfs dye release was started. After 56 tidal cycles, the flow at Pinopolis was reduced to zero for 17 tidal cycles (Figure 10), by which time the salinity at sta BRL had reached 680 ppm. This was done to determine the rates of increases of waste concentrations at critical locations should a disaster reduce the freshwater discharge from Pinopolis to zero. Time-dye concentration plots for Test 6 are shown in Plates 93-115.

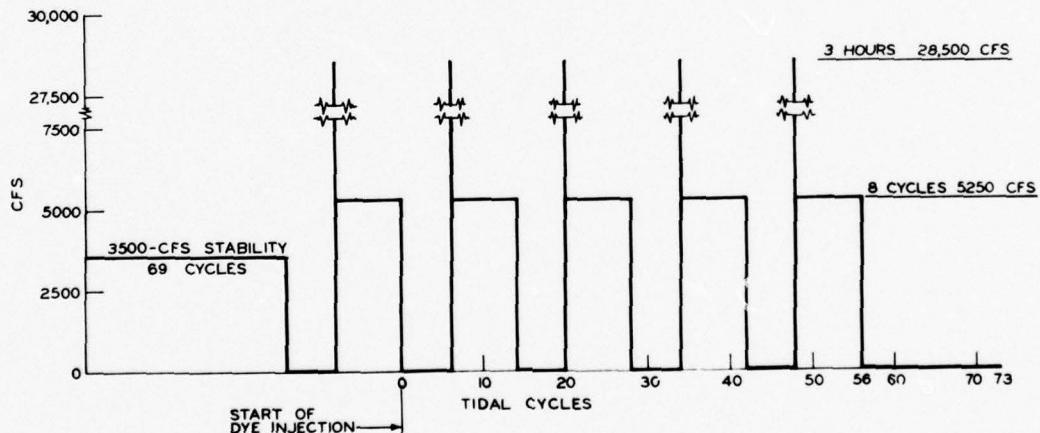


Figure 10. Test 6 discharge schedule

37. Measurable dye concentrations (0.06 percent of initial concentration) were detected (Plate 107) at sta 43C within three tidal cycles after injection. Maximum dye concentrations reached about 0.6 percent of initial concentration during the high-water slack period of the tidal cycle. During operation with the Schedule E hydrograph,

measurable concentrations of dye were detected upstream to sta 45C and downstream to sta 00C. There was no definite indication that the dye moved farther upstream during the period of zero flow.

38. Plate 111 and Table 3 show that measurable dye concentrations were observed at sta BRC within three tidal cycles after injection. After about four tidal cycles (Plates 112 and 113) dye had reached sta BR1 and BR2. The maximum concentration observed at sta BR1 was about 0.25 percent of initial concentration and about 0.2 percent at sta BR2.

PART IV: SALINITY TESTS AND RESULTS

39. During each dye dispersion test (Tests 1-6), salinity data were obtained at the Tee (mile 39.5) and sta 43C in the Cooper River and at various stations in the Back River Canal and Reservoir. In addition, the testing program was expanded to include three repeat tests in order to obtain more comprehensive salinity data in the Back River Reservoir and to check the previous salinity results. These tests are referred to as 1R, 2R, and 6R. Tests 1R and 2R were conducted exactly as Tests 1 and 2, respectively. Test 6R duplicated Test 6, except that the test was terminated after 6 cycles of zero flow instead of 17 cycles.

40. After salinity stability was obtained for Schedules C and E, high-water slack bottom salinity samples were taken after each zero and 5250-cfs flow period of the hydrograph. These data are included in Tables 4-12. Average maximum and minimum salinities for each location are presented in Table 13. The maximum salinities were obtained after the zero flow period of the hydrograph while the minimum salinities were obtained after the 5250-cfs flow period of the hydrograph. Averages of the data taken during the various tests indicate that maximum salinities in the Back River Reservoir for the Schedule C Pinopolis release varied from 15 ppm total salt at sta BR1 to 46 ppm at sta BR2. For the Schedule E Pinopolis release, the maximum salinities varied from 10 ppm at sta BR1 to 15 ppm at sta BR2 and BR3.

41. At the end of Tests 1, 1R, 5, and 6, the flow at Pinopolis was reduced to zero, and salinity samples were obtained to determine the effects of prolonged periods of zero flow on salinity concentrations in the Back River Reservoir. Results of these tests, shown in Table 14, indicate that salinity concentrations of about 70 to 120 ppm were detected in the Back River Reservoir (BR1 and BR2) after six cycles of zero flow with the Schedule C hydrograph. With the Schedule E hydrograph, salinities of this magnitude did not reach the Back River Reservoir until after about 11 cycles of zero flow (Table 14). At the end of Test 3 (after cycle 100, Figure 7), the flow at Pinopolis was reduced to 1135 cfs, and salinity samples were obtained to determine the effects

on salinity concentrations in the Back River Reservoir. This was done to determine the rates of increases of salinity concentrations at critical locations should a disaster reduce the freshwater discharge from Pinopolis to 1135 cfs. Results of this test along with the results of the zero flow after Test 1R, shown in Table 15, indicate that with the 1135-cfs continuous flow condition, salinity concentrations of about 90 ppm reached the Back River Reservoir (BR2) after about 18 tidal cycles. For a comparable test (1R) with zero flow, salinity concentrations of about 90 ppm reached the Back River Reservoir (BR2) after about 12 tidal cycles (Table 15).

42. Time-history plots were developed for selected stations from the data in Tables 4-12. Plates 116-119 present comparisons of salinities at sta 43, BRC, BR1, and BR2 for Test 3 during operation of the Schedule C hydrograph with salinities for Test 6 during operation of the Schedule E hydrograph. The plots show that during the Schedule C hydrograph, the salinity moved in and out of the Back River Reservoir as the flow changed from zero to 5250 cfs. During the zero flow period of the hydrograph, the salinity front moved into the reservoir and during the 5250-cfs flow period, the salinity front was moved out of the reservoir. This action continued throughout the hydrograph. For the Schedule E hydrograph, the salt did not move into the Back River Reservoir.

43. Salinity profiles for bottom depths at high-water slack for Cooper River during Pinopolis release Schedules C and E are shown in Plates 120 and 121, respectively. The salinity values shown in the two plates were determined by averaging measurements made on Tuesday after the zero flow period of the weekly release hydrograph and by averaging measurements made on Saturday after the high-flow period (Tables 1 and 2). During the hydrograph week, the salinity front would migrate between the two extremes.

44. The upstream limit of intrusion (100 ppm) of ocean salt water (high-water slack, bottom) was at approximately mile 43 for the 3000-cfs flow Schedule C (Plate 120). The upstream limit of intrusion of ocean salt water for the 3500-cfs flow Schedule E was at approximately mile 41 (Plate 121).

45. Profiles of salinity concentrations in Cooper River for bottom depths, at time of high-water slack, for the two schedules tested are repeated in Plate 122 for direct comparison of the effects of each schedule on the salinity distribution in the Cooper River during the zero flow period.

PART V: CONCLUSIONS

46. Based on the results of the model tests reported herein, the following conclusions have been derived regarding dye dispersion and salinity intrusion in the Charleston Estuary:

- a. For the Schedule C hydrograph and continuous dye release at Cooper River mile 37 (sta 37C), measurable concentrations reached the Back River Reservoir (sta BR1) within four tidal cycles after the release (Test 1). The maximum concentrations at BR1 were about 0.4 percent of initial concentration and about 0.6 percent at sta BR2. During the period of sustained zero flow (cycles 56-75), dye concentrations were increased to about 1.0 percent at sta BR1 and BR2.
- b. For the Schedule C hydrograph and the dye released at Cooper River mile 37 (sta 37C) at the rate of 30 cfs during each ebb phase of the tide and 0 cfs during each flood phase, measurable dye concentrations reached the Back River Reservoir (sta BR1) within four tidal cycles after the release (Test 2). The *maximum* concentration observed at BR1 was about 0.5 percent of initial concentration and about 0.3 percent at sta BR2. Comparison of Test 2 results with the continuous dye release at mile 37 (Test 1) showed that the dye arrived at sta BR1 about the same time with a noticeable reduction in the average maximum concentration in the Back River Reservoir from about 0.5 percent of initial concentration (Test 1) to about 0.4 percent (Test 2).
- c. For the Schedule C hydrograph and continuous dye release at Cooper River mile 33 (sta 33C), measurable dye concentrations reached the Back River Reservoir (sta BR1) within five tidal cycles after the release (Test 3). The maximum concentration observed at BR1 was about 0.09 percent of initial concentration and about 0.05 percent at sta BR2. Comparison of Test 3 with the continuous dye release at mile 37 (Test 1) showed that the dye arrived at sta BR1 about one tidal cycle later with a noticeable reduction in the average maximum concentration in the Back River Reservoir from about 0.5 percent of initial concentration (Test 1) to about 0.07 percent (Test 3).
- d. For the Schedule C hydrograph and continuous dye released at Cooper River mile 33 (sta 33C) at the rate of 30 cfs during each ebb phase of the tide and 0 cfs during each flood phase, measurable dye concentrations reached the Back River Reservoir (sta BR1) within five tidal cycles after the release (Test 4). The maximum concentration

observed at BR1 was about 0.11 percent of initial concentration and about 0.08 percent at sta BR2.

- e. For the Schedule C hydrograph and continuous dye release at Cooper River mile 30 (sta 30C), measurable dye concentrations reached the Back River Reservoir (sta BR1) within 25 tidal cycles after the release (Test 5). The maximum concentration observed at BR1 and BR2 was about 0.02 percent of initial concentration during normal operation of Schedule C. During the period of zero flow (cycles 56-68), dye moved into the Back River Reservoir with maximum concentrations of about 0.09 to 0.13 percent of initial concentration. After resuming the Schedule C hydrograph, the dye was flushed from sta BR1 with about 0.02 to 0.05 percent still remaining at sta BR2, BR3, and BR4 when the test was terminated. Comparison of the results of Test 5 (dye released at mile 30) with the results of Test 1 (dye released at mile 37) showed that the dye arrived at sta BR1 about 21 tidal cycles later with a reduction in the average maximum concentration in the Back River Reservoir from about 0.5 percent of initial concentration (Test 1) to about 0.02 percent (Test 5). Comparison of Test 5 with Test 3 (dye released at mile 33) showed that the dye arrived at sta BR1 about 20 tidal cycles later with a reduction in the average maximum concentration in Back River Reservoir from about 0.07 percent of initial concentration (Test 3) to about 0.02 (Test 5).
- f. For the Schedule E hydrograph and continuous dye release at Cooper River mile 37 (sta 37C), measurable dye concentrations reached the Back River Reservoir (sta BR1) within three tidal cycles after the release (Test 6). The maximum concentration observed at BR1 was about 0.25 percent of initial concentration and about 0.2 percent at sta BR2. Comparison of the results of Test 6 (Schedule E hydrograph and dye released at mile 37) with the results of Test 1 (Schedule C hydrograph and dye released at mile 37) showed that within four tidal cycles the average maximum concentration was observed in the Back River Reservoir with an average maximum of about 0.5 percent of initial concentration for Test 1 and 0.25 percent for Test 6.
- g. For the Schedule C hydrograph, maximum salinities in the Back River Reservoir varied from 15 ppm total salt at sta BR1 to 46 ppm at sta BR2. For the Schedule E hydrograph, the maximum salinities varied from 10 ppm at sta BR1 to 15 ppm at sta BR2 and BR3.
- h. The upstream limit of intrusion (100 ppm) of ocean salt water (high-water slack, bottom) was approximately Cooper River mile 43 (sta 43C) for Schedule C and approximately Cooper River mile 41 (sta 41C) for Schedule E.

Table 1
Schedule C Pinopolis Releases After Rediversion
Zero Flow for 72 hr; Weekly Average 3000 cfs

| Hour | Sunday P M | Monday P M | Tuesday P M | Wednesday P M | Thursday P M | Friday P M | Saturday P M |
|---------------|------------------|------------------|-------------------|---------------------|--------------------|------------------|--------------------|
| 1 a.m. | 0 | 0 | 0 | 1,200 | 5,250 | 1,200 | 5,250 |
| 2 | 0 | 0 | 0 | 1,200 | 5,250 | 1,200 | 5,250 |
| 3 | 0 | 0 | 0 | 1,200 | 5,250 | 1,200 | 5,250 |
| 4 | 0 | 0 | 0 | 1,200 | 5,250 | 1,200 | 5,250 |
| 5 | 0 | 0 | 0 | 1,200 | 5,250 | 1,200 | 5,250 |
| 6 | 0 | 0 | 0 | 1,200 | 5,250 | 1,200 | 5,250 |
| 7 | 0 | 0 | 0 | 1,200 | 5,250 | 1,200 | 5,250 |
| 8 | 0 | 0 | 0 | 1,200 | 5,250 | 1,200 | 5,250 |
| 9 | 0 | 0 | 0 | 1,200 | 5,250 | 1,200 | 5,250 |
| 10 | 0 | 0 | 0 | 1,200 | 5,250 | 1,200 | 5,250 |
| 11 | 0 | 0 | 0 | 1,200 | 5,250 | 1,200 | 5,250 |
| 12 N | 0 | 0 | 0 | 1,200 | 5,250 | 1,200 | 5,250 |
| 1 p.m. | 0 | 0 | 0 | 1,200 | 5,250 | 1,200 | 5,250 |
| 2 | 0 | 0 | 0 | 1,200 | 5,250 | 1,200 | 5,250 |
| 3 | 0 | 0 | 0 | 1,200 | 5,250 | 1,200 | 5,250 |
| 4 | 0 | 0 | 0 | 1,200 | 5,250 | 1,200 | 5,250 |
| 5 | 0 | 0 | 0 | 1,200 | 5,250 | 1,200 | 5,250 |
| 6 | 0 | 0 | 0 | 1,200 | 5,250 | 1,200 | 5,250 |
| 7 | 0 | 0 | 0 | 1,200 | 5,250 | 1,200 | 5,250 |
| 8 | 0 | 0 | 0 | 1,200 | 5,250 | 1,200 | 5,250 |
| 9 | 0 | 0 | 0 | 1,200 | 5,250 | 1,200 | 5,250 |
| 10 | 0 | 0 | 0 | 1,200 | 5,250 | 1,200 | 5,250 |
| 11 | 0 | 0 | 0 | 1,200 | 5,250 | 1,200 | 5,250 |
| 12 M | 0 | 0 | 0 | 1,200 | 5,250 | 1,200 | 5,250 |
| Total | 0 | 0 | 0 | 126,000 | 126,000 | 126,000 | 126,000 |
| Daily average | 0 | 0 | 0 | 5,250 | 5,250 | 5,250 | 5,250 |

Table 2
Schedule E Pinopolis Releases After Rediversion
Zero Flow for 69 hr; Weekly Average 3500 cfs

Table 3
Dye Release Summary Table

| Test | Pinopolis Release Schedule | Continuous Dye Release of 15 cfs at River Mile | EBB Dye Release of 30 cfs at River Mile | Arrival Time Cycles After Release | BR1 BR2 | Maximum Concentration Percent of Initial Concentration | | | |
|------|----------------------------------|---|--|--------------------------------------|------------|--|------|------|------|
| | | | | | | BR1 | BR2 | BR3 | BR4 |
| 1 | C | 37 | 37 | 1 4 | 3 | 0.9 | 0.4 | 0.6 | |
| 2 | C | | | 1 4 | 5 | 0.8 | 0.5 | 0.3 | |
| 3 | C | 33 | | 3 5 | 6 | 0.15 | 0.09 | 0.05 | 0.04 |
| 4 | C | | 33 | 4 5 | 8 | 0.2 | 0.11 | 0.08 | |
| 5 | C | 30 | | 5 25 | 25 | 0.04 | 0.02 | 0.01 | 0.01 |
| 6 | E | 37 | | 1 3 4 | 4 | 0.4 | 0.25 | 0.2 | 0.16 |

Table 4
High-Water Slack Bottom Salinities (ppm) at Selected
Locations for Pinopolis Release Schedule C, Test 1

| Flow cfs | Cycles After Stability | Salinity, ppm | | | |
|-------------|------------------------------|---------------|-----|-----|-----|
| | | Tee | 43C | BRC | BR1 |
| 0 | 1 | 100 | | | 110 |
| | 2 | | 60 | | |
| | 3 | 160 | | | 100 |
| | 4 | | 110 | | |
| | 5 | 370 | | | 100 |
| | 6 | | 270 | | |
| 5250 | 7 | 770 | | | 90 |
| | 8 | | 150 | | |
| | 9 | 470 | | | 80 |
| | 10 | | 70 | | |
| | 11 | | | | |
| | 12 | | | | |
| | 13 | | | | |
| | 14 | 90 | | | 100 |
| | 15 | | 50 | | |
| | 16 | | | | |
| | 17 | | | | |
| | 18 | | | | |
| | 19 | 510 | | | 80 |
| | 20 | | 180 | | |
| 5250 | 21 | | | | |
| | 22 | | | | |
| | 23 | | | | |
| | 24 | 280 | | | 70 |
| | 25 | | 40 | | |
| | 26 | | | | |
| | 27 | | | | |
| | 28 | | | | |
| 0 | 29 | 100 | | | 80 |
| | 30 | | 50 | | |
| | 31 | | | | |
| | 32 | | | | |
| | 33 | 480 | | | 60 |
| | 34 | | | | |

(Continued)

(Sheet 1 of 3)

Table 4 (Continued)

| Flow cfs | Cycles After <u>Stability</u> | Salinity, ppm | | | |
|-------------|-------------------------------------|---------------|------|-----|-----|
| | | Tee | 43C | BRC | BR1 |
| 5250 | 35 | | 180 | | |
| | 36 | | | | |
| | 37 | | | | |
| | 38 | | | | |
| | 39 | 140 | | | 60 |
| | 40 | | 50 | | |
| | 41 | | | | |
| | 42 | | | | |
| 0 | 43 | | | | |
| | 44 | 50 | | | 90 |
| | 45 | | 80 | | |
| | 46 | | | | |
| | 47 | | | | |
| | 48 | | | | |
| 5250 | 49 | 580 | | | 70 |
| | 50 | | 70 | | |
| | 51 | | | | |
| | 52 | | | | |
| | 53 | | | | |
| | 54 | 120 | | | 50 |
| | 55 | | 40 | | |
| | 56 | | | | |
| 0 | 57 | | | | |
| | 58 | | | | |
| | 59 | 90 | | 10 | 90 |
| | 60 | | 110 | | |
| | 61 | 270 | | 40 | |
| | 62 | | | | 120 |
| | 63 | 640 | 230 | 50 | 140 |
| | 64 | | 340 | | 180 |
| | 65 | 1020 | | 110 | 280 |
| | 66 | | 680 | | 250 |
| | 67 | 1720 | | 220 | 230 |
| | 68 | | 1120 | | 350 |
| | 69 | 2320 | | 440 | 540 |
| | 70 | | 1620 | | 480 |
| | | | | 650 | |

(Continued)

(Sheet 2 of 3)

Table 4 (Concluded)

| <u>Flow cfs</u> | <u>Cycles After Stability</u> | <u>Salinity, ppm</u> | | | |
|---------------------|---------------------------------------|----------------------|------------|------------|------------|
| | | <u>Tee</u> | <u>43C</u> | <u>BRC</u> | <u>BR1</u> |
| 0 | 71 | | | | 1190 |
| | 72 | | | | |
| | 73 | | | | |
| | 74 | | 3620 | 1120 | 1320 |
| | 75 | | 2720 | | 690 |
| 28,500 | 76 | | 60 | 310 | 780 |
| | 77 | | 20 | | 540 |
| | 78 | | 10 | 60 | 650 |
| | 79 | | 10 | | 440 |
| | 80 | 60 | 0 | 0 | 260 |
| | 81 | | 0 | | 140 |
| | 82 | 0 | 0 | 30 | 80 |
| | 83 | | 0 | | 40 |
| | 84 | 0 | 0 | 0 | 40 |
| | 85 | | 0 | | 20 |
| | 86 | 0 | 0 | 0 | 20 |
| | 87 | | 0 | | 1490 |
| | 88 | | | | 40 |

Table 5
High-Water Slack Bottom Salinities (ppm) at Selected
Locations for Pinopolis Release Schedule C, Test 1R

| Flow cfs | Cycles After Stability | Salinity, ppm | | | | | |
|-------------|------------------------------|---------------|-----|-----|-----|-----|-----|
| | | Tee | 43C | BRC | BR1 | BR2 | BR3 |
| 0 | 1 | | 10 | 0 | | | |
| | 2 | | 10 | 0 | | | |
| | 3 | | 20 | 90 | | | |
| | 4 | | 60 | 20 | | | |
| | 5 | | 120 | 40 | | | |
| | 6 | 650 | 200 | 90 | 20 | 10 | 20 |
| 5250 | 7 | | 190 | 170 | | | |
| | 8 | | 80 | 130 | | | |
| | 9 | | 50 | 70 | | | |
| | 10 | | 20 | 40 | | | |
| | 11 | | 20 | 30 | | | |
| | 12 | | 20 | 30 | | | |
| | 13 | | 10 | 20 | | | |
| | 14 | 60 | 10 | 10 | 10 | 20 | 20 |
| | 15 | | | | | | |
| | 16 | | | | | | |
| | 17 | | | | | | |
| | 18 | | | | | | |
| | 19 | | | | | | |
| 0 | 20 | 530 | 190 | 90 | 30 | 20 | 30 |
| | 21 | | | | | | |
| | 22 | | | | | | |
| | 23 | | | | | | |
| | 24 | | | | | | |
| | 25 | | | | | | |
| 5250 | 26 | | | | | | |
| | 27 | | | | | | |
| | 28 | 60 | 30 | 10 | 20 | 30 | 20 |
| | 29 | | | | | | |
| | 30 | | | | | | |
| | 31 | | | | | | |
| 0 | 32 | | | | | | |
| | 33 | | | | | | |
| | 34 | 360 | 100 | 50 | 20 | 20 | 20 |

(Continued)

(Sheet 1 of 3)

Table 5 (Continued)

| Flow cfs | Cycles After Stability | Salinity, ppm | | | | | |
|-------------|------------------------------|---------------|-----|-----|-----|-----|-----|
| | | Tee | 43C | BRC | BR1 | BR2 | BR3 |
| 5250 | 35 | | | | | | |
| | 36 | | | | | | |
| | 37 | | | | | | |
| | 38 | | | | | | |
| | 39 | | | | | | |
| | 40 | | | | | | |
| | 41 | | | | | | |
| | 42 | 40 | 20 | 10 | 10 | 20 | 20 |
| 0 | 43 | | | | | | |
| | 44 | | | | | | |
| | 45 | | | | | | |
| | 46 | | | | | | |
| | 47 | | | | | | |
| | 48 | 490 | 160 | 70 | 20 | 20 | 30 |
| 5250 | 49 | | | | | | |
| | 50 | | | | | | |
| | 51 | | | | | | |
| | 52 | | | | | | |
| | 53 | | | | | | |
| | 54 | | | | | | |
| | 55 | | | | | | |
| | 56 | 50 | 30 | 10 | 20 | 30 | 60 |
| 0 | 57 | | | | | | |
| | 58 | | | | | | |
| | 59 | | 30 | 10 | | 20 | |
| | 60 | 130 | 60 | 10 | 20 | 20 | 40 |
| | 61 | | 70 | 20 | | 20 | |
| | 62 | | 120 | 60 | | 20 | |
| 5250 | 63 | | 110 | 100 | | 60 | |
| | 64 | | 60 | 90 | | 50 | |
| | 65 | | 40 | 50 | | 40 | |
| | 66 | | 30 | 30 | | 90 | |
| | 67 | 110 | 20 | 20 | 30 | 70 | 30 |
| | 68 | | 10 | 20 | | 80 | |
| | 69 | | 0 | 0 | | 80 | |
| | 70 | 50 | 0 | 0 | 20 | 50 | 30 |
| 0 | 71 | | 0 | 0 | | 70 | |
| | 72 | | 0 | 10 | | 60 | |
| | 73 | | 10 | 0 | | 70 | |
| | 74 | 50 | 20 | 0 | 10 | 60 | 50 |

(Continued)

(Sheet 2 of 3)

Table 5 (Concluded)

| <u>Flow cfs</u> | <u>Cycles After Stability</u> | <u>Tee</u> | <u>Salinity, ppm</u> | | | | |
|---------------------|---------------------------------------|------------|----------------------|------------|------------|------------|------------|
| | | | <u>43C</u> | <u>BRC</u> | <u>BR1</u> | <u>BR2</u> | <u>BR3</u> |
| 0 | 75 | | 50 | 10 | | 30 | |
| | 76 | | 170 | 40 | | 70 | |
| | 77 | | 260 | 180 | | 40 | |
| | 78 | | 370 | 200 | | 70 | |
| | 79 | | 500 | 280 | | 60 | |
| | 80 | | 710 | 440 | | 60 | |
| | 81 | 2420 | 1120 | 700 | 330 | 50 | 40 60 |
| | 82 | | 1720 | 1020 | | 90 | |
| | 83 | | 2020 | 1320 | | 200 | |
| | 84 | | 2220 | 1820 | | 320 | |
| | 85 | | 2520 | 2120 | | 450 | |
| | 86 | | 2720 | 2320 | | 610 | |
| | 87 | | 2820 | 2520 | | 810 | |
| | 88 | | 3120 | 2720 | | 1020 | |
| | 89 | 4220 | 3320 | 3020 | 1720 | 1120 | 780 520 |
| 28,500 | 90 | | 50 | 3120 | | 1320 | |
| | 91 | | 10 | 100 | | 2120 | |
| | 92 | | 0 | 30 | | 2220 | |
| | 93 | | 0 | 10 | | 2220 | |
| | 94 | | 20 | 20 | | 2120 | |
| | 95 | | 10 | 0 | | 2220 | |
| | 96 | | 0 | 0 | | 2120 | |
| | 97 | | 0 | 0 | | 2120 | |
| | 98 | | 0 | 0 | | 2020 | |
| | 99 | | 0 | 0 | | 2020 | |
| | 100 | | 10 | 0 | | 1920 | |
| | 101 | | 30 | 10 | | 1620 | |

Table 6
High-Water Slack Bottom Salinities (ppm) at Selected
Locations for Pinopolis Release Schedule C, Test 2

| Flow cfs | Cycles After Stability | Tee | Salinity, ppm | |
|-------------|------------------------------|-----|---------------|-----|
| | | | 43C | BR2 |
| 0 | 1 | 180 | | |
| | 2 | | 30 | |
| | 3 | 160 | | 190 |
| | 4 | | 120 | |
| | 5 | 430 | | 70 |
| | 6 | | 290 | |
| 5250 | 7 | 810 | | 70 |
| | 8 | | 150 | |
| | 9 | 460 | | 80 |
| | 10 | | 60 | |
| | 11 | | | |
| | 12 | | | |
| | 13 | | | |
| | 14 | 80 | | 80 |
| | 15 | | 20 | |
| | 16 | | | |
| | 17 | | | |
| | 18 | | | |
| | 19 | 270 | | 60 |
| | 20 | | 190 | |
| 5250 | 21 | | | |
| | 22 | | | |
| | 23 | | | |
| | 24 | 170 | | 110 |
| | 25 | | | |
| | 26 | | | |
| | 27 | | | |
| | 28 | | | |
| 0 | 29 | 30 | | 60 |
| | 30 | | 10 | |
| | 31 | | | |
| | 32 | | | |
| | 33 | | | |
| | 34 | 540 | | 50 |

(Continued)

Table 6 (Concluded)

| <u>Flow cfs</u> | <u>Cycles After Stability</u> | <u>Tee</u> | <u>Salinity, ppm</u> | |
|---------------------|---------------------------------------|------------|----------------------|------------|
| | | | <u>43C</u> | <u>BR2</u> |
| 5250 | 35 | | 140 | |
| | 36 | | | |
| | 37 | | | |
| | 38 | | | |
| | 39 | 220 | | |
| | 40 | | 20 | 90 |
| | 41 | | | |
| | 42 | | | |
| 0 | 43 | | | |
| | 44 | 80 | | |
| | 45 | | 40 | 50 |
| | 46 | | | |
| | 47 | | | |
| | 48 | | | |
| 5250 | 49 | 540 | | 140 |
| | 50 | | 70 | |
| | 51 | | | |
| | 52 | | | |
| | 53 | | | |
| | 54 | 140 | | 60 |
| | 55 | | 20 | |
| | 56 | | | |
| 0 | 57 | | | |
| | 58 | | | |
| | 59 | 70 | | 50 |
| | 60 | | | |

Table 7
High-Water Slack Bottom Salinities (ppm) at Selected
Locations for Pinopolis Release Schedule C, Test 2R

| Flow cfs | Cycles After Stability | Salinity, ppm | | | |
|-------------|------------------------------|---------------|-----|-----|-----|
| | | Tee | 43C | BRC | BR1 |
| 0 | 1 | | | | |
| | 2 | | | | |
| | 3 | | | | |
| | 4 | | | | |
| | 5 | | | | |
| | 6 | 330 | 140 | 300 | 10 |
| 5250 | 7 | | | | |
| | 8 | | | | |
| | 9 | | | | |
| | 10 | | | | |
| | 11 | | | | |
| | 12 | | | | |
| | 13 | | | | |
| | 14 | 30 | 20 | 140 | 10 |
| 0 | 15 | | | | |
| | 16 | | | | |
| | 17 | | | | |
| | 18 | | | | |
| | 19 | | | | |
| | 20 | 350 | 110 | 110 | 10 |
| 5250 | 21 | | | | |
| | 22 | | | | |
| | 23 | | | | |
| | 24 | | | | |
| | 25 | | | | |
| | 26 | | | | |
| | 27 | | | | |
| | 28 | 20 | 0 | 20 | 10 |
| 0 | 29 | | | | |
| | 30 | | | | |
| | 31 | | | | |
| | 32 | | | | |
| | 33 | | | | |
| | 34 | 290 | 80 | 20 | 0 |
| | | | | | 30 |

(Continued)

Table 7 (Concluded)

| <u>Flow cfs</u> | <u>Cycles After Stability</u> | <u>Tee</u> | <u>43C</u> | <u>Salinity, ppm</u> | <u>BRC</u> | <u>BR1</u> | <u>BR2</u> |
|---------------------|---------------------------------------|------------|------------|----------------------|------------|------------|------------|
| 5250 | 35 | | | | | | |
| | 36 | | | | | | |
| | 37 | | | | | | |
| | 38 | | | | | | |
| | 39 | | | | | | |
| | 40 | | | | | | |
| | 41 | | | | | | |
| | 42 | 60 | 30 | 60 | 0 | 10 | |
| 0 | 43 | | | | | | |
| | 44 | | | | | | |
| | 45 | | | | | | |
| | 46 | | | | | | |
| | 47 | | | | | | |
| | 48 | 260 | 70 | 60 | 20 | 10 | |
| 5250 | 49 | | | | | | |
| | 50 | | | | | | |
| | 51 | | | | | | |
| | 52 | | | | | | |
| | 53 | | | | | | |
| | 54 | | | | | | |
| | 55 | | | | | | |
| | 56 | 10 | 10 | 30 | 0 | 10 | |
| 0 | 57 | | | | | | |
| | 58 | | | | | | |
| | 59 | | | | | | |
| | 60 | 50 | 30 | 100 | 20 | 10 | |

Table 8
High-Water Slack Bottom Salinities (ppm) at Selected
Locations for Pinopolis Release Schedule C, Test 3

| Flow cfs | Cycles After Stability | Salinity, ppm | | | | | |
|-------------|------------------------------|---------------|-----|-----------------|-----------------|-----------------|-----------------|
| | | Tee | 43C | BR _C | BR ₁ | BR ₂ | BR ₃ |
| 0 | 1 | 30 | 0 | | 10 | 20 | |
| | 2 | | | 0 | 10 | 30 | 0 |
| | 3 | 90 | 0 | | | 20 | |
| | 4 | | | 10 | 0 | | 10 |
| | 5 | 310 | 30 | | | 10 | |
| | 6 | | | 50 | 10 | 0 | 0 |
| 5250 | 7 | 450 | 90 | | | 10 | |
| | 8 | | | 90 | 40 | 20 | 0 |
| | 9 | 310 | 10 | | | 10 | |
| | 10 | | | 20 | 20 | 0 | 10 |
| | 11 | | | | | 30 | 0 |
| | 12 | | | | | | 10 |
| 0 | 13 | | | | | | |
| | 14 | 40 | 0 | 20 | 20 | 10 | |
| | 15 | | | 0 | 0 | 0 | 10 |
| | 16 | | | | | | |
| | 17 | | | | | | |
| | 18 | | | | | | |
| 5250 | 19 | 160 | 20 | | | 10 | |
| | 20 | | 60 | 20 | 10 | 10 | 10 |
| | 21 | | | | | | |
| | 22 | | | | | | |
| | 23 | | | | | | |
| | 24 | 110 | 0 | | | 10 | |
| 0 | 25 | | | 20 | 10 | 10 | 10 |
| | 26 | | | | | | |
| | 27 | | | | | | |
| | 28 | | 0 | 10 | 0 | 20 | |
| | 29 | 30 | 0 | | | 10 | |
| | 30 | | | 0 | 0 | 10 | 10 |
| 31 | 31 | | | | | | |
| | 32 | | | | | | |
| | 33 | | | | | 10 | |
| | 34 | 410 | 90 | 40 | 10 | 0 | |

(Continued)

(Sheet 1 of 3)

Table 8 (Continued)

| <u>Flow cfs</u> | <u>Cycles After Stability</u> | <u>Tee</u> | <u>43C</u> | <u>BRC</u> | <u>BR1</u> | <u>BR2</u> | <u>BR3</u> | <u>BR4</u> |
|---------------------|---------------------------------------|------------|------------|------------|------------|------------|------------|------------|
| 5250 | 35 | | | 60 | 20 | | 10 | 50 |
| | 36 | | | | | | | |
| | 37 | | | | | | | |
| | 38 | | | | | | | |
| | 39 | 120 | 0 | | | 10 | | |
| | 40 | | | 20 | 10 | | 10 | 10 |
| | 41 | | | | | | | |
| | 42 | | 0 | 0 | 10 | 30 | | |
| 0 | 43 | | | | | | | |
| | 44 | 30 | 0 | | | 20 | | |
| | 45 | | | 0 | 0 | | 10 | 20 |
| | 46 | | | | | | | |
| | 47 | | | | | 20 | | |
| | 48 | | 80 | 30 | 10 | | | |
| 5250 | 49 | 350 | 40 | | | 0 | | |
| | 50 | | | 70 | 30 | | 20 | 30 |
| | 51 | | | | | | | |
| | 52 | | | | | | | |
| | 53 | | | | | | | |
| | 54 | 70 | 0 | | | 20 | | |
| | 55 | | | 10 | 10 | 20 | 10 | 20 |
| | 56 | | 0 | 0 | 20 | | | |
| 0 | 57 | | | | | | | |
| | 58 | | | | | | | |
| | 59 | 60 | 10 | | | 10 | | |
| | 60 | | | 20 | 0 | | 20 | 30 |
| | 61 | | | | | | | |
| | 62 | | 90 | 40 | 10 | 20 | | |
| 5250 | 63 | | | | | | | |
| | 64 | 310 | 40 | | | 10 | | |
| | 65 | | | 50 | 20 | | 20 | 20 |
| | 66 | | | | | | | |
| | 67 | | | | | | | |
| | 68 | | | | | | | |
| | 69 | 40 | 0 | | | 20 | | |
| | 70 | | 0 | 10 | 10 | 10 | 20 | 20 |
| 0 | 71 | | | | | | | |
| | 72 | | | | | | | |
| | 73 | | | | | | | |
| | 74 | 180 | 10 | | | 10 | | |
| | 75 | | | 20 | 10 | | 20 | 30 |
| | 76 | | 80 | 30 | 10 | | | |

(Continued)

(Sheet 2 of 3)

Table 8 (Concluded)

| <u>Flow cfs</u> | <u>Cycles After Stability</u> | <u>Tee</u> | <u>43C</u> | <u>Salinity, ppm</u> | | | | |
|---------------------|---------------------------------------|------------|------------|----------------------|------------|------------|------------|------------|
| | | | | <u>BRC</u> | <u>BRI</u> | <u>BR2</u> | <u>BR3</u> | <u>BR4</u> |
| 5250 | 77 | | | | | | | |
| | 78 | | | | | | | |
| | 79 | 210 | 10 | | | 30 | | |
| | 80 | | | 30 | 10 | | 20 | 30 |
| | 81 | | | | | | | |
| | 82 | | | | | | | |
| | 83 | | | | | | | |
| | 84 | 30 | 0 | 0 | 0 | 20 | | |
| 0 | 85 | | | 0 | 0 | | 20 | 30 |
| | 86 | | | | | | | |
| | 87 | | | | | | | |
| | 88 | | | | | | | |
| | 89 | 200 | 20 | | | 20 | | |
| | 90 | | 40 | 20 | 10 | 10 | 20 | 30 |
| 5250 | 91 | | | | | | | |
| | 92 | | | | | | | |
| | 93 | | | | | | | |
| | 94 | 170 | 0 | | | 30 | | |
| | 95 | | | 20 | 10 | | 20 | 30 |
| | 96 | | | | | | | |
| | 97 | | | | | | | |
| | 98 | | 0 | 0 | 0 | 10 | | |
| 0 | 99 | 30 | 0 | 10 | | 40 | | |
| 0 | 100 | | 0 | 10 | 0 | 20 | 60 | 30 |
| 1135 | 101 | | 10 | 10 | | 20 | | |
| | 102 | | 10 | 10 | | 20 | | |
| | 103 | | 50 | 10 | | 20 | | |
| | 104 | | 50 | 30 | | 40 | | |
| | 105 | | 60 | 60 | | 10 | | |
| | 106 | | 90 | 60 | | 20 | | |
| | 107 | | 120 | 60 | | 30 | | |
| | 108 | | 160 | 120 | | 20 | | |
| | 109 | | 190 | 150 | | 40 | | |
| | 110 | | 150 | 170 | | 30 | | |
| | 111 | | 260 | 190 | | 30 | | |
| | 112 | | 260 | 230 | | 40 | | |
| | 113 | | 260 | 240 | | 50 | | |
| | 114 | | 370 | 220 | | 50 | | |
| | 115 | | 410 | 300 | | 60 | | |
| | 116 | | 410 | 330 | | 80 | | |
| | 117 | | 460 | 340 | | 80 | | |
| | 118 | | 500 | 360 | | 90 | | |
| | 119 | | 560 | 400 | | | | |
| | 120 | | 570 | 450 | | 150 | | |

Table 9
High-Water Slack Bottom Salinities (ppm) at Selected
Locations for Pinopolis Release Schedule C, Test 4

| Flow cfs | Cycles After Stability | <u>Tee</u> | Salinity, ppm | |
|-------------|------------------------------|------------|---------------|------------|
| | | | <u>43C</u> | <u>BR2</u> |
| 0 | 1 | 50 | | 40 |
| | 2 | | 30 | |
| | 3 | 110 | | 30 |
| | 4 | | 40 | |
| | 5 | 300 | | 20 |
| | 6 | | 130 | |
| 5250 | 7 | 70 | | 40 |
| | 8 | | 100 | |
| | 9 | 320 | | 20 |
| | 10 | | | |
| | 11 | | | |
| | 12 | | | |
| 0 | 13 | | | |
| | 14 | 80 | | 30 |
| | 15 | | 20 | |
| | 16 | | | |
| | 17 | | | |
| | 18 | | | |
| 5250 | 19 | 260 | | 20 |
| | 20 | | 80 | |
| | 21 | | | |
| | 22 | | | |
| | 23 | | | |
| | 24 | 250 | | 20 |
| 0 | 25 | | 0 | |
| | 26 | | | |
| | 27 | | | |
| | 28 | | | |
| | 29 | 60 | | 40 |
| | 30 | | 30 | |
| | 31 | | | |
| | 32 | | | |
| | 33 | | | |
| | 34 | 270 | | 50 |

(Continued)

Table 9 (Concluded)

| <u>Flow cfs</u> | <u>Cycles After Stability</u> | <u>Tee</u> | <u>Salinity, ppm</u> | <u>BR2</u> |
|---------------------|--|------------|----------------------|------------|
| | | | <u>43C</u> | |
| 5250 | 35 36 37 38 39 40 41 42 | | 30 | |
| 0 | 43 44 45 46 47 48 | 80 20 | 0 10 | 20 |
| 5250 | 49 50 51 52 53 54 55 56 | 800 150 | 50 0 | 20 |
| 0 | 57 58 59 60 | 150 | 50 | 60 |

Table 10
High-Water Slack Bottom Salinities (ppm) at Selected
Locations for Pinopolis Release Schedule C, Test 5

| Flow cfs | Cycles After Stability | Salinity, ppm | | | | | |
|-------------|------------------------------|---------------|-----|-----|-----|-----|-----|
| | | Tee | 43C | BRC | BR1 | BR2 | BR3 |
| 0 | 1 | 30 | | 10 | | 110 | |
| | 2 | | 20 | | 10 | | 40 |
| | 3 | 120 | | 10 | | 100 | |
| | 4 | | 70 | | 10 | | 40 |
| | 5 | 240 | | 20 | | 70 | |
| | 6 | | 60 | 50 | 10 | | 40 |
| 5250 | 7 | 380 | | 100 | | | |
| | 8 | | 0 | | 30 | | 40 |
| | 9 | 170 | | 30 | | 50 | |
| | 10 | | 0 | | 10 | | 40 |
| | 11 | | | | | | 10 |
| | 12 | | | | | | 40 |
| 0 | 13 | | | | | | 30 |
| | 14 | 20 | 0 | 0 | 0 | 30 | |
| | 15 | | 0 | | 0 | | 40 |
| | 16 | | | | | | 40 |
| | 17 | | | | | | |
| | 18 | | | | | | |
| 5250 | 19 | 300 | | 40 | | 50 | |
| | 20 | | 50 | 50 | 0 | | 30 |
| | 21 | | | | | | |
| | 22 | | | | | | |
| | 23 | | | | | | |
| | 24 | 170 | | 30 | | 40 | |
| 0 | 25 | | 10 | | 10 | | 30 |
| | 26 | | | | | | 40 |
| | 27 | | | | | | |
| | 28 | | 10 | 0 | 0 | | |
| | 29 | 20 | | 0 | | 30 | |
| | 30 | | 20 | | | 30 | |
| 5250 | 31 | | | | | | |
| | 32 | | | | | | |
| | 33 | | | | | | |
| | 34 | 430 | 70 | 50 | 0 | 40 | |

(Continued)

(Sheet 1 of 3)

Table 10 (Continued)

| <u>Flow cfs</u> | <u>Cycles After Stability</u> | <u>Tee</u> | <u>43C</u> | <u>BRC</u> | <u>Salinity, ppm</u> | <u>BR1</u> | <u>BR2</u> | <u>BR3</u> | <u>BR4</u> |
|---------------------|---------------------------------------|------------|------------|------------|----------------------|------------|------------|------------|------------|
| 5250 | 35 | | 10 | | 10 | | | 20 | 30 |
| | 36 | | | | | | | | |
| | 37 | | | | | | | | |
| | 38 | | | 10 | | | | | |
| | 39 | 70 | | | | | 40 | | |
| | 40 | | 0 | | 10 | | | 80 | 20 |
| | 41 | | | | | | | | |
| | 42 | | 10 | 0 | 0 | | | | |
| 0 | 43 | | | | | | | | |
| | 44 | 20 | | 0 | | | 40 | | |
| | 45 | | 40 | | 0 | | | 20 | 20 |
| | 46 | | | | | | | | |
| | 47 | | | | | | | | |
| | 48 | | 40 | 50 | 0 | | | | |
| 5250 | 49 | 470 | | 110 | | 30 | | | |
| | 50 | | 30 | | 30 | | | 30 | 20 |
| | 51 | | | | | | | | |
| | 52 | | | | | | | | |
| | 53 | | | | | | | | |
| | 54 | 70 | | 0 | | | 50 | | |
| | 55 | | 10 | | 0 | | | 30 | 30 |
| | 56 | | 0 | 0 | 0 | | | | |
| 0 | 57 | | | | | | | | |
| | 58 | | | | | | | | |
| | 59 | 140 | | 0 | | 40 | | | |
| | 60 | | 60 | | 0 | | 40 | 20 | |
| | 61 | 180 | 100 | 50 | 10 | 20 | | | |
| | 62 | | 50 | 80 | 10 | | 30 | 20 | |
| | 63 | 730 | 290 | 150 | 30 | 20 | | | |
| | 64 | | 100 | 230 | 90 | | 30 | 30 | |
| | 65 | 1910 | 460 | 330 | 150 | 40 | | | |
| | 66 | | 770 | 560 | 210 | | 20 | 30 | |
| | 67 | 2210 | 340 | 720 | 300 | 100 | | | |
| | 68 | | 1110 | 900 | 410 | | 30 | 20 | |
| 5250 | 69 | 2510 | 910 | | 560 | 290 | | | |
| | 70 | | 660 | 890 | 620 | | 100 | | |
| | 71 | | | 680 | 470 | 490 | | | |
| | 72 | | 250 | 420 | 350 | | 340 | 240 | |
| | 73 | 530 | 140 | 250 | 260 | 370 | | | |
| | 74 | | 120 | 150 | 240 | | 360 | 360 | |
| | 75 | 360 | 50 | 110 | 200 | 330 | | | |
| | 76 | | 30 | 90 | 70 | | | | |

(Continued)

(Sheet 2 of 3)

Table 10 (Concluded)

| <u>Flow cfs</u> | <u>Cycles After Stability</u> | <u>Salinity, ppm</u> | | | | | |
|---------------------|---------------------------------------|----------------------|------------|------------|------------|------------|------------|
| | | <u>Tee</u> | <u>43C</u> | <u>BRC</u> | <u>BR1</u> | <u>BR2</u> | <u>BR3</u> |
| 0 | 77 | 200 | 30 | 50 | 50 | 300 | 360 |
| | 78 | | 70 | 50 | 70 | | 360 |
| | 79 | 260 | 120 | 70 | 70 | 240 | 360 |
| | 80 | | 70 | 110 | 60 | | 350 |
| | 81 | | 150 | 130 | 70 | 180 | |
| | 82 | | 220 | 160 | 80 | | 290 |
| 5250 | 83 | 540 | 200 | 200 | 230 | 150 | |
| | 84 | | 120 | 180 | 120 | | 310 |
| | 85 | 390 | 60 | 140 | 80 | 140 | |
| | 86 | | | 70 | 60 | | 270 |
| | 87 | 20 | 30 | 50 | 40 | 130 | |
| | 88 | | 20 | 30 | 20 | | 210 |
| | 89 | 50 | 0 | 20 | 20 | 130 | |
| | 90 | | 0 | 10 | 10 | | 200 |
| | 0 | 91 | 80 | 10 | 0 | 110 | |
| | | 92 | | 10 | 0 | | 180 |
| | | 93 | 70 | 20 | 10 | 110 | |
| | | 94 | | 20 | 30 | | 180 |
| | | 95 | 590 | 30 | 30 | 10 | |
| | | 96 | | 50 | 60 | 20 | 140 |
| | | | | | | | 260 |

Table 11
High-Water Slack Bottom Salinities (ppm) at Selected
Locations for Pinopolis Release Schedule E, Test 6

| Flow cfs | Cycles After Stability | Salinity, ppm | | | | | |
|----------------|------------------------------|---------------|-----|-----|-----|-----|-----|
| | | Tee | 43C | BRC | BR1 | BR2 | BR3 |
| 0 | 1 | 40 | 10 | | | | |
| | 2 | | | 0 | 0 | 10 | 0 |
| | 3 | 170 | 0 | | | | |
| | 4 | | | 0 | 10 | 0 | 20 |
| | 5 | 120 | 20 | | | | 10 |
| 28,500 3 hr | 6 | | | 10 | 30 | 10 | 0 |
| 5250 | 7 | 40 | 40 | | | | |
| | 8 | . | | 10 | 10 | 0 | 0 |
| | 9 | 30 | 60 | | | | |
| | 10 | | | 0 | 0 | 10 | 30 |
| | 11 | 20 | 10 | | | | |
| | 12 | | | 10 | 0 | 10 | |
| | 13 | 0 | 0 | 0 | 0 | 10 | 20 |
| | 14 | 30 | 0 | 0 | 0 | 0 | 0 |
| 0 | 15 | | | | | | |
| | 16 | 0 | 0 | 0 | | | |
| | 17 | | | | 0 | 0 | |
| | 18 | | | | | | |
| | 19 | | | 10 | 0 | 10 | 10 |
| 28,500 3 hr | 20 | 320 | | | | | |
| 5250 | 21 | | | | | | |
| | 22 | | | | | | |
| | 23 | 40 | 30 | | | | |
| | 24 | | | 0 | 0 | 0 | |
| | 25 | | | | | | |
| | 26 | | | 0 | 20 | 10 | 20 |
| | 27 | | | 0 | 20 | 0 | 20 |
| | 28 | 0 | 0 | | | | |
| 0 | 29 | | | | | | |
| | 30 | 40 | 0 | | | | |
| | 31 | | | 0 | | | |
| | 32 | | | | 0 | 0 | |
| | 33 | | | 0 | 0 | 0 | 20 |

(Continued)

Table 11 (Concluded)

| <u>Flow cfs</u> | <u>Cycles After Stability</u> | <u>Tee</u> | <u>43C</u> | <u>BRC</u> | <u>Salinity, ppm</u> | <u>BR1</u> | <u>BR2</u> | <u>BR3</u> | <u>BR4</u> |
|---------------------|---------------------------------------|------------|------------|------------|----------------------|------------|------------|------------|------------|
| 28,500 3 hr | 34 | 170 | 30 | | | | | | |
| 5250 | 35 | | | | | | | | |
| | 36 | | | | | | | | |
| | 37 | 10 | 0 | | | | | | |
| | 38 | | | 0 | 10 | 0 | | | |
| | 39 | | | | | | | | |
| | 40 | | | | | | | | |
| | 41 | | | 0 | 0 | 0 | 0 | 20 | 30 |
| | 42 | 0 | 0 | | | | | | |
| 0 | 43 | | | | | | | | |
| | 44 | 10 | 0 | | | | | | |
| | 45 | | | 0 | 10 | 0 | | | |
| | 46 | | | | | | | | |
| | 47 | | | 0 | 0 | 10 | 10 | 10 | 10 |
| 28,500 3 hr | 48 | 250 | 10 | | | | | | |
| 5250 | 49 | | | | | | | | |
| | 50 | | | | | | | | |
| | 51 | 20 | 0 | | | | | | |
| | 52 | | | 0 | 0 | 0 | | | |
| | 53 | | | | | | | | |
| | 54 | | | | | | | | |
| | 55 | | | 0 | 0 | 0 | 20 | 10 | |
| | 56 | 0 | 0 | | | | | | |
| 0 | 57 | | | | | | | | |
| | 58 | 0 | 10 | | 0 | | | | |
| | 59 | 20 | 10 | | 0 | 0 | 20 | 20 | |
| | 60 | | | | 0 | 0 | 0 | 10 | 20 |
| | 61 | | | | 0 | 0 | 0 | 40 | |
| | 62 | 150 | 30 | | 0 | 0 | | | |
| | 63 | | | | 0 | 0 | | | |
| | 64 | 670 | 140 | | 10 | | | | |
| | 65 | 170 | | 170 | 30 | 0 | 0 | 70 | |
| | 66 | 1010 | 330 | | 70 | | | | |
| | 67 | | | 620 | 130 | 0 | 0 | 20 | |
| | 68 | 1610 | 620 | | 210 | | | | |
| | 69 | | | 740 | 280 | 40 | 0 | 10 | |
| | 70 | 2110 | 1410 | | 390 | | | | |
| | 71 | | | 1310 | 470 | 160 | 0 | 0 | |
| | 72 | 2510 | 1510 | | 590 | | | | |
| | 73 | | | 1110 | 680 | 340 | 0 | 100 | |
| | 74 | | | | 790 | | | | |

Table 12
High-Water Slack Bottom Salinities (ppm) at Selected
Locations for Pinopolis Release Schedule E, Test 6R

| Flow cfs | Cycles After Stability | Salinity, ppm | | | | | | |
|----------------|------------------------------|---------------|-----|-----|-----|-----|-----|-----|
| | | Tee | 43C | BRC | BR1 | BR2 | BR3 | BR4 |
| 0 | 1 | 0 | 0 | | | | | |
| | 2 | | | 0 | 0 | 10 | 10 | 10 |
| | 3 | 20 | 0 | | | | | |
| | 4 | | | 0 | 0 | 10 | 10 | 10 |
| | 5 | 80 | 20 | | | | | |
| 28,500 3 hr | 6 | | | 20 | 0 | 0 | 10 | 0 |
| | 7 | 50 | 10 | | | | | |
| | 8 | | | 10 | 10 | 10 | 10 | 0 |
| | 9 | 80 | 20 | | | | | |
| | 10 | | | 0 | 10 | | 10 | 10 |
| 5250 | 11 | 20 | 0 | | | | | |
| | 12 | | | 0 | 0 | 10 | | |
| | 13 | 10 | 0 | | | 10 | 10 | 0 |
| | 14 | 10 | 0 | 10 | 0 | 10 | | |
| | 15 | | | | | | | |
| 0 | 16 | 10 | 0 | | | | | |
| | 17 | | | 0 | 0 | 10 | | |
| | 18 | | | | | | | |
| | 19 | | | 0 | 0 | 20 | 10 | 10 |
| | 20 | 140 | 30 | | | | | |
| 28,500 3 hr | 21 | | | | | | | |
| | 22 | | | | | | | |
| | 23 | 20 | 0 | | | | | |
| | 24 | | | 0 | 0 | 10 | | |
| | 25 | | | | | | | |
| 5250 | 26 | | | | | | | |
| | 27 | | | 0 | 0 | 10 | 10 | 20 |
| | 28 | 10 | 0 | | | | | |
| | 29 | | | | | | | |
| | 30 | 10 | 20 | | | | | |
| 0 | 31 | | | 0 | 0 | 10 | | |
| | 32 | | | | | | | |
| | 33 | | | 0 | 0 | 10 | 10 | 10 |

(Continued)

Table 12 (Concluded)

| Flow cfs | Cycles After <u>Stability</u> | <u>Tee</u> | Salinity, ppm | | | | |
|----------------|-------------------------------------|------------|---------------|------------|------------|------------|------------|
| | | | <u>43C</u> | <u>BRC</u> | <u>BR1</u> | <u>BR2</u> | <u>BR3</u> |
| 28,500 3 hr | 34 | 130 | 20 | | | | |
| 5250 | 35 | | | | | | |
| | 36 | | | | | | |
| | 37 | 30 | 0 | | | | |
| | 38 | | | 0 | 0 | 10 | |
| | 39 | | | | | | |
| | 40 | | | | | | |
| | 41 | | | 0 | 0 | 0 | 10 |
| | 42 | 0 | 0 | | | | 20 |
| 0 | 43 | | | | | | |
| | 44 | 10 | 0 | | | | |
| | 45 | | | 0 | 0 | 10 | |
| | 46 | | | | | | |
| | 47 | | | 0 | 0 | 0 | 10 |
| 28,500 3 hr | 48 | 220 | 80 | | | | |
| 5250 | 49 | | | | | | |
| | 50 | | | | | | |
| | 51 | 60 | 10 | | | | |
| | 52 | | | 30 | 0 | 10 | |
| | 53 | | | | | | |
| | 54 | | | | | | |
| | 55 | | | 0 | 0 | 10 | 10 |
| | 56 | 10 | 0 | | | | 10 |
| 0 | 57 | | | | | | |
| | 58 | 30 | 0 | | | | |
| | 59 | | | 0 | 0 | 10 | 10 |
| | 60 | 40 | 10 | | | | |
| | 61 | | | 0 | 0 | 10 | 20 |
| 28,500 3 hr | 62 | 160 | 30 | | | | |

Table 13
 High-Water Slack Bottom Salinities, ppm, at Selected Locations for Pinopolis Release Schedules C and E
 40-Ft Cooper River Navigation Channel to Mile 23.0

| Test No. | Freshwater Release Schedule | Avg Weekly Flow, cfs | Tee | Total Salt, ppm | | | | | | | | | | | | |
|----------|-----------------------------|----------------------|-----|-----------------|-----|-----|-----|------------|-----|-----|-----|--------------|-----|-----|-----|----|
| | | | | Cooper River | | | | Back River | | | | Foster Creek | | | | |
| | | | | Max | Min | Max | Min | Max | Min | Max | Min | Max | Min | Max | Min | |
| 1 | C-3000 | 480 | 45 | 180 | 50 | -- | -- | -- | 0 | 20 | 80 | 60 | -- | -- | -- | |
| 1R | C-3000 | 550 | 55 | 160 | 20 | 80 | 0 | 0 | 20 | 20 | 40 | 20 | 60 | 60 | 35 | |
| 2 | C-3000 | 540 | 70 | 140 | 20 | -- | -- | -- | 100 | 50 | -- | -- | -- | -- | -- | |
| 2R | C-3000 | 310 | 30 | 100 | 15 | 65 | 35 | 10 | 5 | 20 | 15 | -- | -- | -- | -- | |
| 3 | C-3000 | 300 | 30 | 90 | 0 | 50 | 10 | 20 | 0 | 20 | 0 | 20 | 20 | 30 | 20 | |
| 4 | C-3000 | 300 | 60 | 80 | 0 | -- | -- | -- | 40 | 20 | -- | -- | -- | -- | -- | |
| 5 | C-3000 | 460 | 20 | 70 | 0 | 50 | 0 | 10 | 0 | 40 | 20 | 30 | 25 | 30 | 20 | |
| Average | | | | 420 | 44 | 117 | 15 | 61 | 11 | 15 | 0 | 46 | 28 | 30 | 22 | 40 |
| 6 | E-3500 | 220 | 0 | 25 | 0 | 0 | 0 | 20 | 20 | 20 | 15 | 20 | 10 | 20 | 10 | |
| 6R | E-3500 | 160 | 10 | 40 | 0 | 0 | 0 | 0 | 0 | 10 | 10 | 10 | 10 | 20 | 10 | |
| Average | | | | 190 | 5 | 33 | 0 | 0 | 0 | 10 | 10 | 15 | 13 | 15 | 10 | 20 |

Note: Maximum salinity data obtained after zero flow period of hydrograph while minimum salinities were obtained after 5250-cfs flow period of hydrograph.

Table 14
High-Water Slack Bottom Salinities, ppm at Selected Locations for Zero Release
at Pinopolis, 40-Ft Cooper River Navigation Channel at Mile 23.0
Schedules C and E

| Cycles of Zero Flow | Test 1, Schedule C | | | | | | Total Salt, ppm | | | | | | Test 6, Schedule E | | | | | | | | | | | | |
|---------------------------|--------------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|--------------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|----|
| | 43 | | | BRC | | | 43 | | | BRC | | | 43 | | | BRC | | | 43 | | | BRC | | | |
| | BR _C | BR _L | BR _R | BR _C | BR _L | BR _R | BR _C | BR _L | BR _R | BR _C | BR _L | BR _R | BR _C | BR _L | BR _R | BR _C | BR _L | BR _R | BR _C | BR _L | BR _R | BR _C | BR _L | BR _R | |
| 0 | -- | -- | 40 | -- | -- | 0 | 0 | 20 | 50 | 0 | 0 | 0 | -- | -- | 0 | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- |
| 1 | -- | -- | 10 | -- | -- | 0 | 0 | -- | 70 | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- |
| 2 | -- | -- | 10 | -- | -- | 0 | 0 | 10 | 60 | -- | -- | -- | -- | -- | -- | -- | -- | -- | 0 | -- | -- | 0 | -- | -- | -- |
| 3 | -- | -- | 10 | -- | -- | 90 | 10 | 0 | -- | 70 | -- | 0 | -- | -- | 40 | -- | -- | -- | -- | 0 | -- | 0 | -- | -- | -- |
| 4 | -- | 110 | -- | -- | 90 | -- | 20 | 0 | 10 | 60 | -- | -- | -- | -- | -- | -- | -- | -- | 0 | -- | -- | 0 | -- | -- | -- |
| 5 | -- | -- | 40 | -- | -- | 50 | 10 | -- | 30 | 100 | 50 | 10 | 20 | -- | -- | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6 | -- | -- | 120 | -- | -- | 170 | 40 | -- | 70 | 50 | 80 | -- | 0 | -- | -- | 0 | -- | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7 | 230 | 50 | 140 | 150 | 260 | 180 | -- | 40 | 290 | 150 | 30 | 20 | -- | 0 | -- | 0 | -- | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8 | 340 | -- | 180 | -- | 370 | 200 | -- | 70 | 100 | 230 | -- | -- | 140 | -- | -- | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| 9 | -- | 110 | -- | 280 | 500 | 280 | -- | 60 | 460 | 330 | 150 | 40 | -- | 170 | -- | 10 | -- | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| 10 | 680 | -- | 250 | -- | 710 | 440 | -- | 60 | 770 | 560 | 210 | -- | 330 | -- | 70 | -- | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| 11 | -- | 220 | -- | 230 | 1120 | 700 | 330 | 50 | 340 | 720 | 300 | 100 | -- | 620 | -- | 130 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| 12 | 1120 | -- | 350 | -- | 1720 | 1020 | -- | 90 | 1110 | 900 | 410 | -- | 620 | -- | 210 | -- | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| 13 | -- | 440 | 540 | 480 | 2020 | 1320 | -- | 200 | -- | -- | -- | 1410 | -- | 740 | -- | 280 | 40 | -- | 0 | 0 | 0 | 0 | 0 | 0 | |
| 14 | 1620 | -- | 650 | -- | 2220 | 1820 | -- | 320 | -- | -- | -- | -- | -- | 1410 | -- | 390 | -- | -- | 0 | 0 | 0 | 0 | 0 | 0 | |
| 15 | -- | -- | 1190 | -- | 2520 | 2120 | -- | 450 | -- | -- | -- | 1310 | -- | 470 | -- | 160 | -- | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| 16 | -- | -- | -- | -- | 2720 | 2320 | -- | 610 | -- | -- | -- | 1510 | -- | 590 | -- | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| 17 | -- | -- | -- | -- | 2820 | 2520 | -- | 810 | -- | -- | -- | 1110 | -- | 680 | -- | 340 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| 18 | -- | 1120 | 1320 | 690 | 3120 | 2720 | -- | 1020 | -- | -- | -- | -- | -- | 790 | -- | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| 19 | 2720 | -- | 1340 | -- | 3320 | 3020 | 1720 | 1120 | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | |

Note: Five weeks (ending on Saturday) of Schedules C and E preceded zero flow. Cycle 7 is the first additional cycle of zero flow (both Schedules C and E started with 3 days of zero flow).

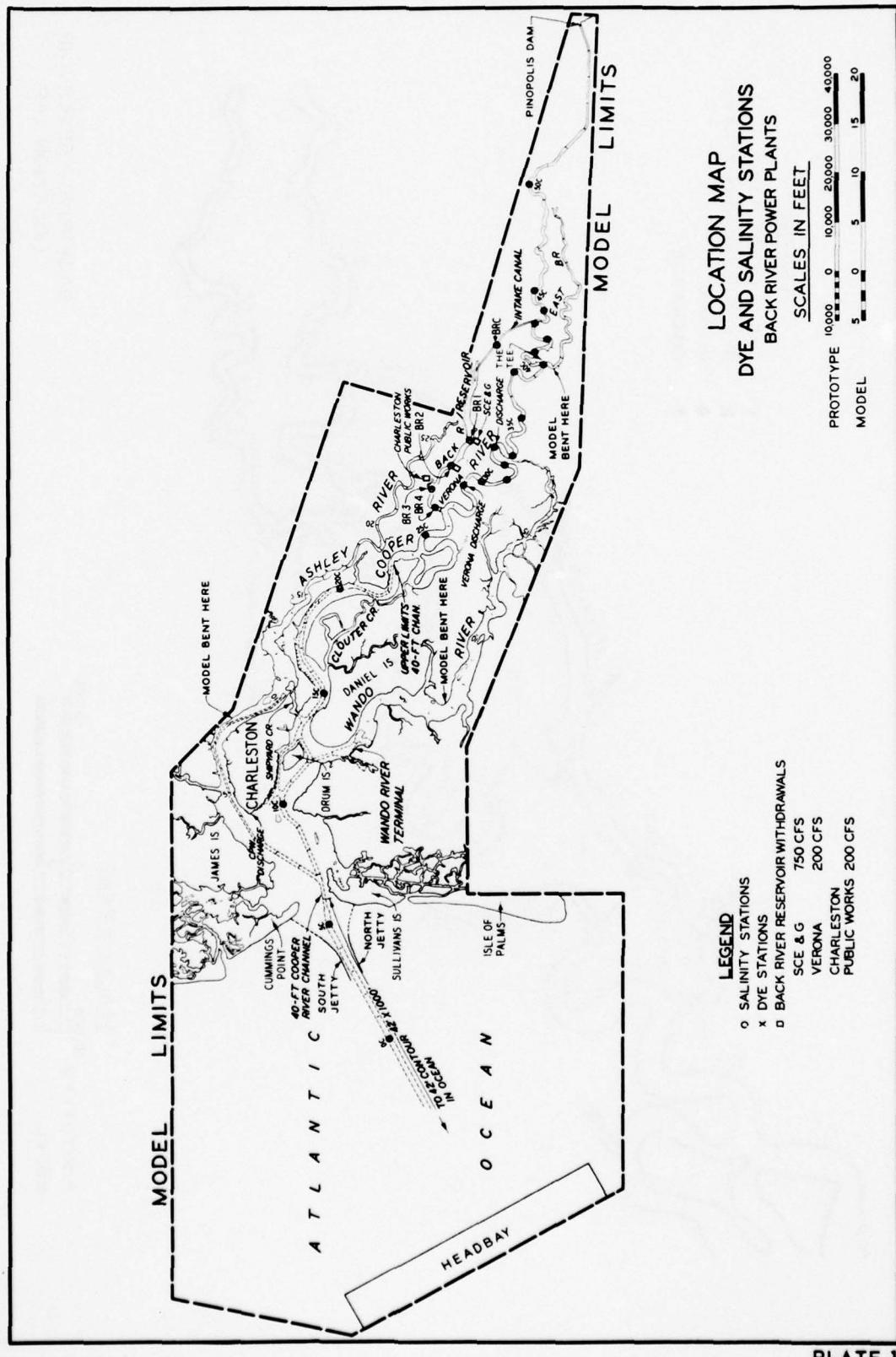
Table 15

High-Water Slack Bottom Salinities, ppm, at Selected Locations
for Zero and 1135-cfs Release at Pinopolis, 40-Ft Cooper

River Navigation Channel to Mile 23.0, Schedule C

| Cycles of Zero Flow | Test 1R | | | Test 3 | | | |
|---------------------------|-----------------|------|------|--------------------------|-----------------|-----|-----|
| | Total Salt, ppm | | | Cycles of 1135 cfs | Total Salt, ppm | | |
| | Mile 43 | BRC | BR2 | | Mile 43 | BRC | BR2 |
| 0 | 0 | 0 | 50 | 0 | 0 | 10 | 20 |
| 1 | 0 | 0 | 70 | 1 | 10 | 10 | 20 |
| 2 | 0 | 10 | 60 | 2 | 10 | 10 | 20 |
| 3 | 10 | 0 | 70 | 3 | 50 | 10 | 20 |
| 4 | 20 | 0 | 60 | 4 | 50 | 30 | 40 |
| 5 | 50 | 10 | 30 | 5 | 60 | 60 | 10 |
| 6 | 170 | 40 | 70 | 6 | 90 | 60 | 20 |
| 7 | 260 | 180 | 40 | 7 | 120 | 60 | 30 |
| 8 | 370 | 200 | 70 | 8 | 160 | 120 | 20 |
| 9 | 500 | 280 | 60 | 9 | 190 | 150 | 40 |
| 10 | 710 | 440 | 60 | 10 | -- | 170 | 30 |
| 11 | 1120 | 700 | 50 | 11 | 260 | 190 | 30 |
| 12 | 1720 | 1020 | 90 | 12 | 260 | 230 | 40 |
| 13 | 2020 | 1320 | 200 | 13 | 260 | 240 | 50 |
| 14 | 2220 | 1820 | 320 | 14 | 370 | 220 | 50 |
| 15 | 2520 | 2120 | 450 | 15 | 410 | 300 | 60 |
| 16 | 2720 | 2320 | 610 | 16 | 410 | 330 | 80 |
| 17 | 2820 | 2520 | 810 | 17 | 460 | 340 | 80 |
| 18 | 3120 | 2720 | 1020 | 18 | 500 | 360 | 90 |
| 19 | 3320 | 3020 | 1120 | 19 | 560 | 400 | -- |
| 20 | | | | 20 | 570 | 450 | 150 |

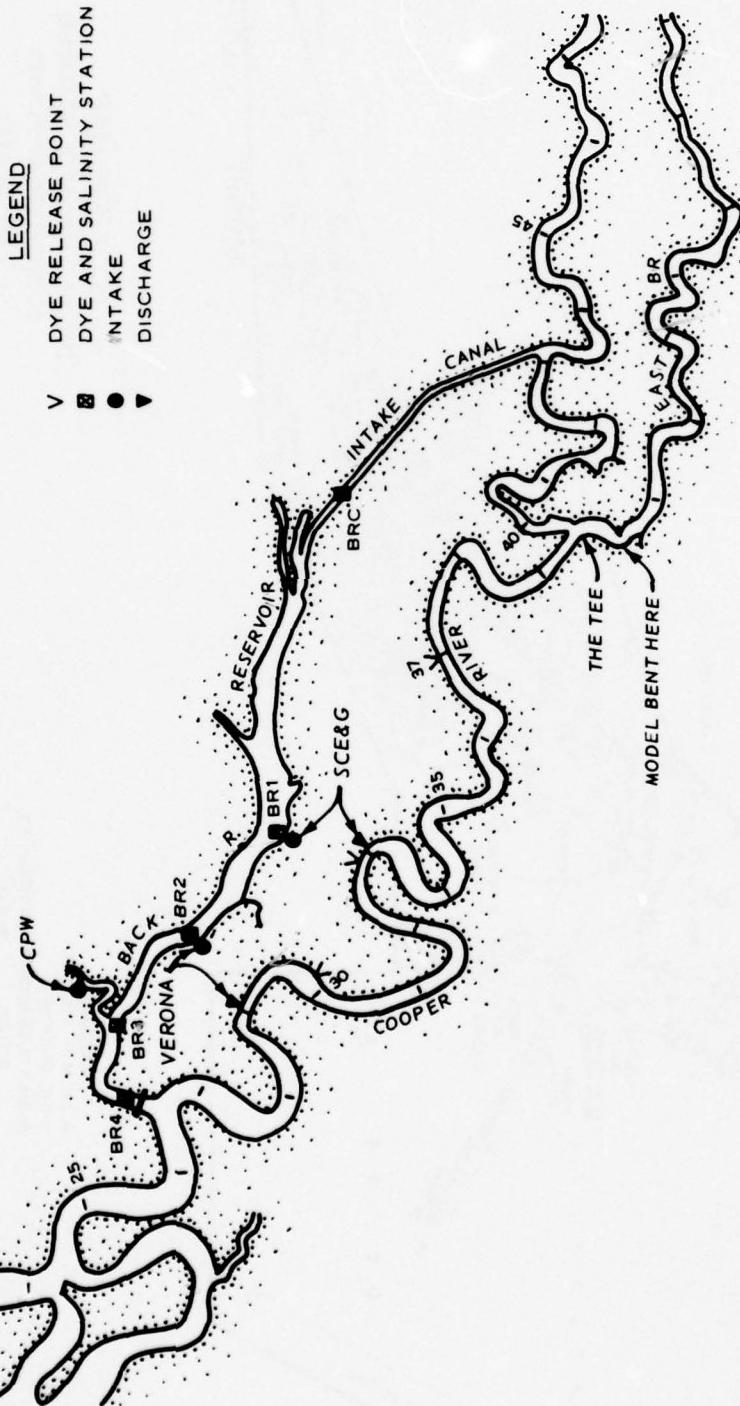
Note: Five weeks of Schedule C preceded 0-cfs release while 8 weeks of Schedule C preceded 1135-cfs release.



BACK RIVER RESERVOIR
LOCATION MAP

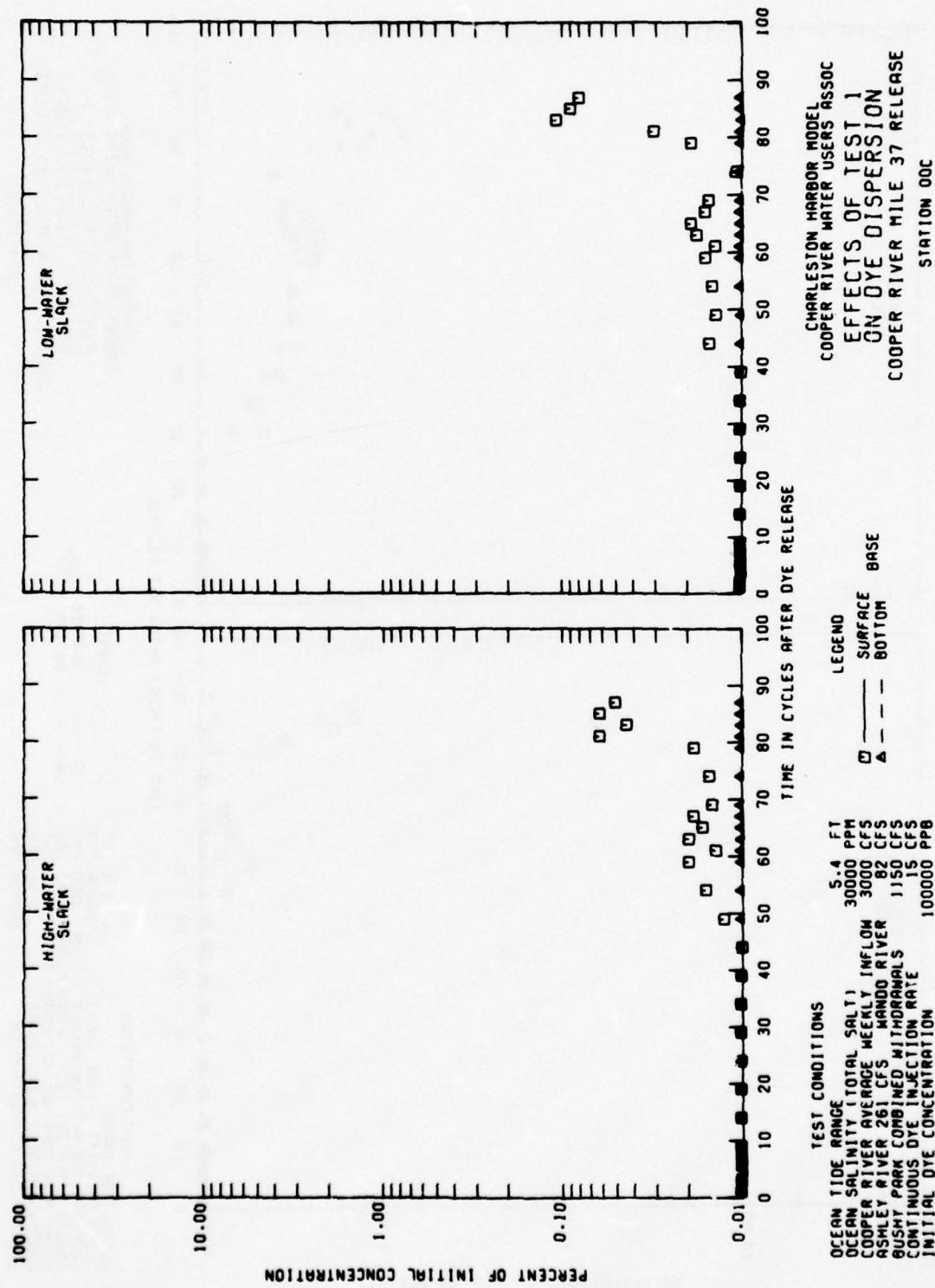
LEGEND

- ▼ DYE RELEASE POINT
- DYE AND SALINITY STATION
- INTAKE
- ▼ DISCHARGE



SCALES IN FEET

| | | |
|-----------|--------|---|
| PROTOTYPE | 10,000 | 0 |
| MODEL | 5 | 0 |



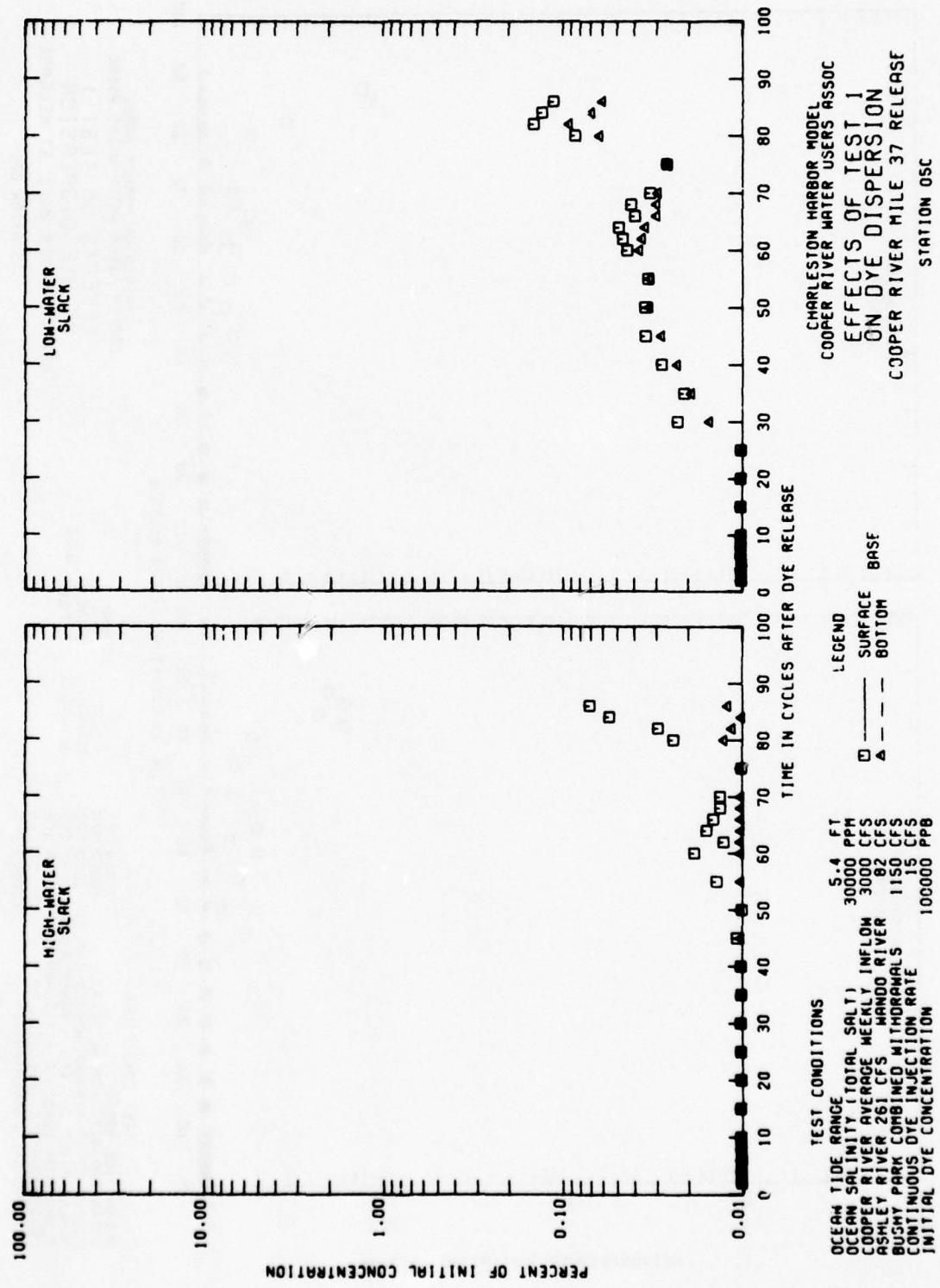
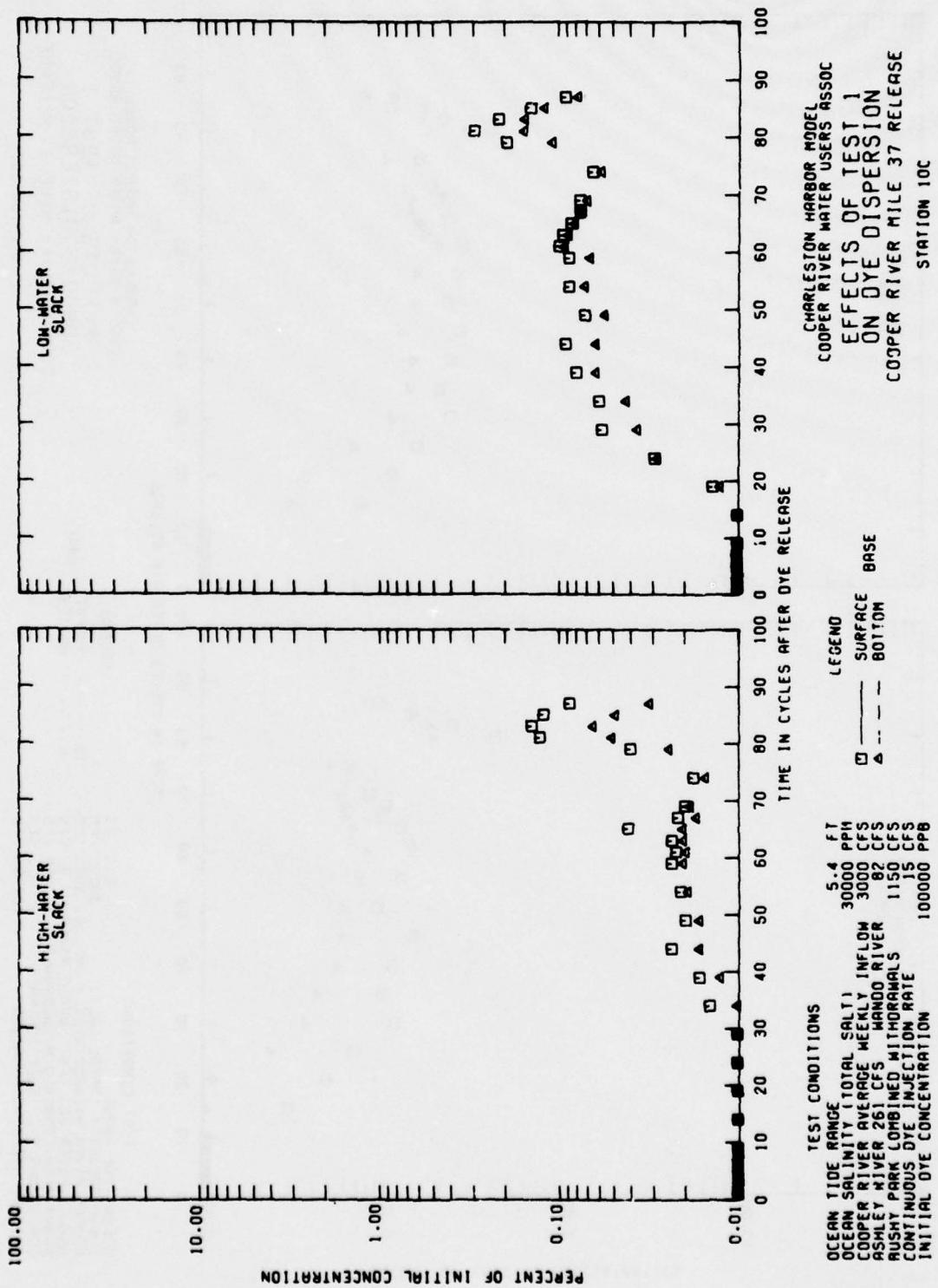


PLATE 4



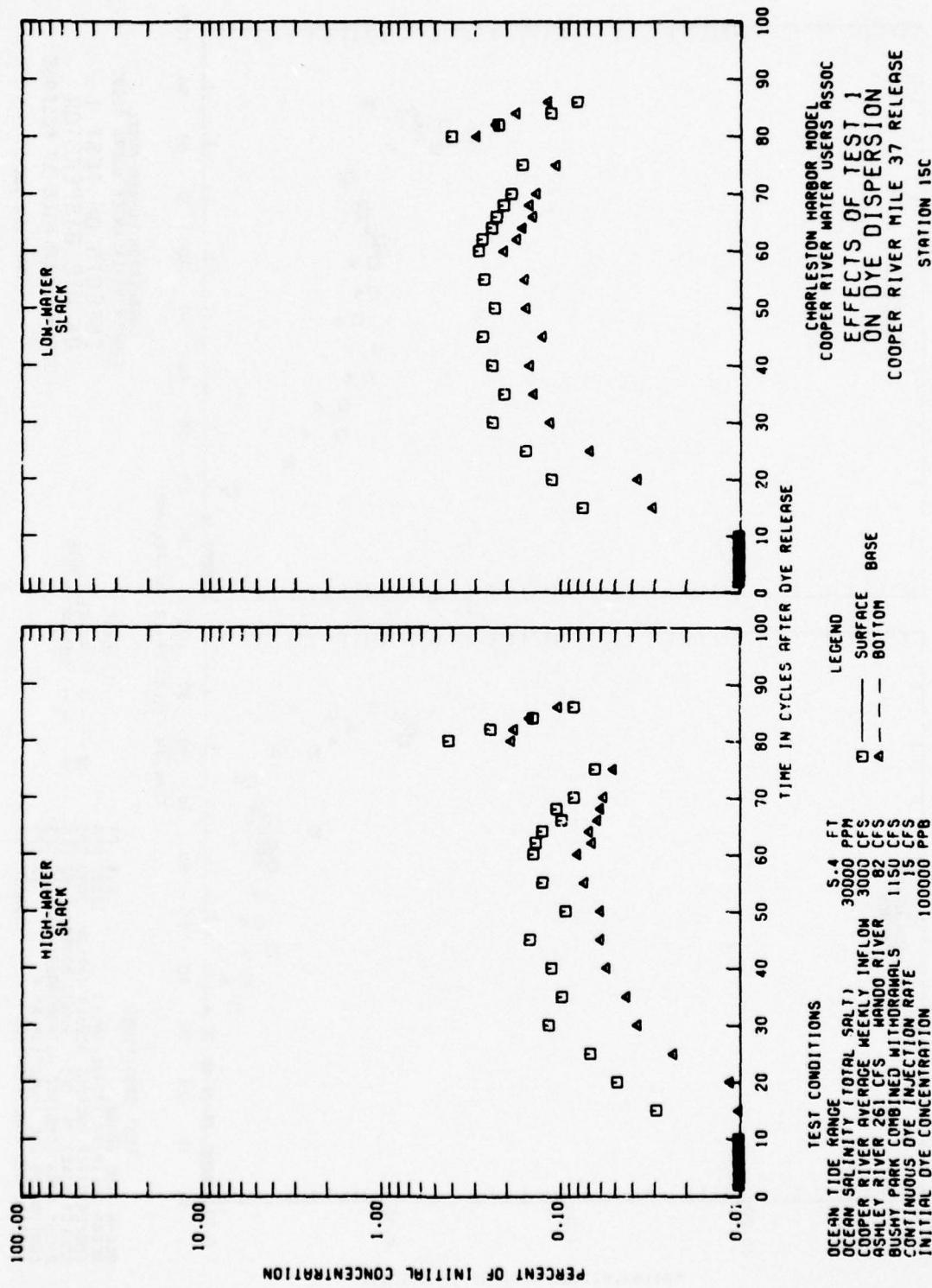
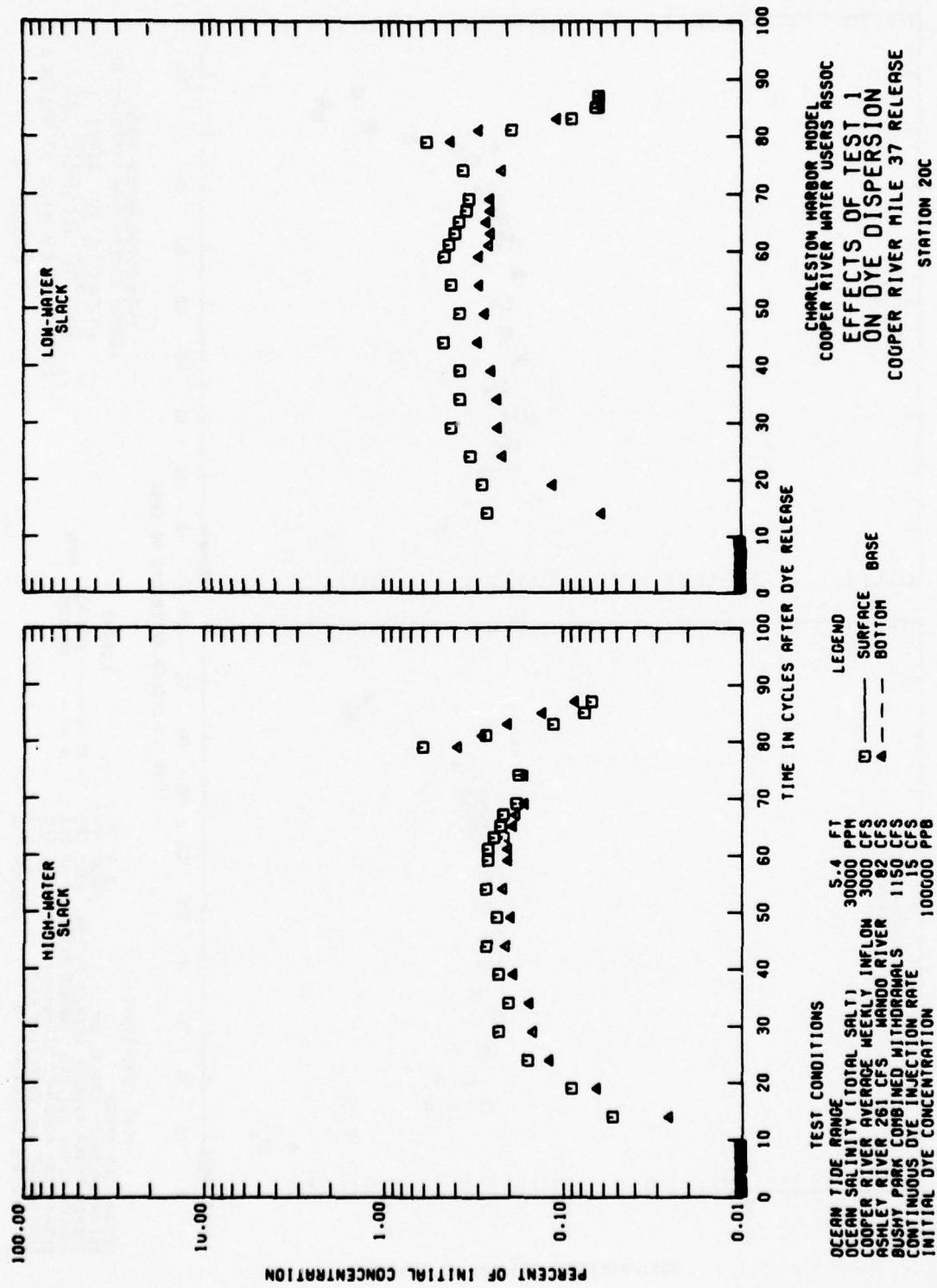


PLATE 6



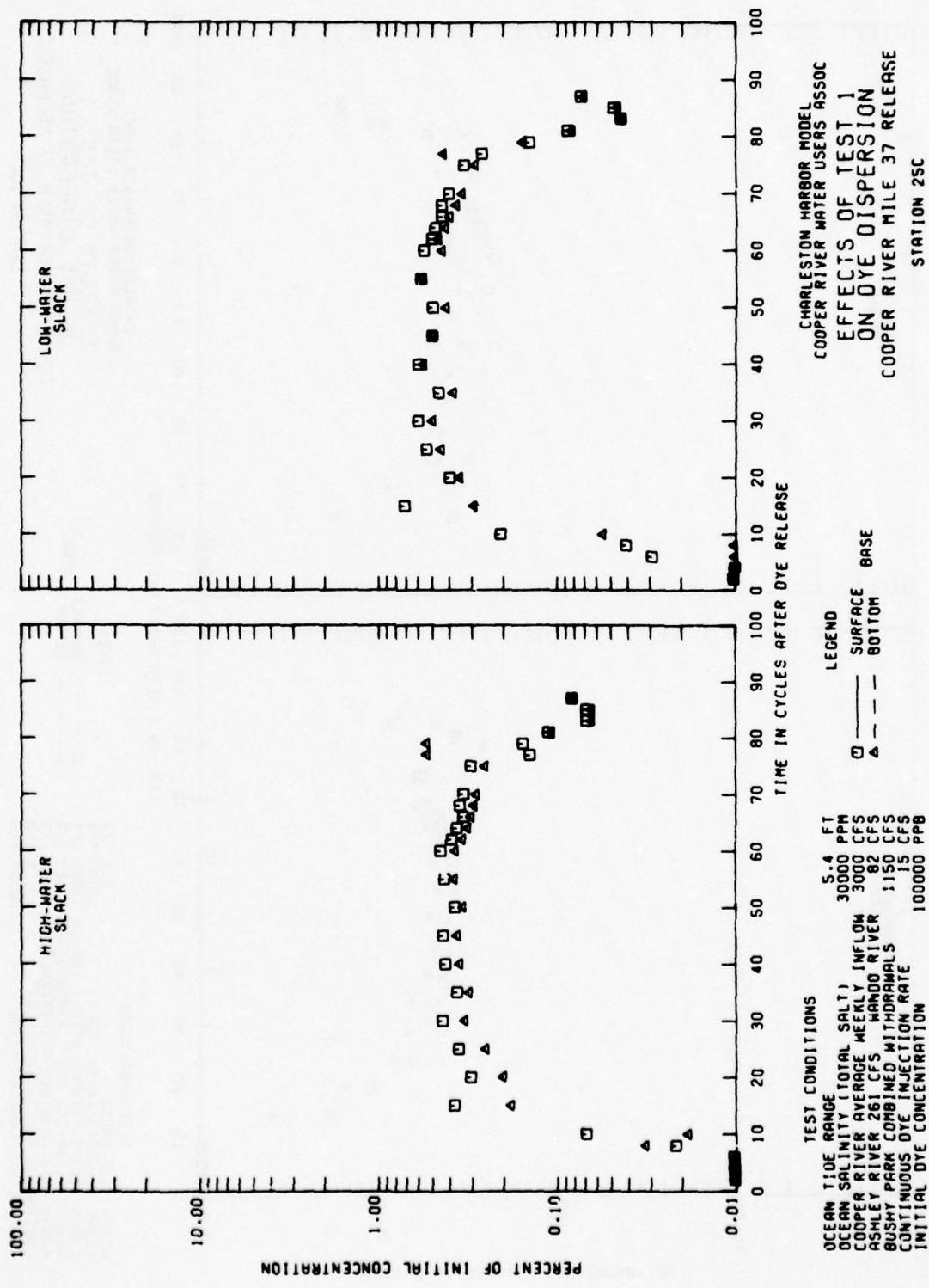
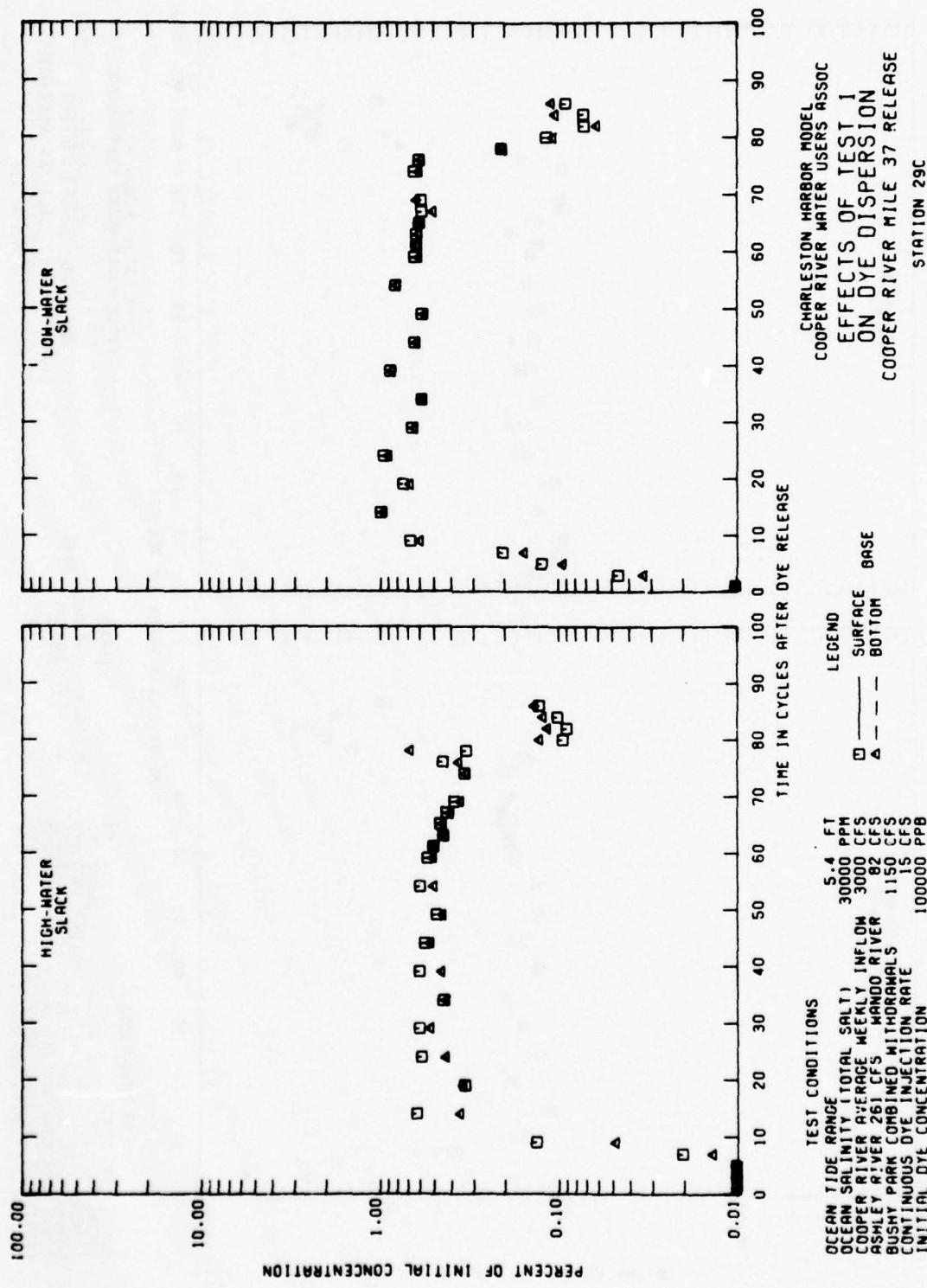
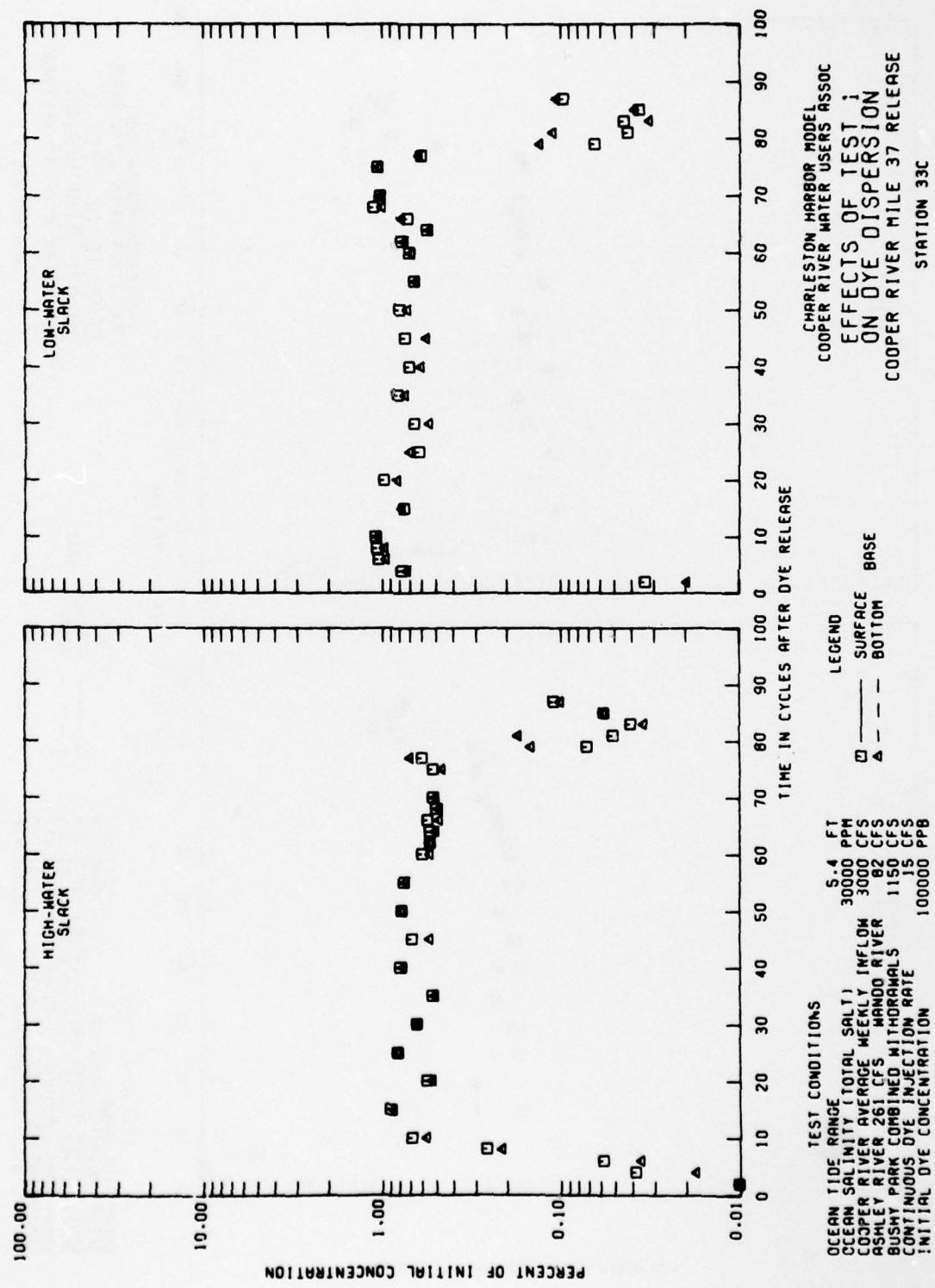
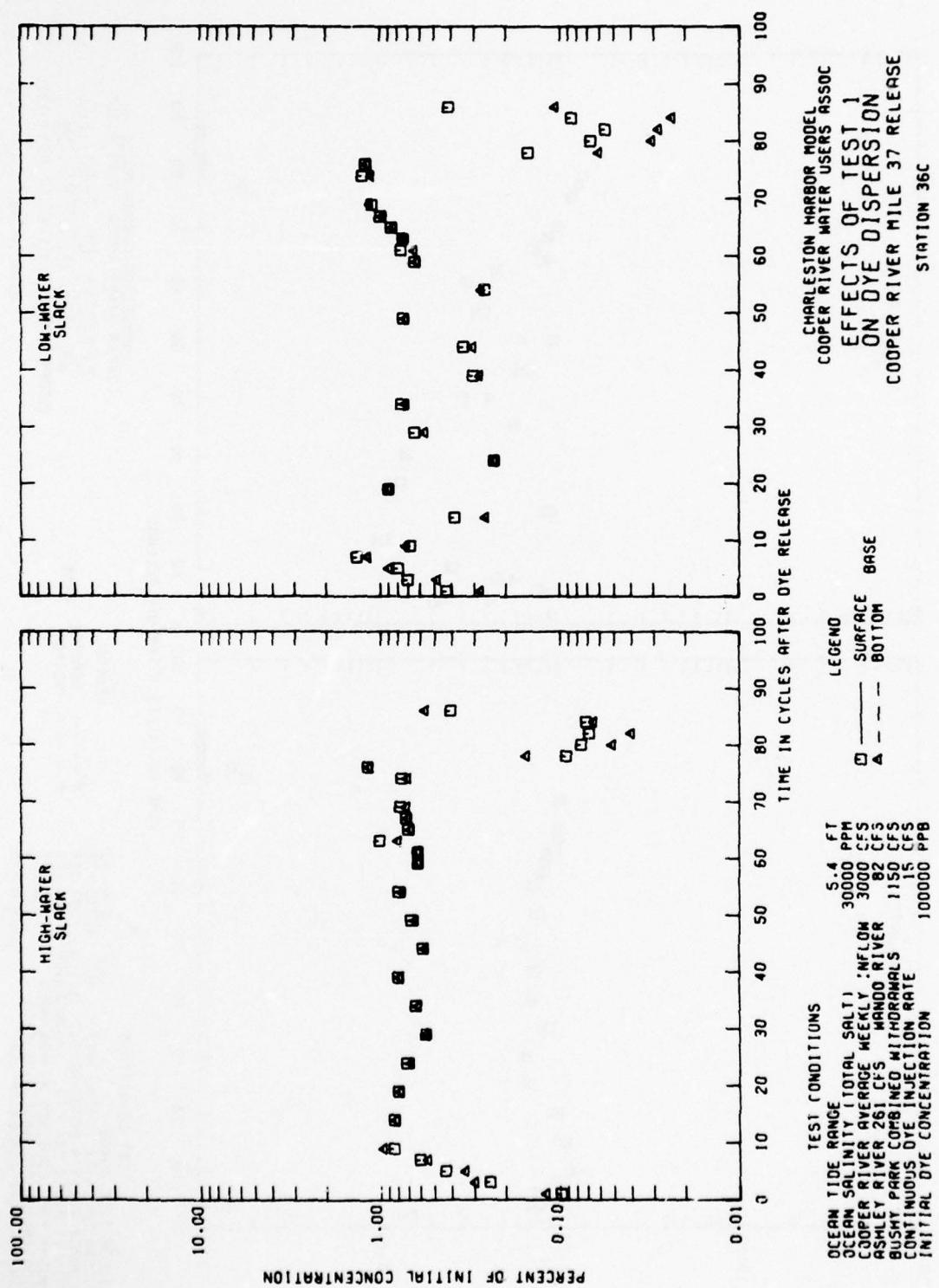
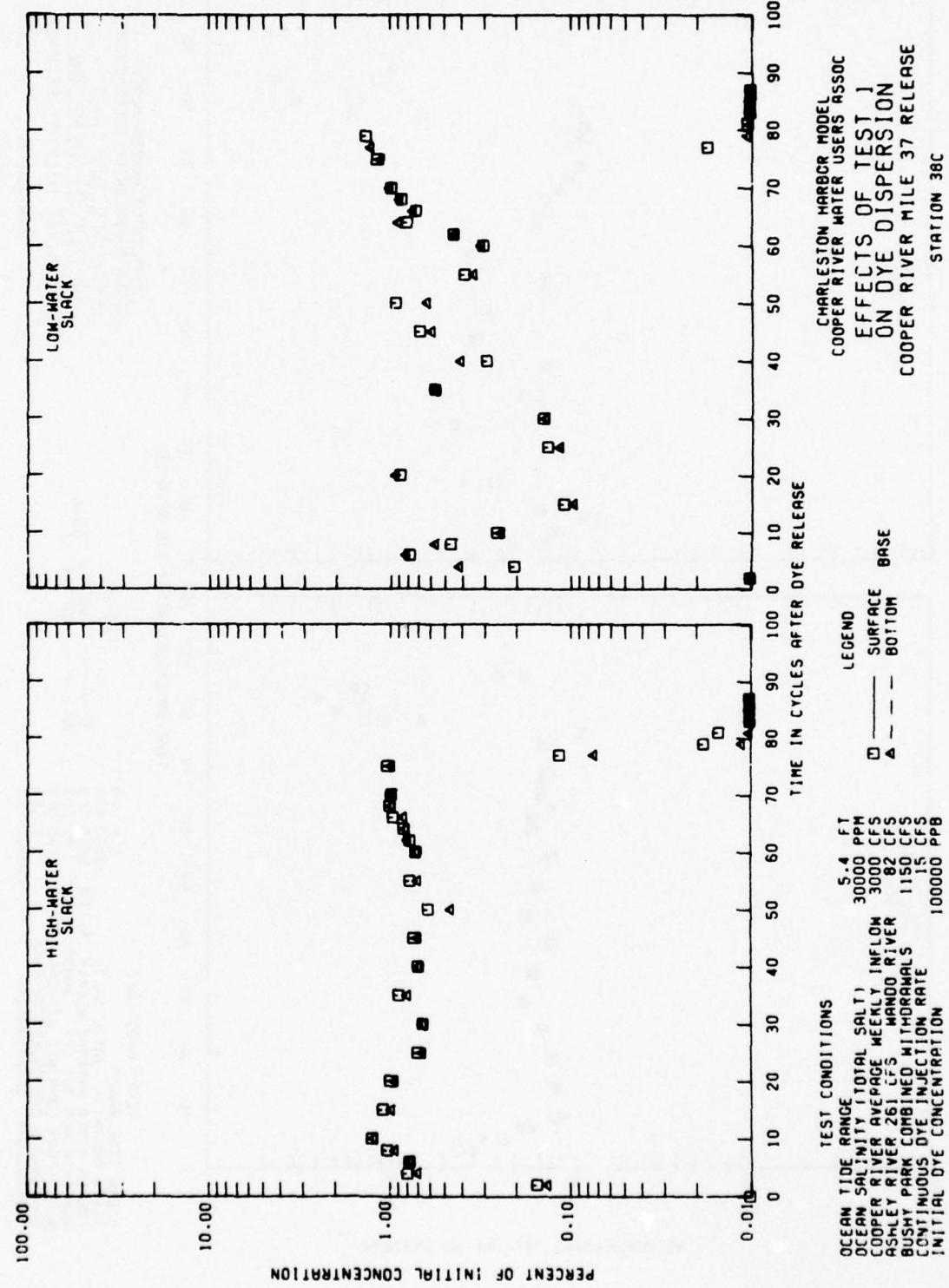


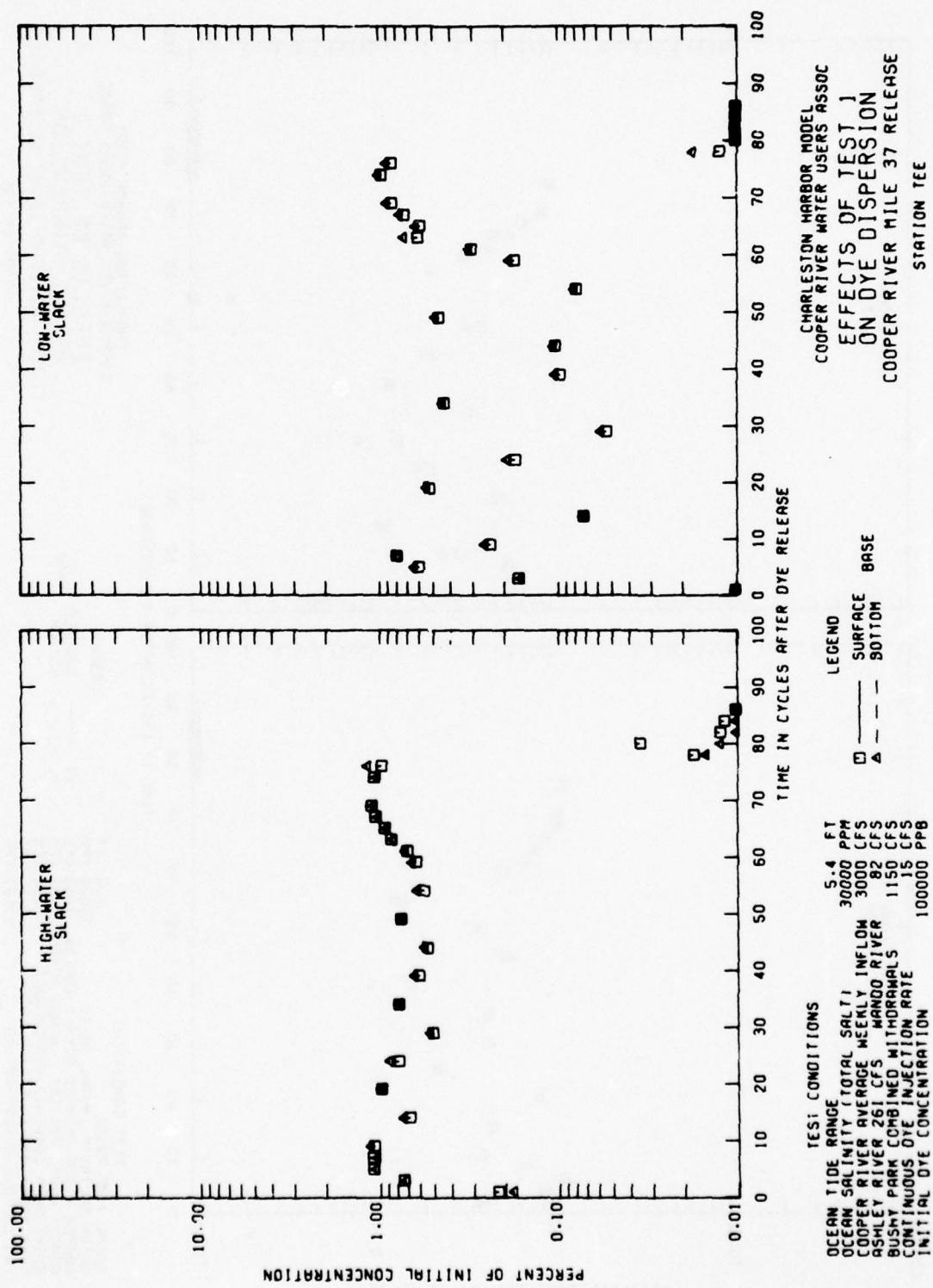
PLATE 8











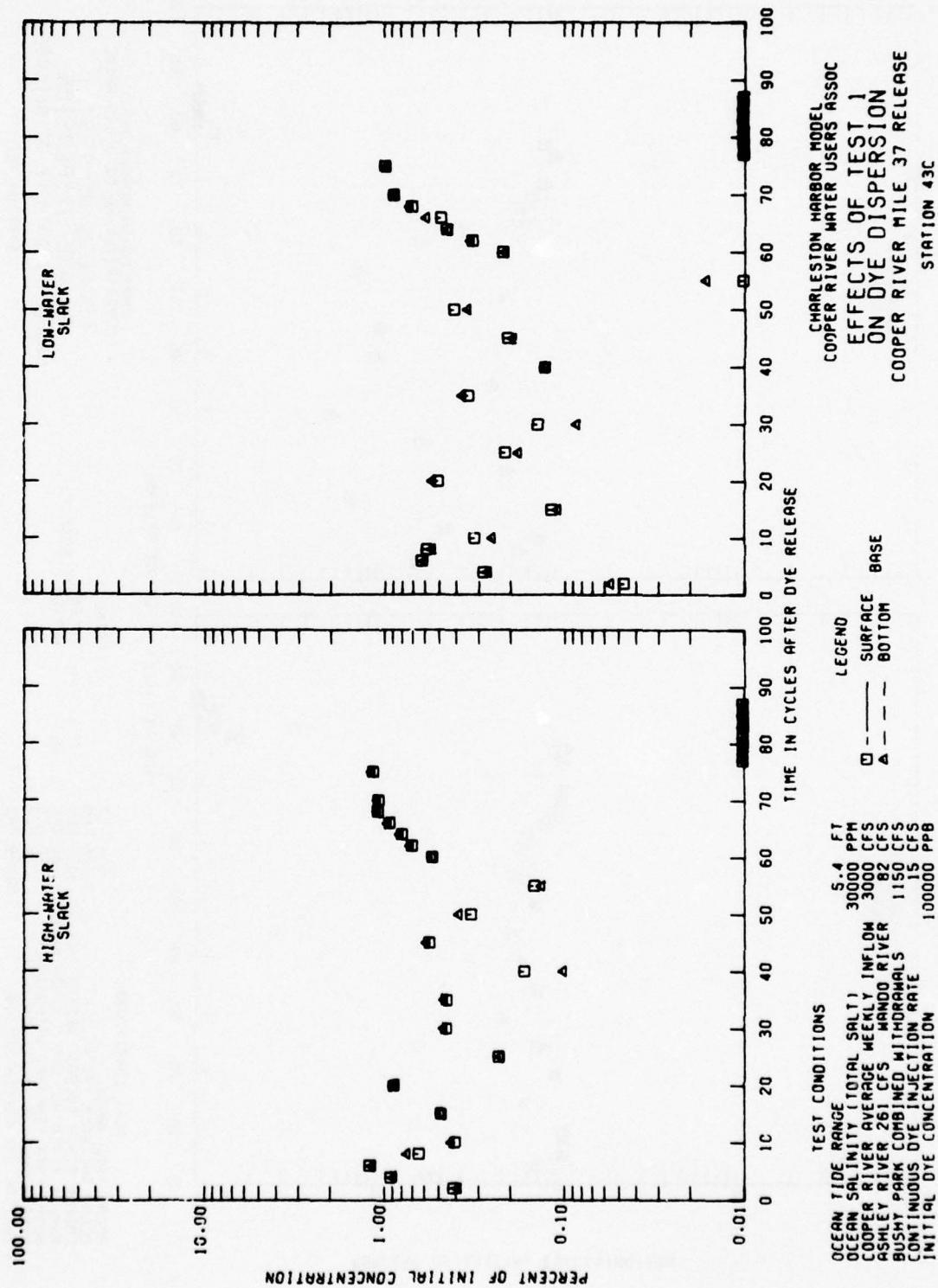
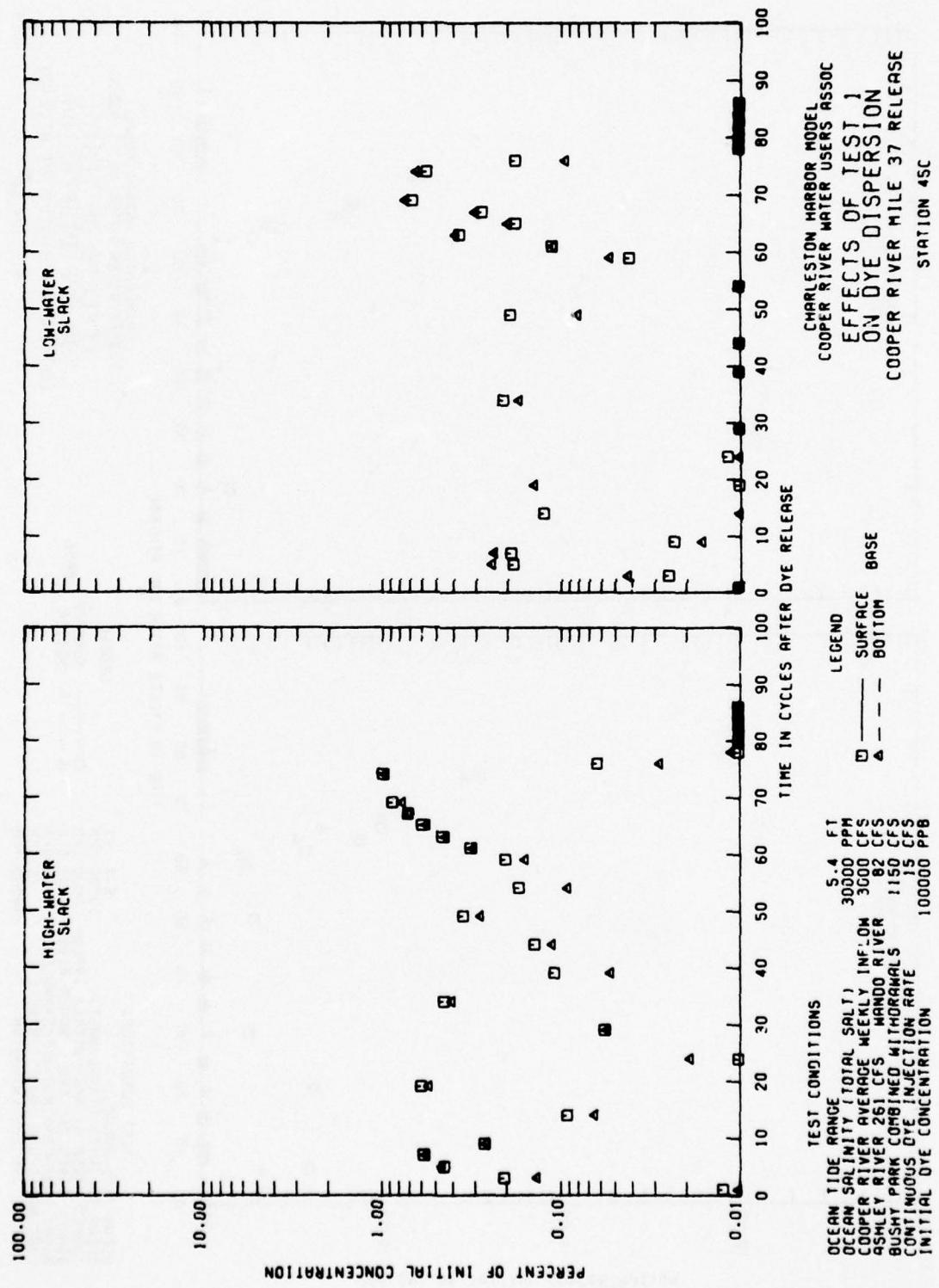


PLATE 14



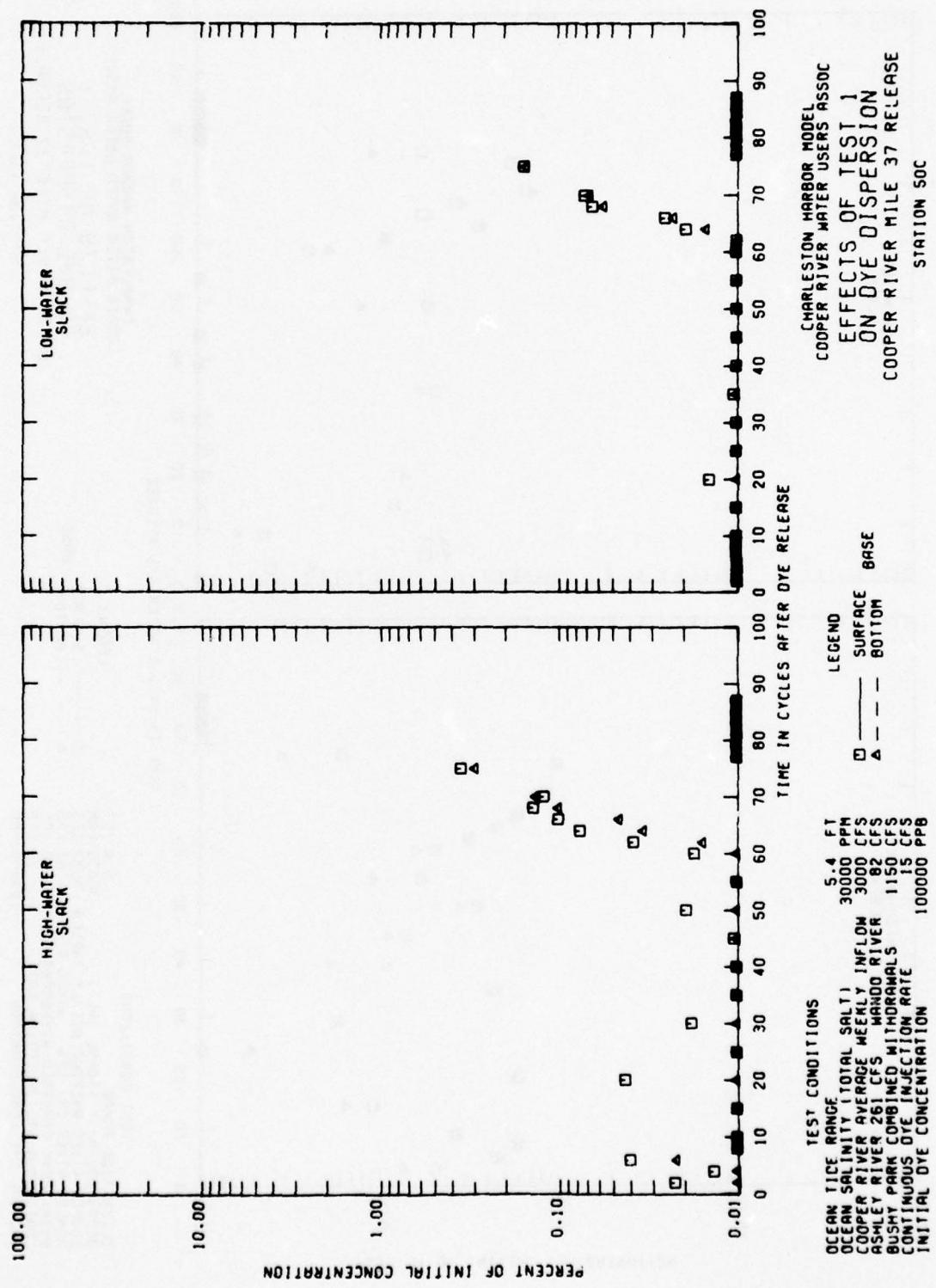
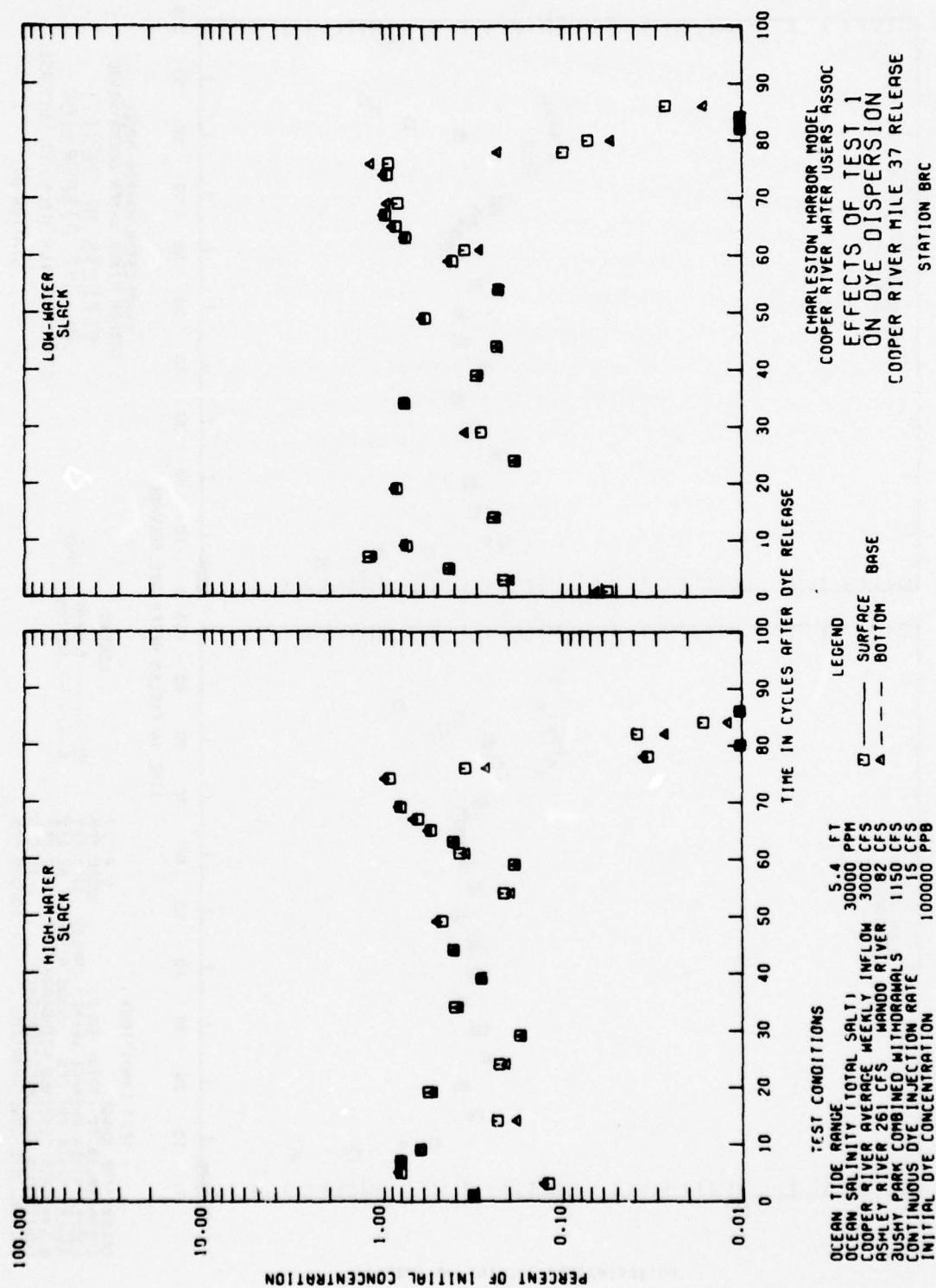


PLATE 16



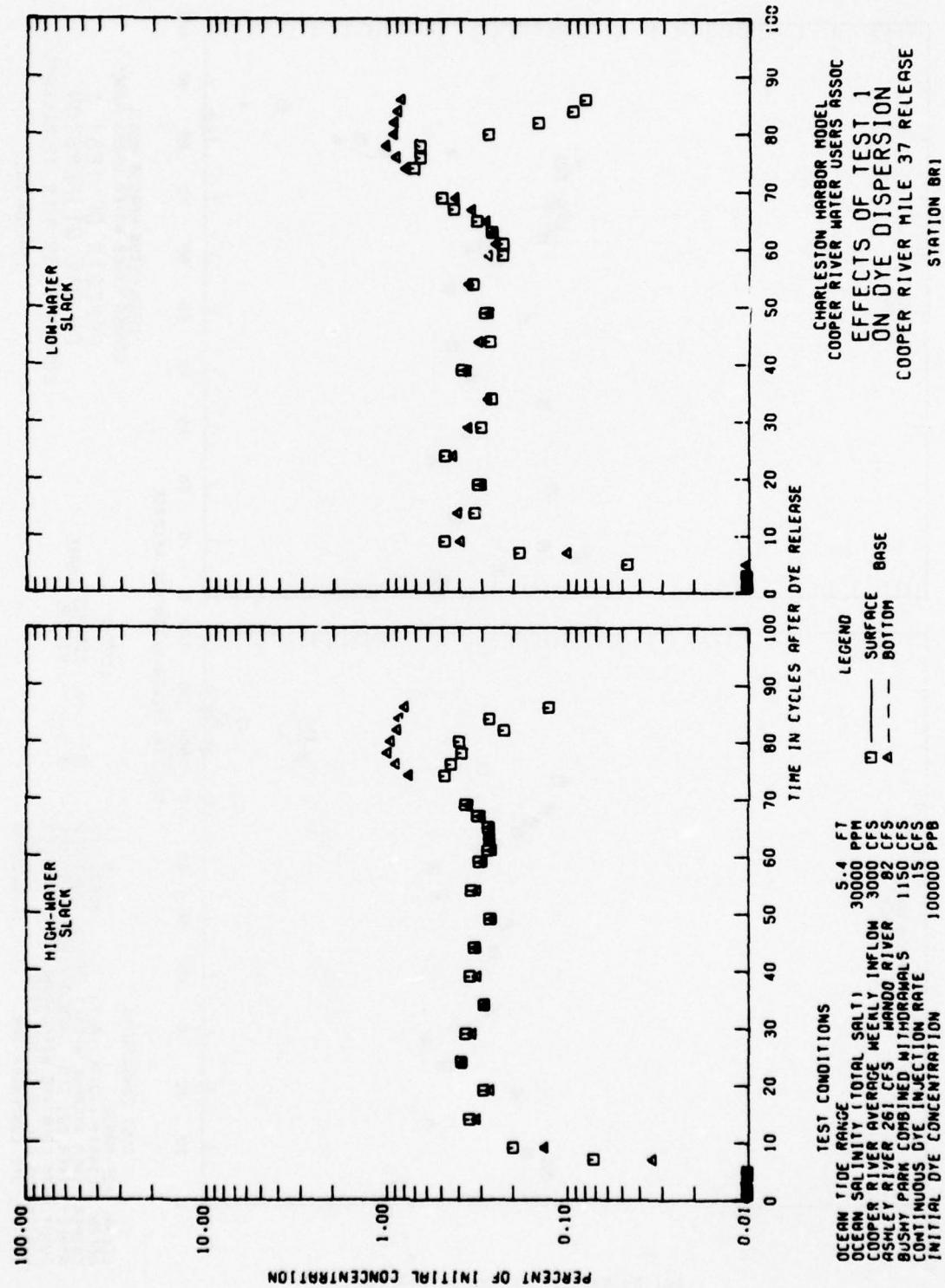
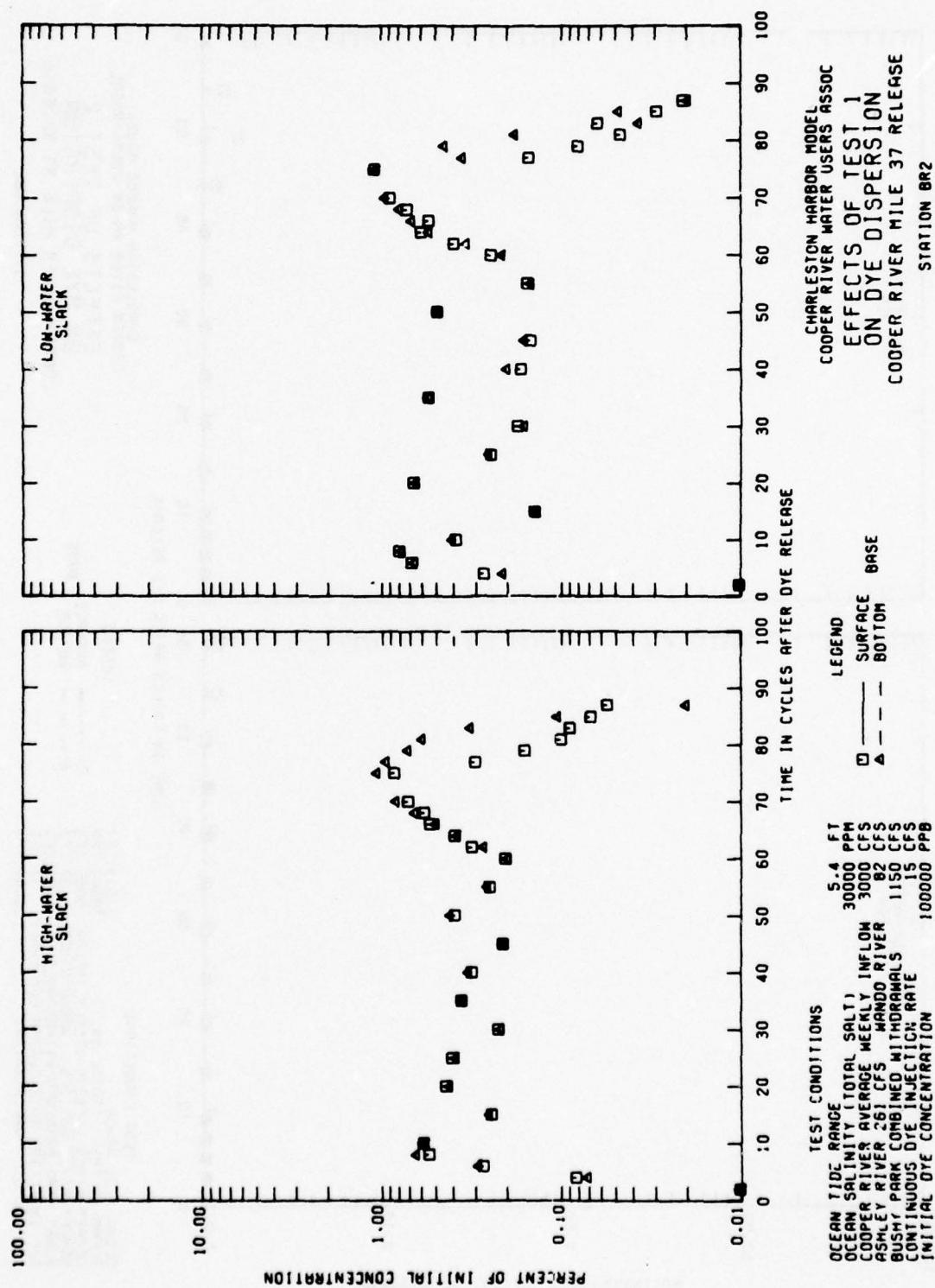
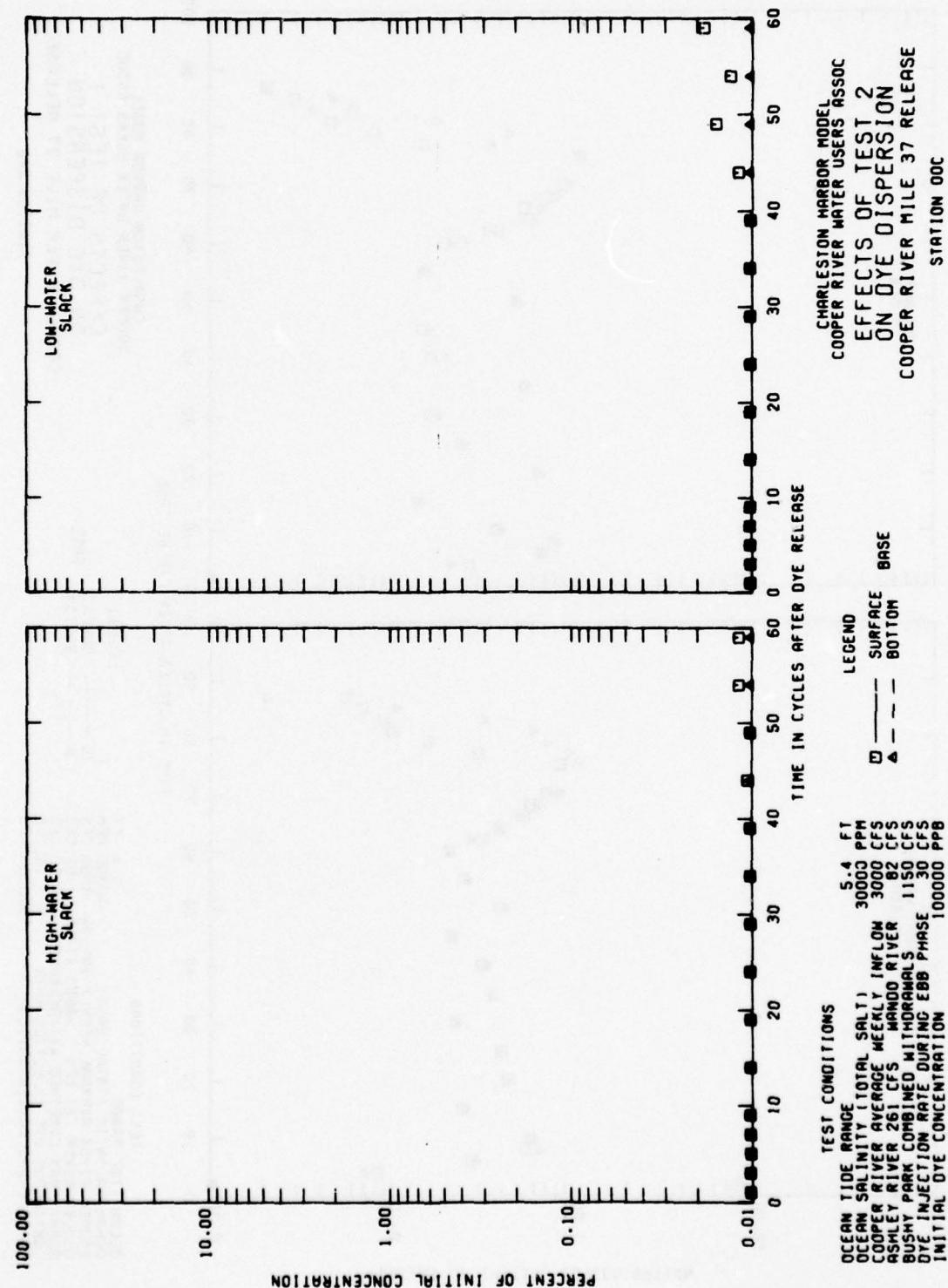
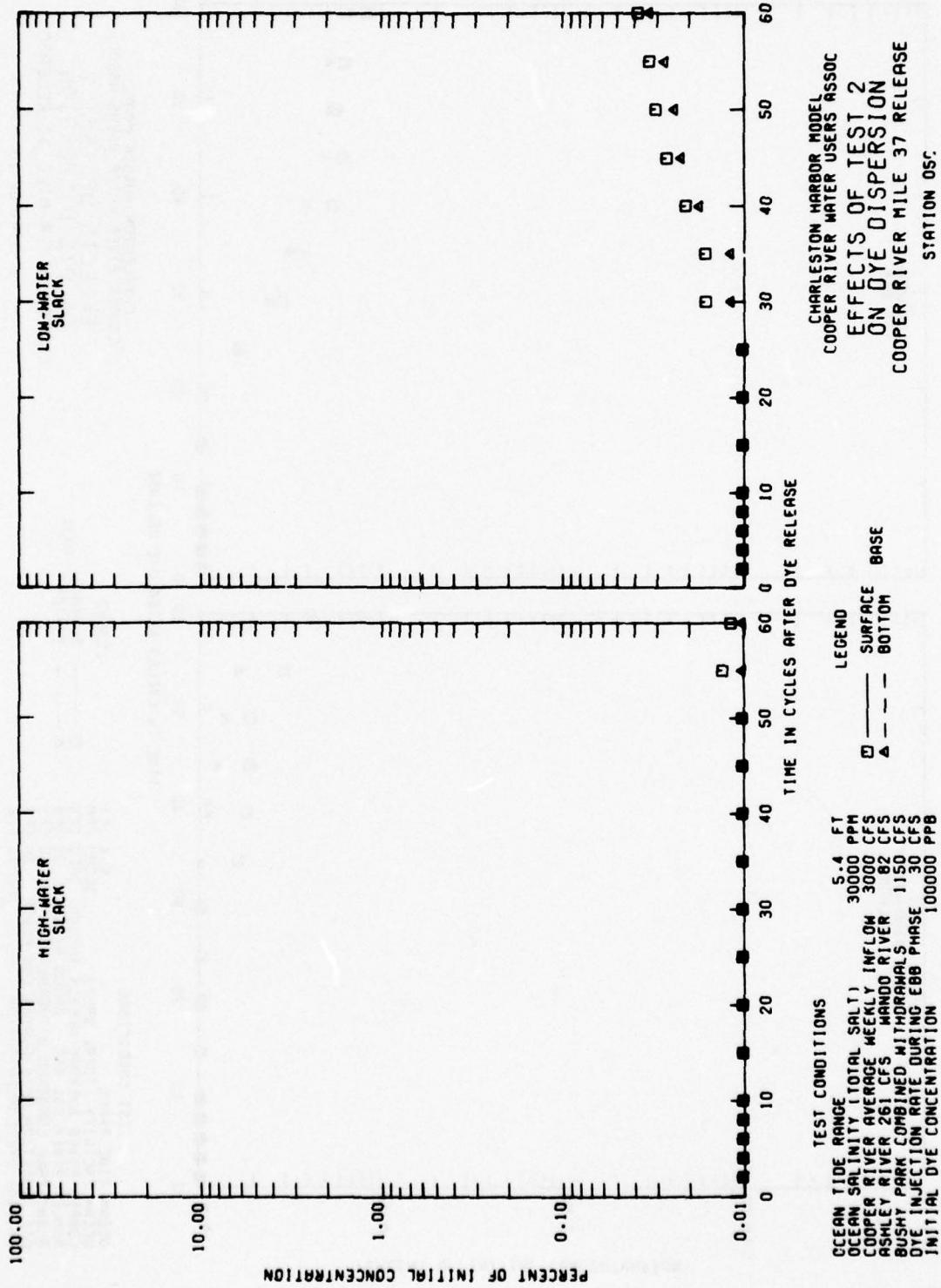
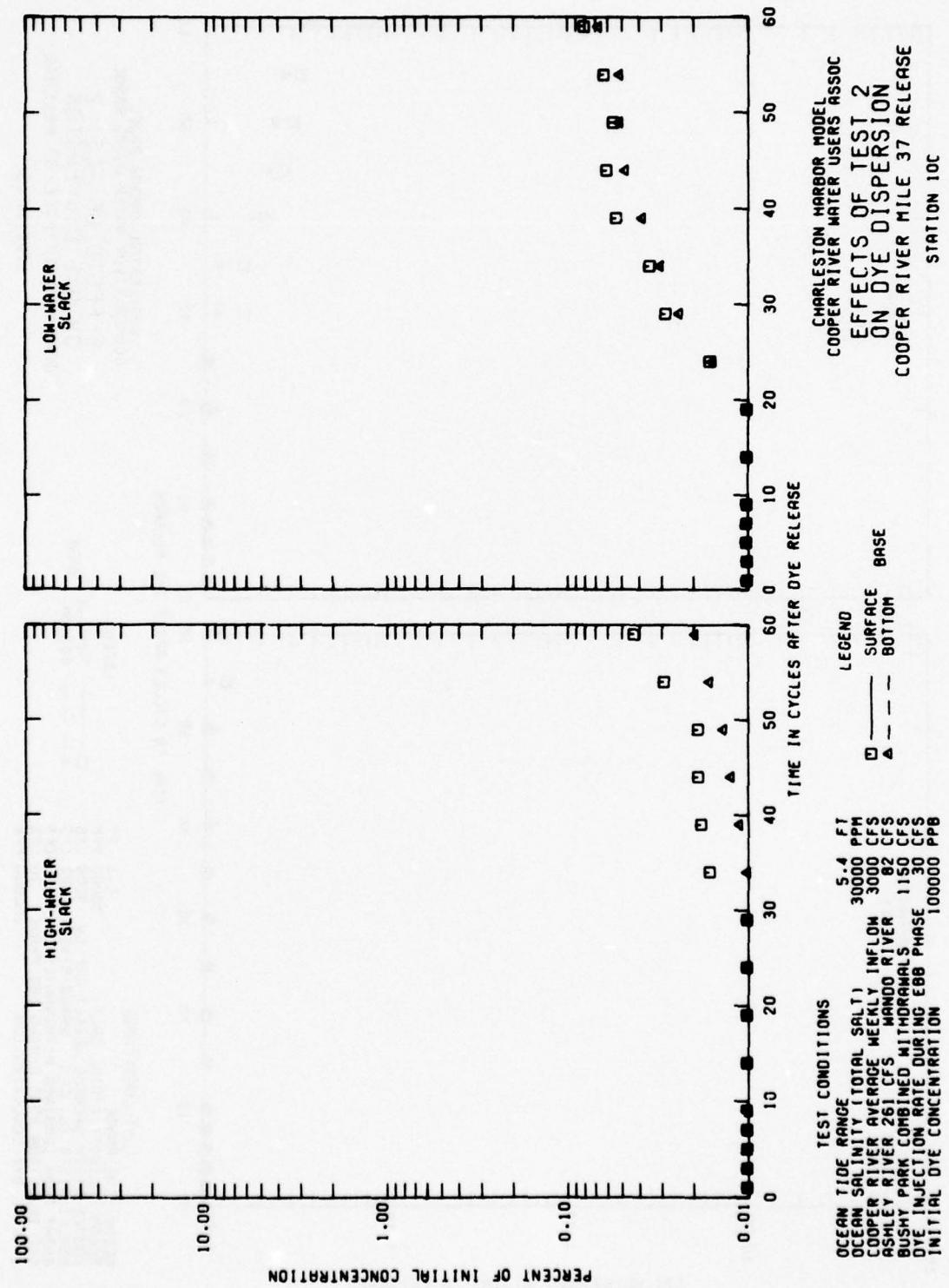


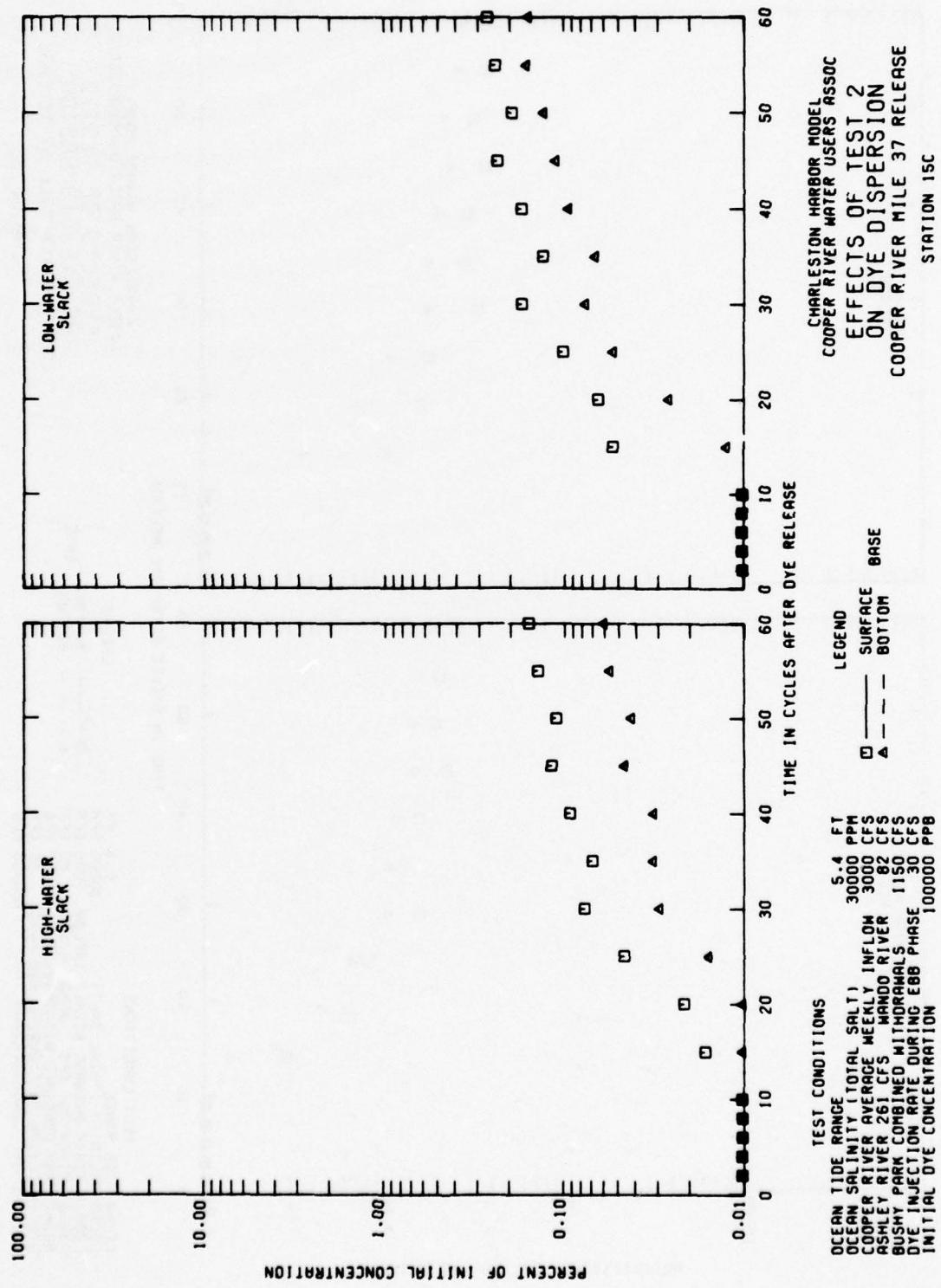
PLATE 18

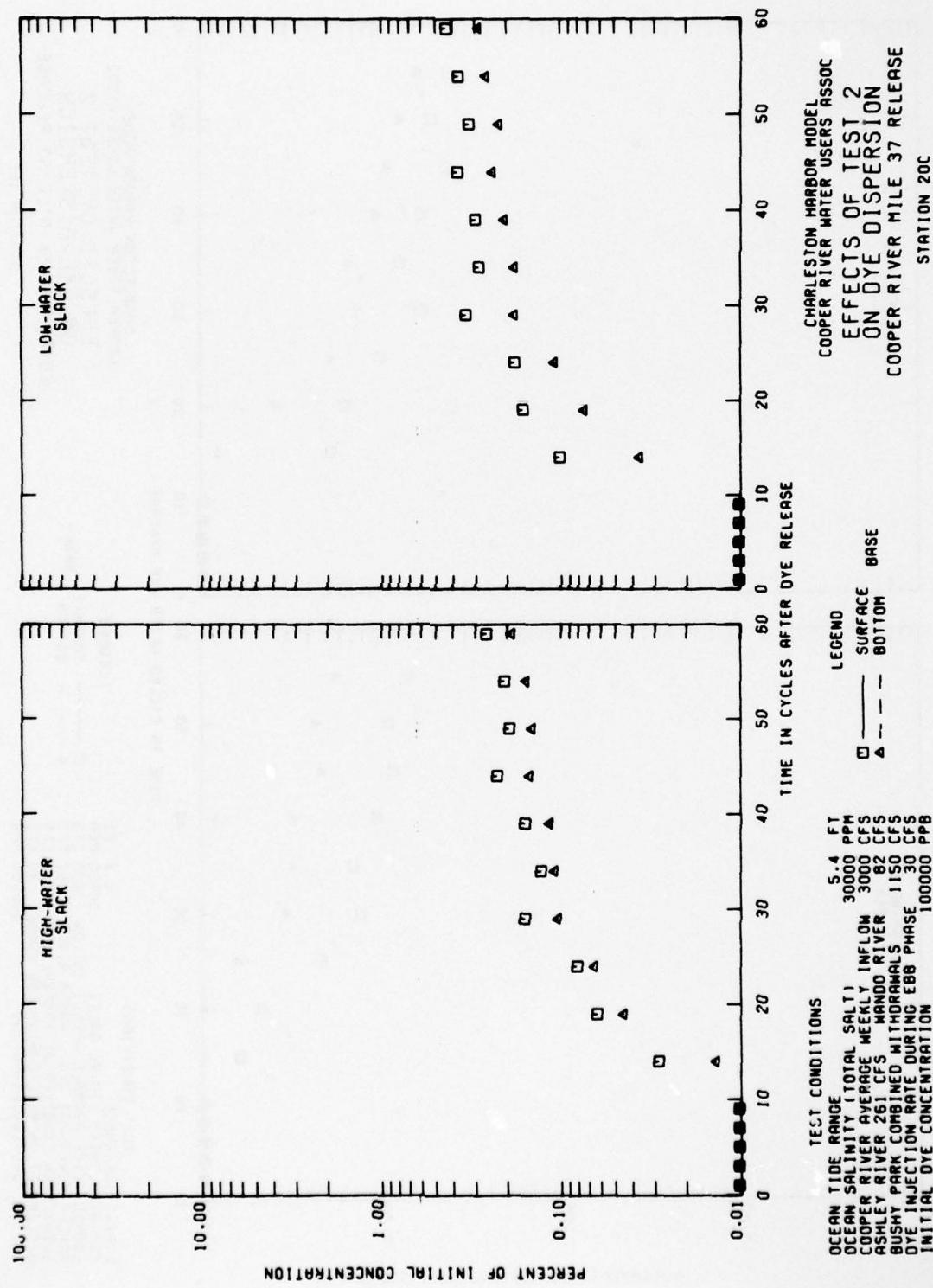


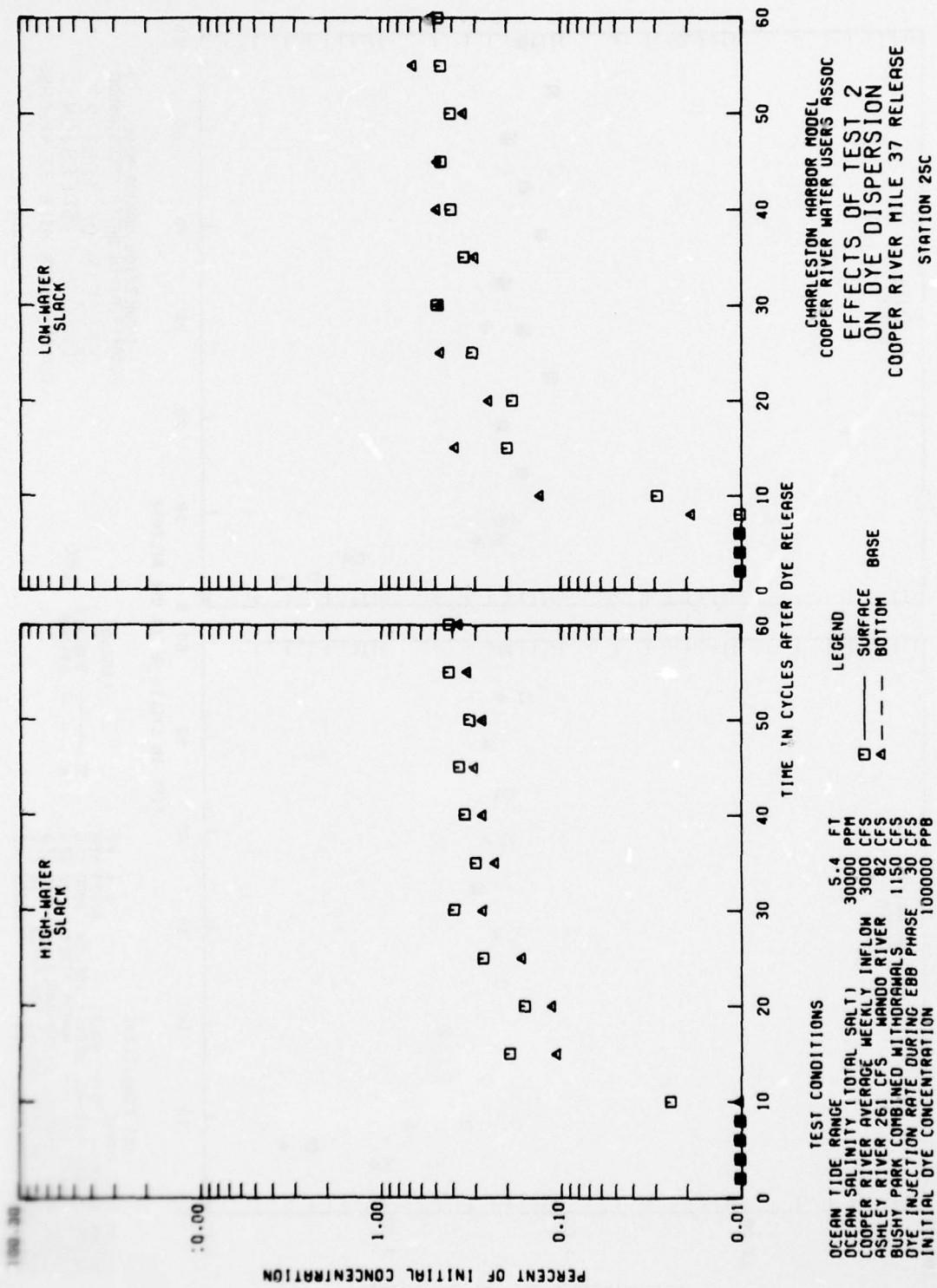


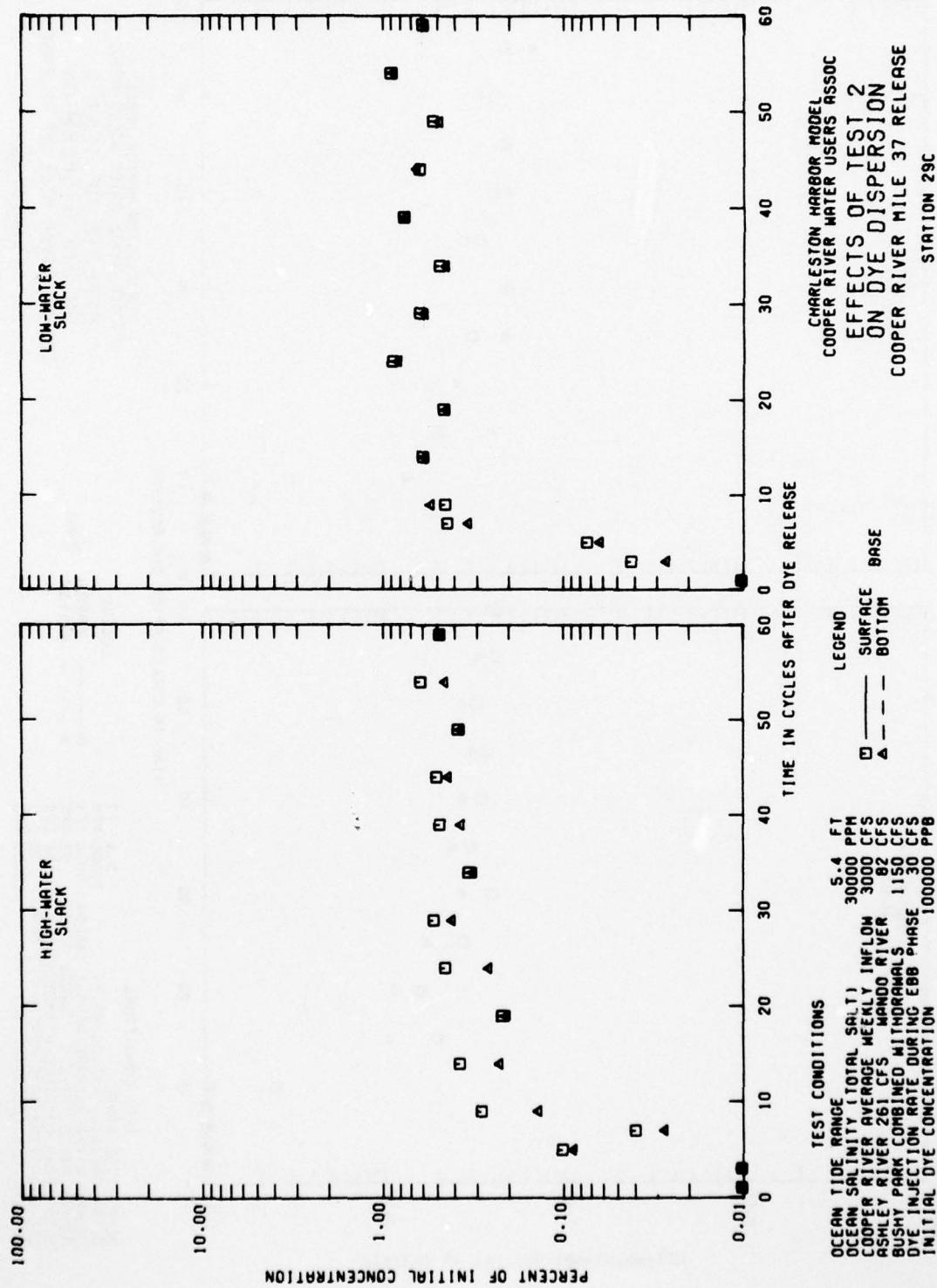


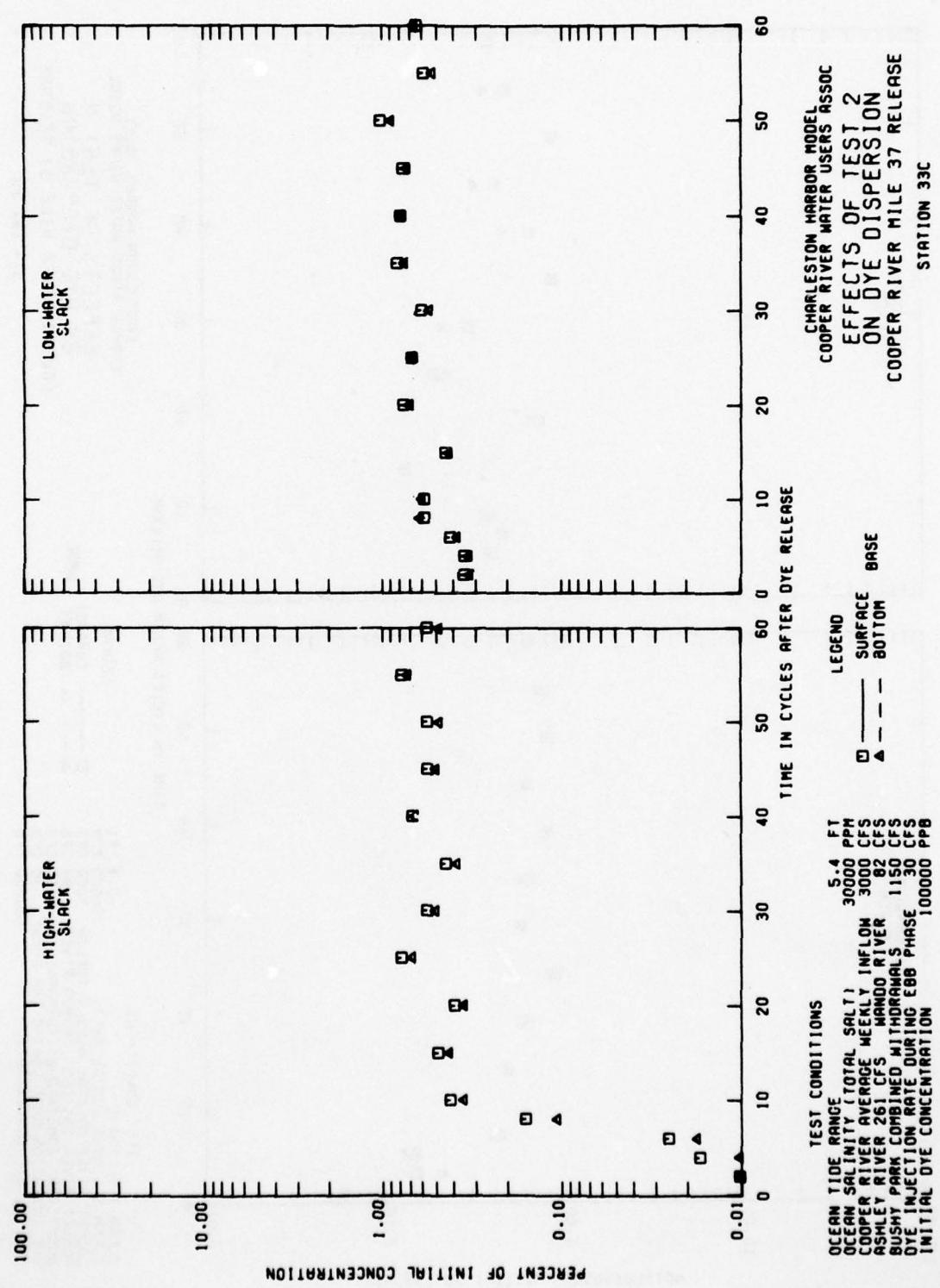


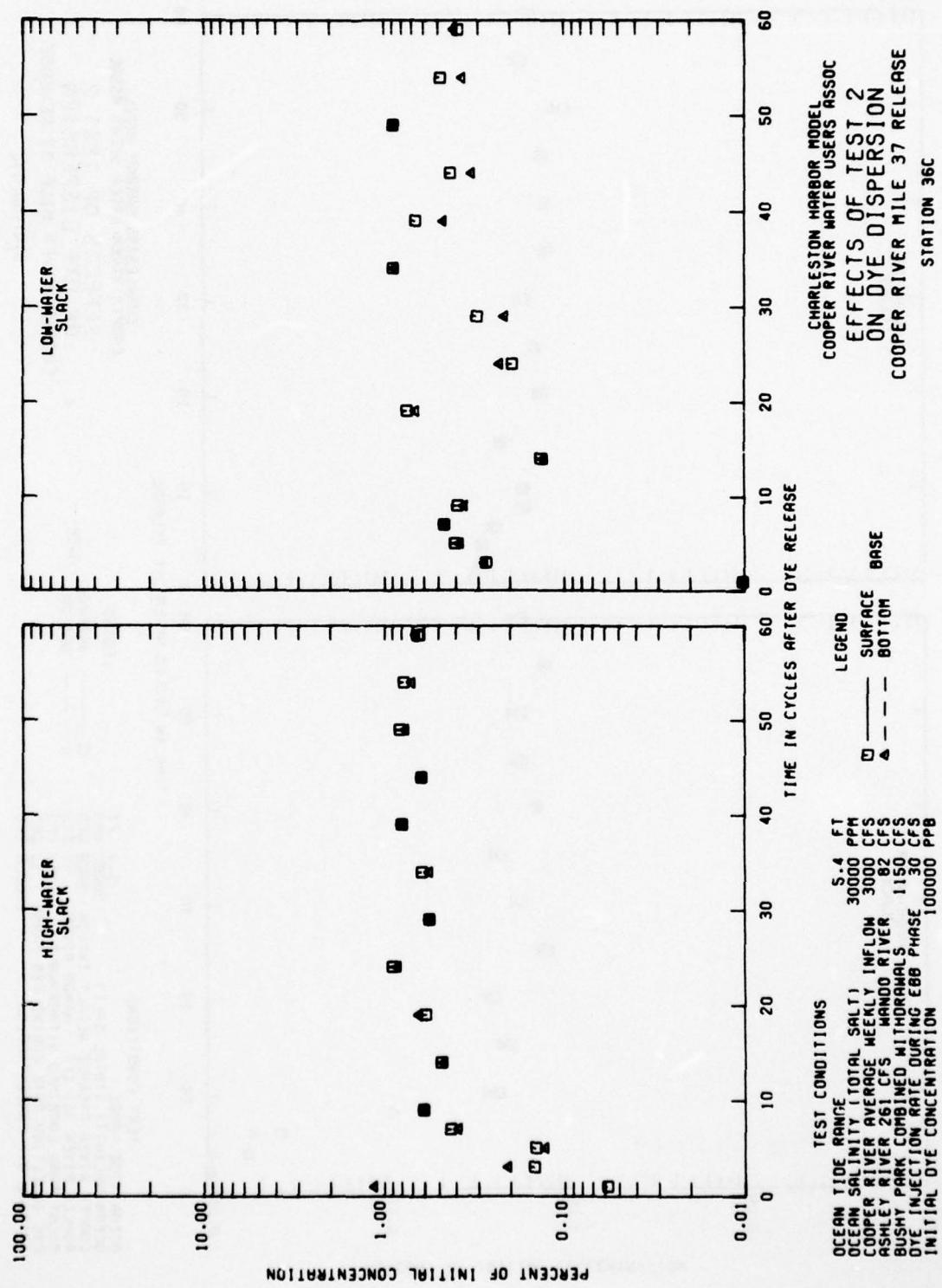


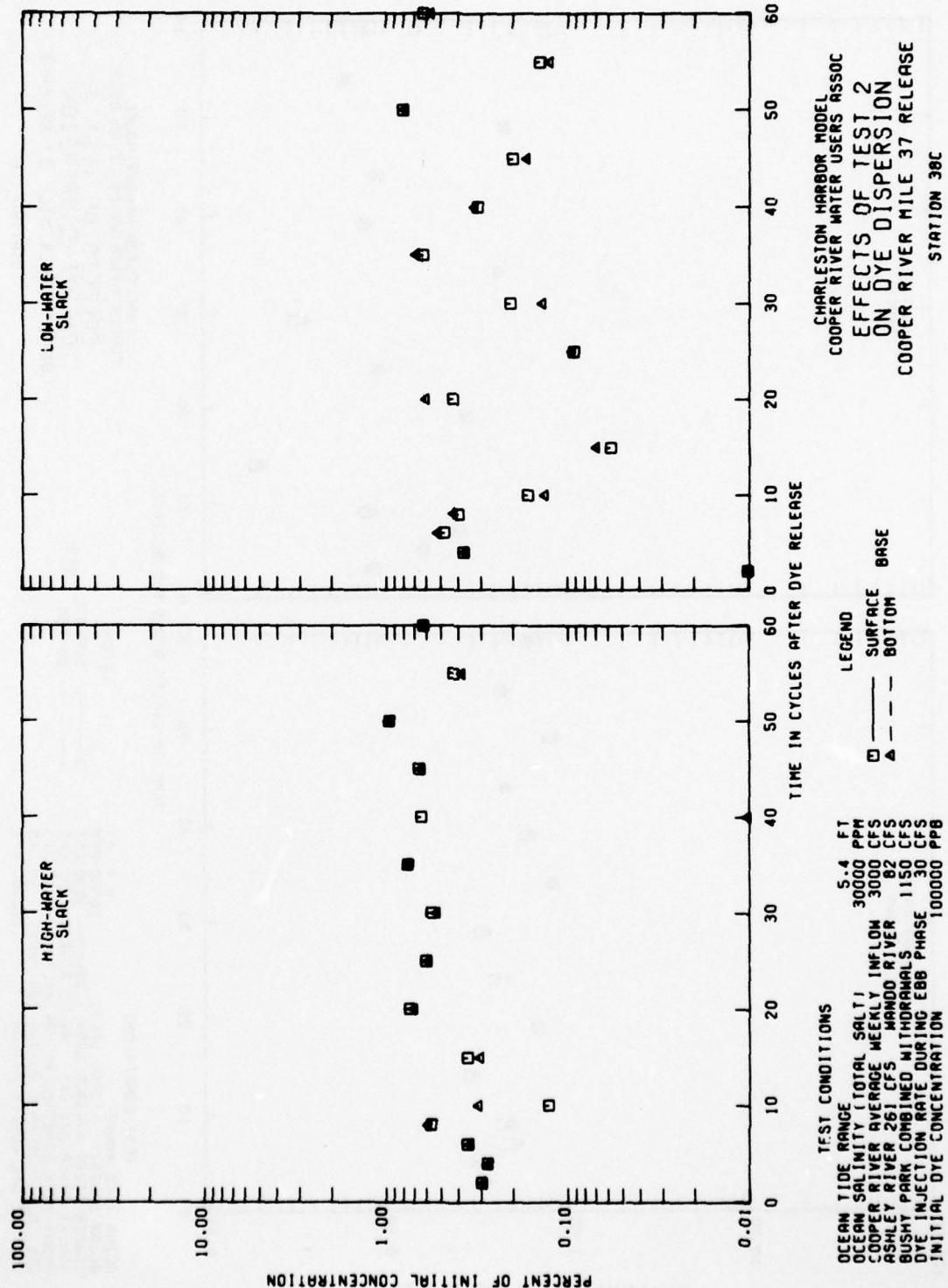


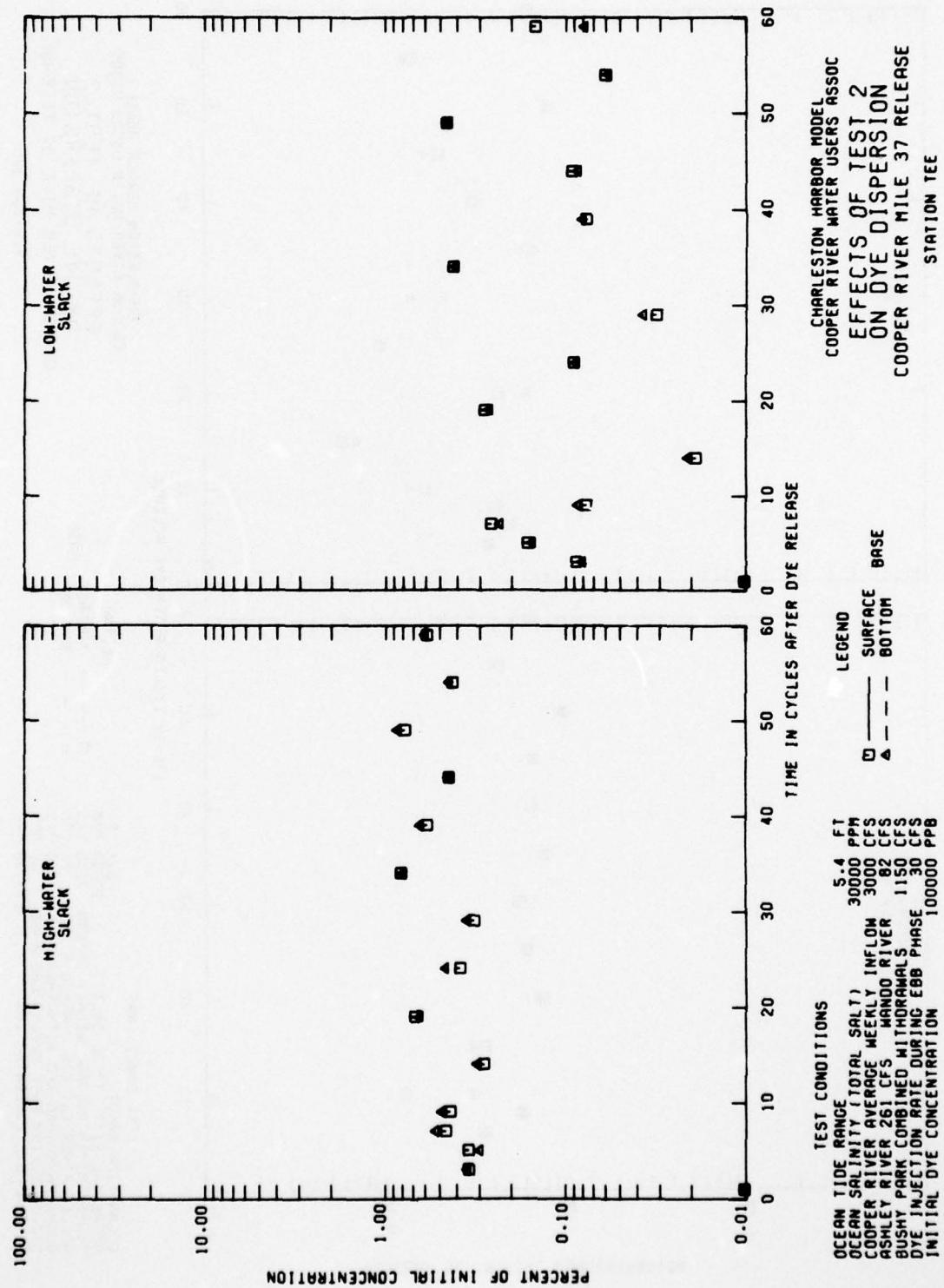


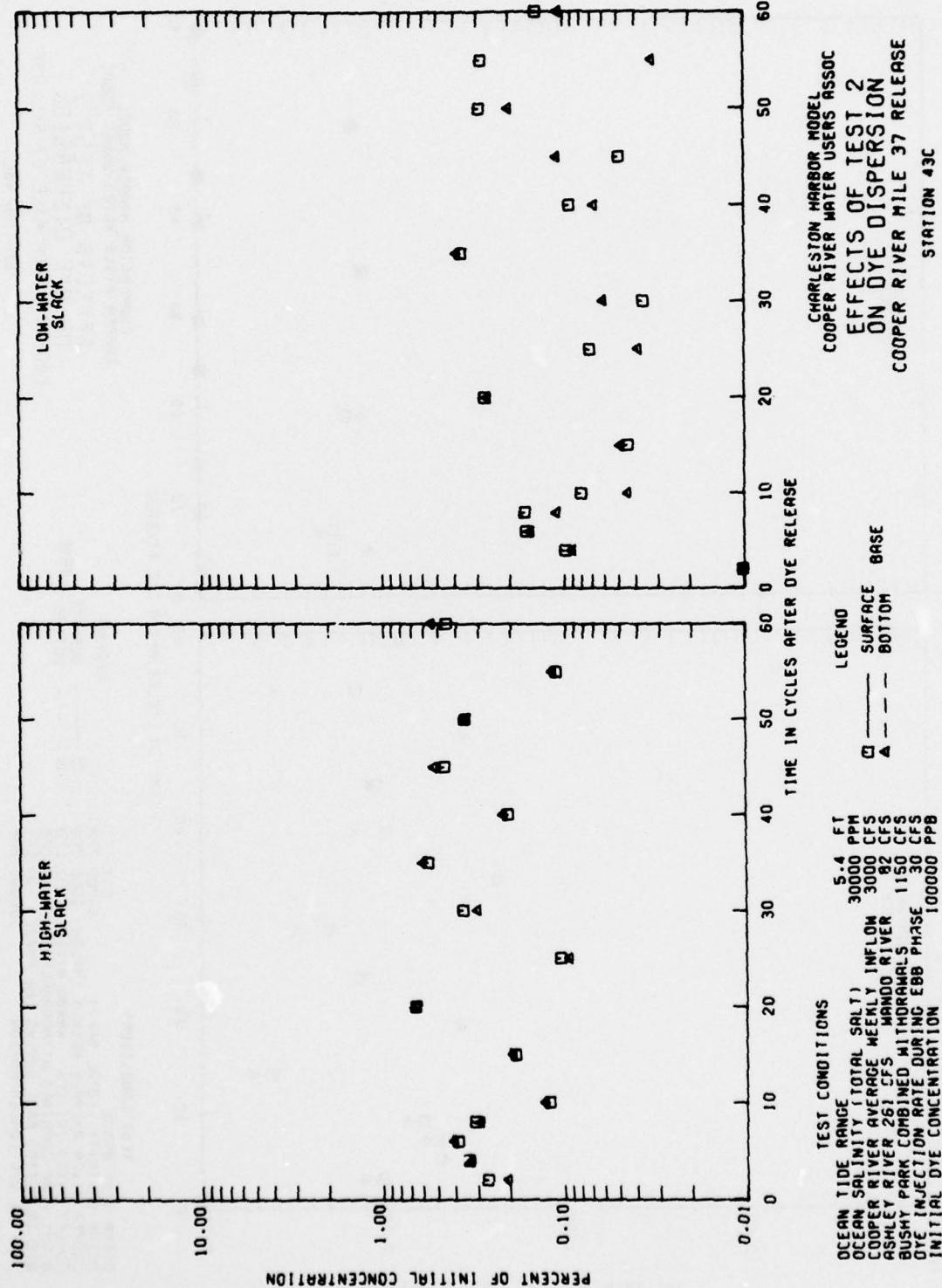


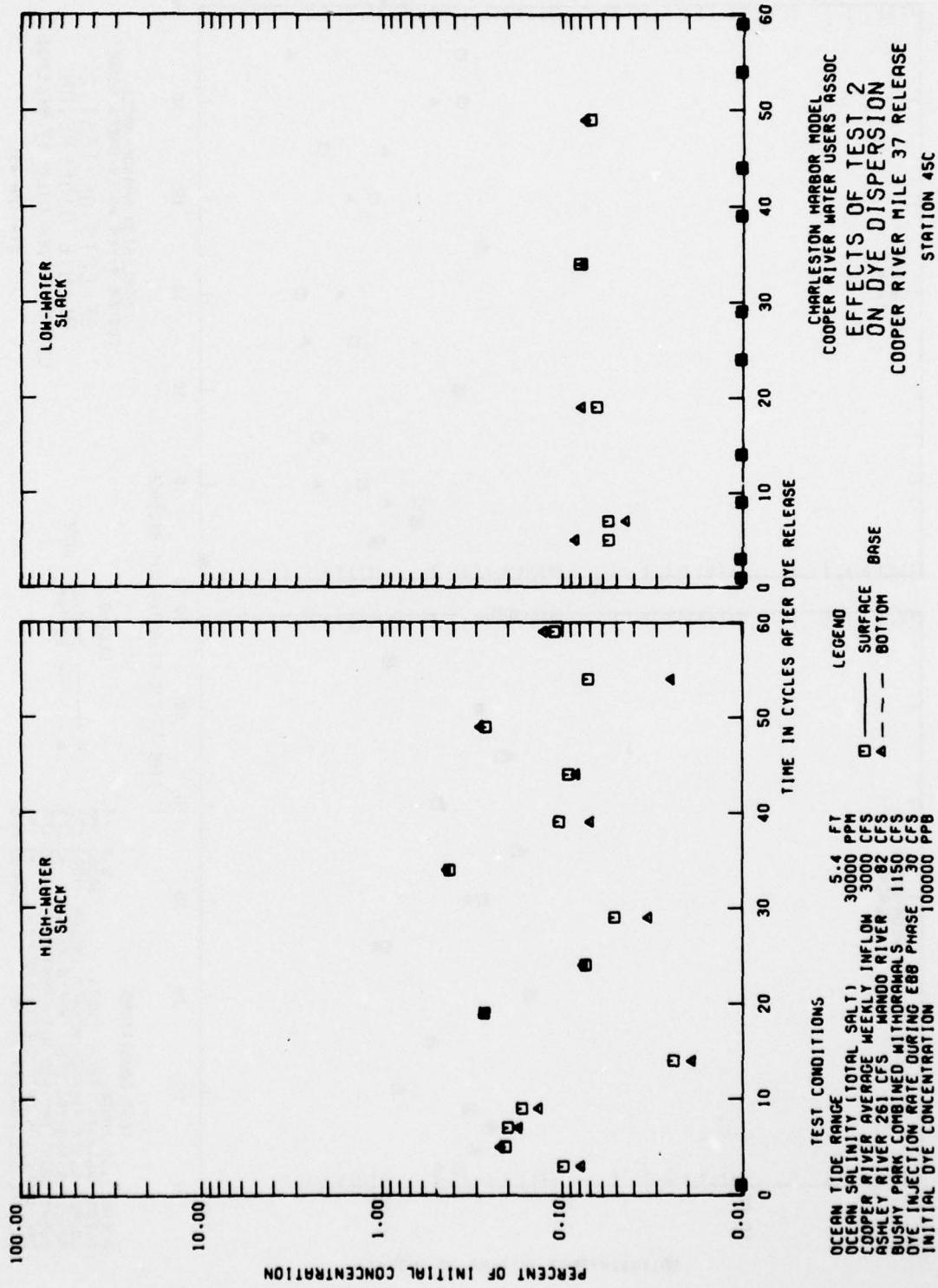


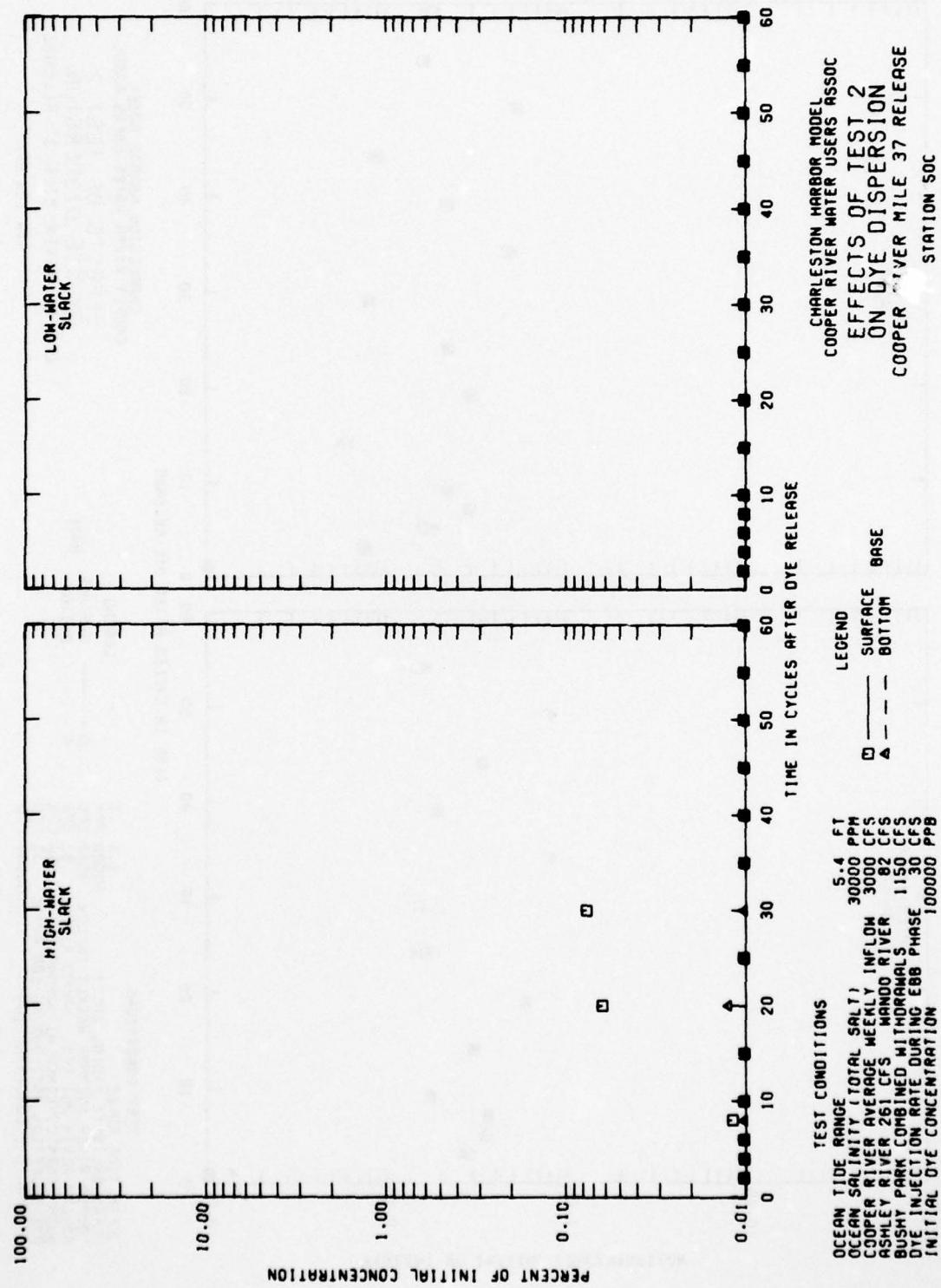


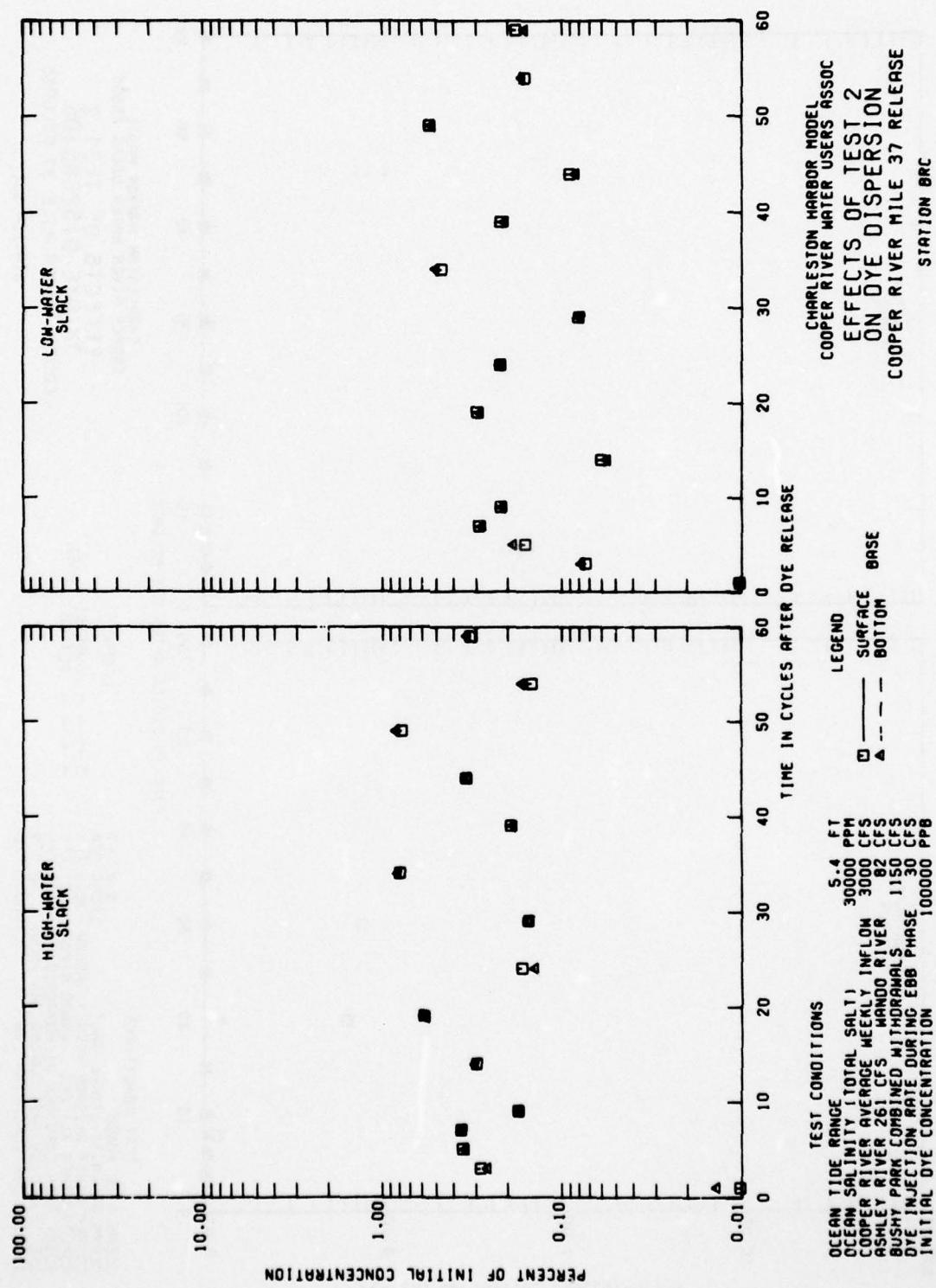


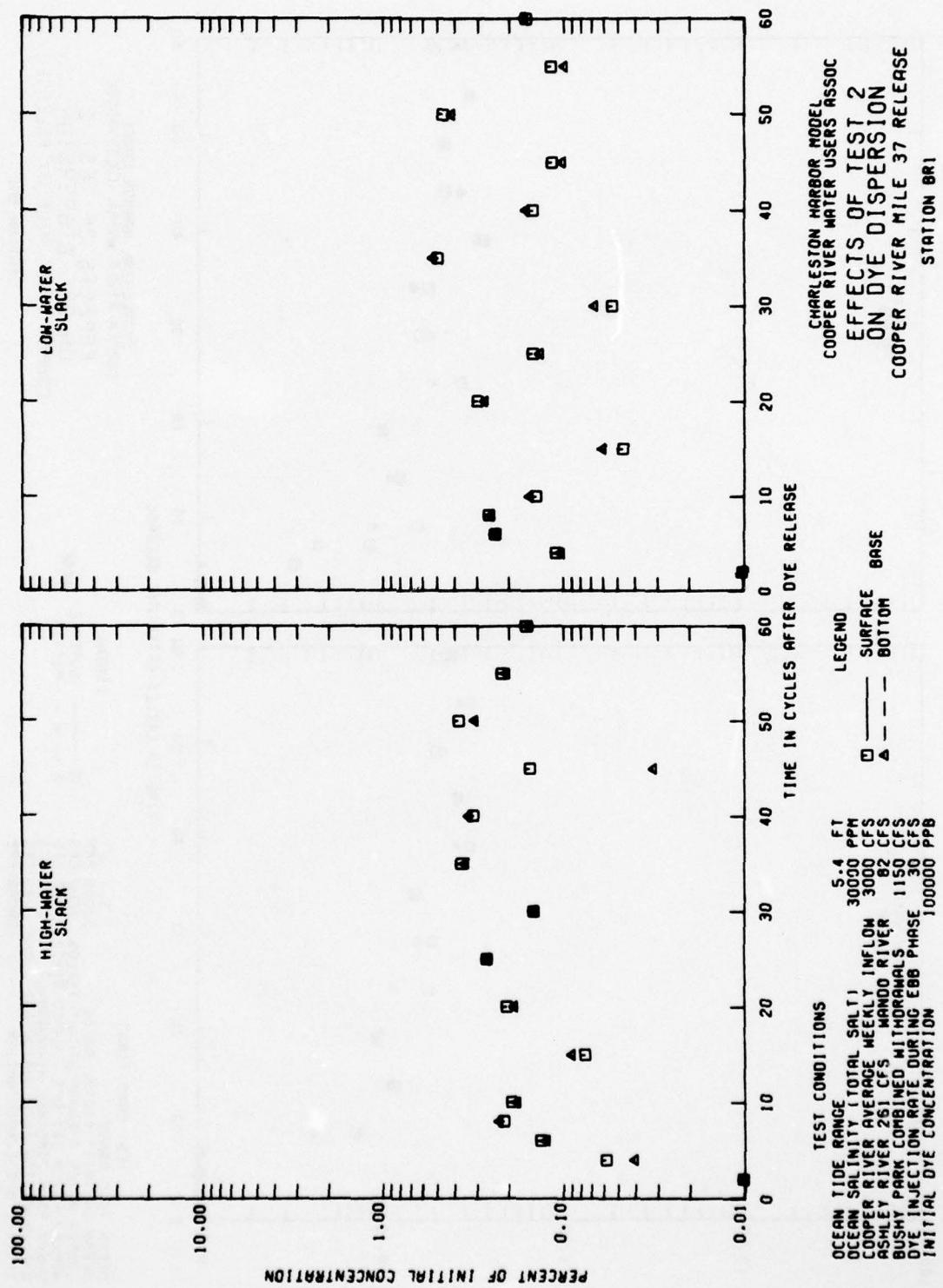


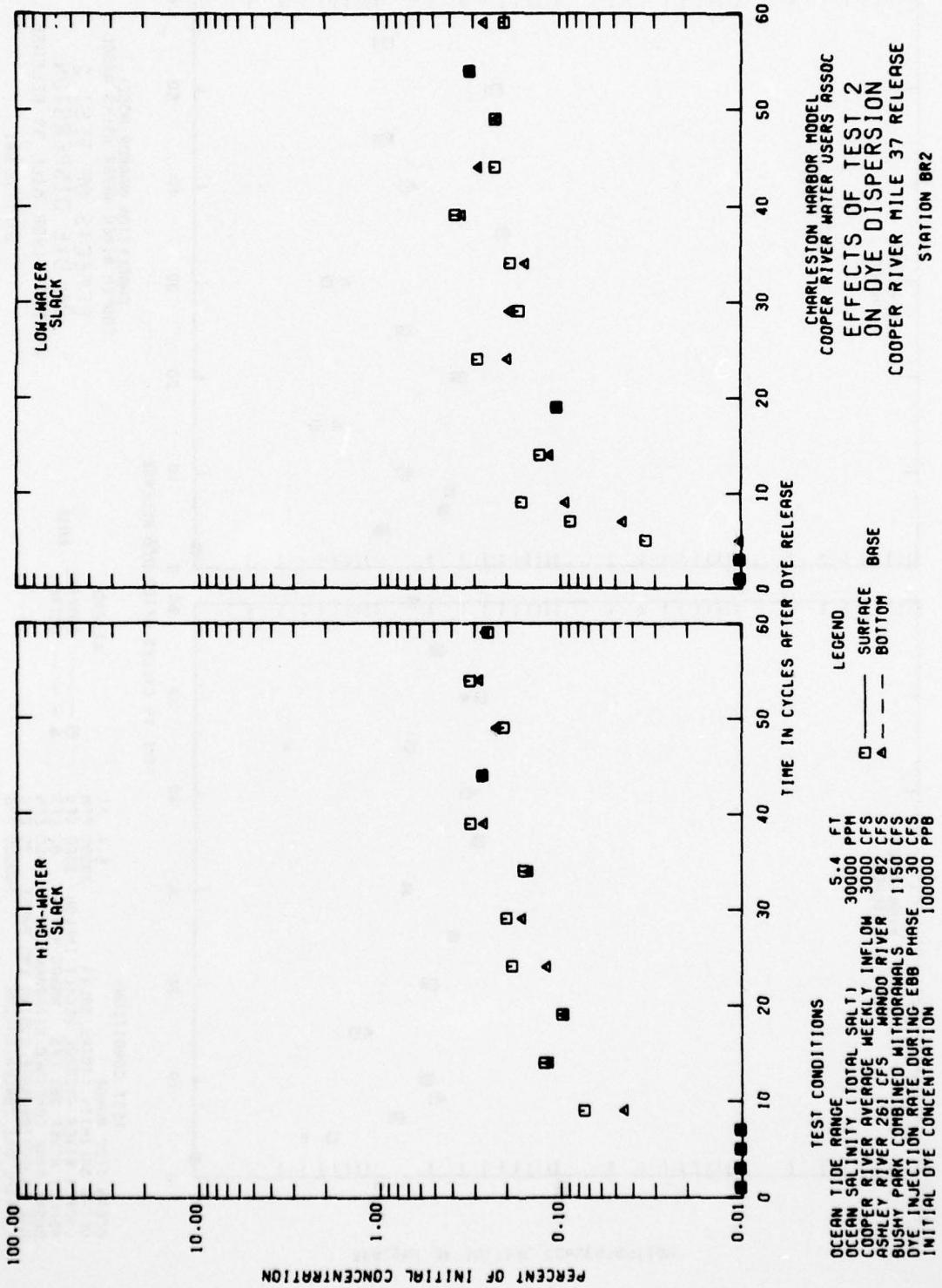


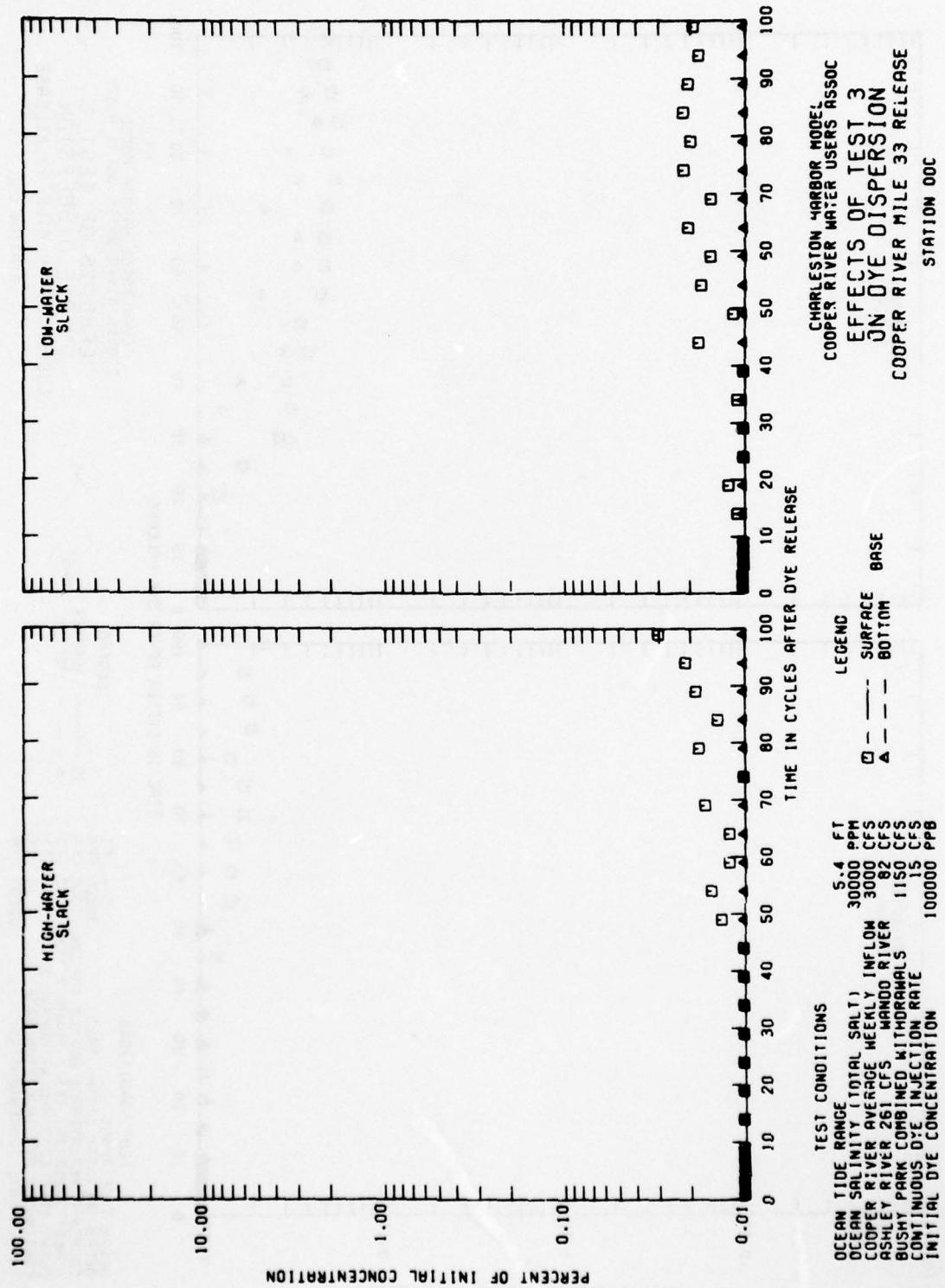












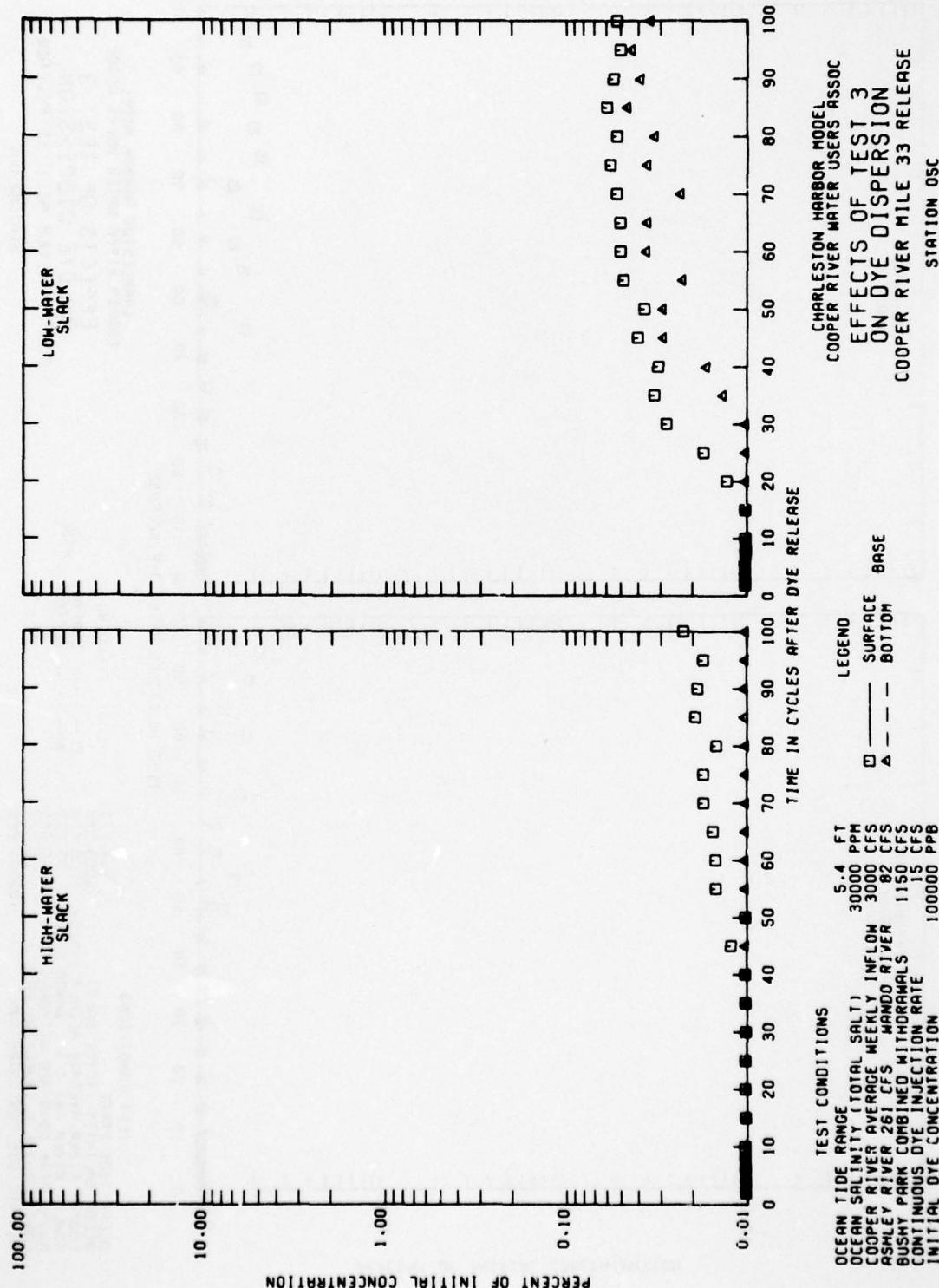


PLATE 38

AD-A051 928

ARMY ENGINEER WATERWAYS EXPERIMENT STATION VICKSBURG MISS F/G 13/2
DISPERSION OF PROPOSED EFFLUENT DISCHARGES AND SALTWATER INTRUS--ETC(U)
NOV 77 H A BENSON, R A BOLAND

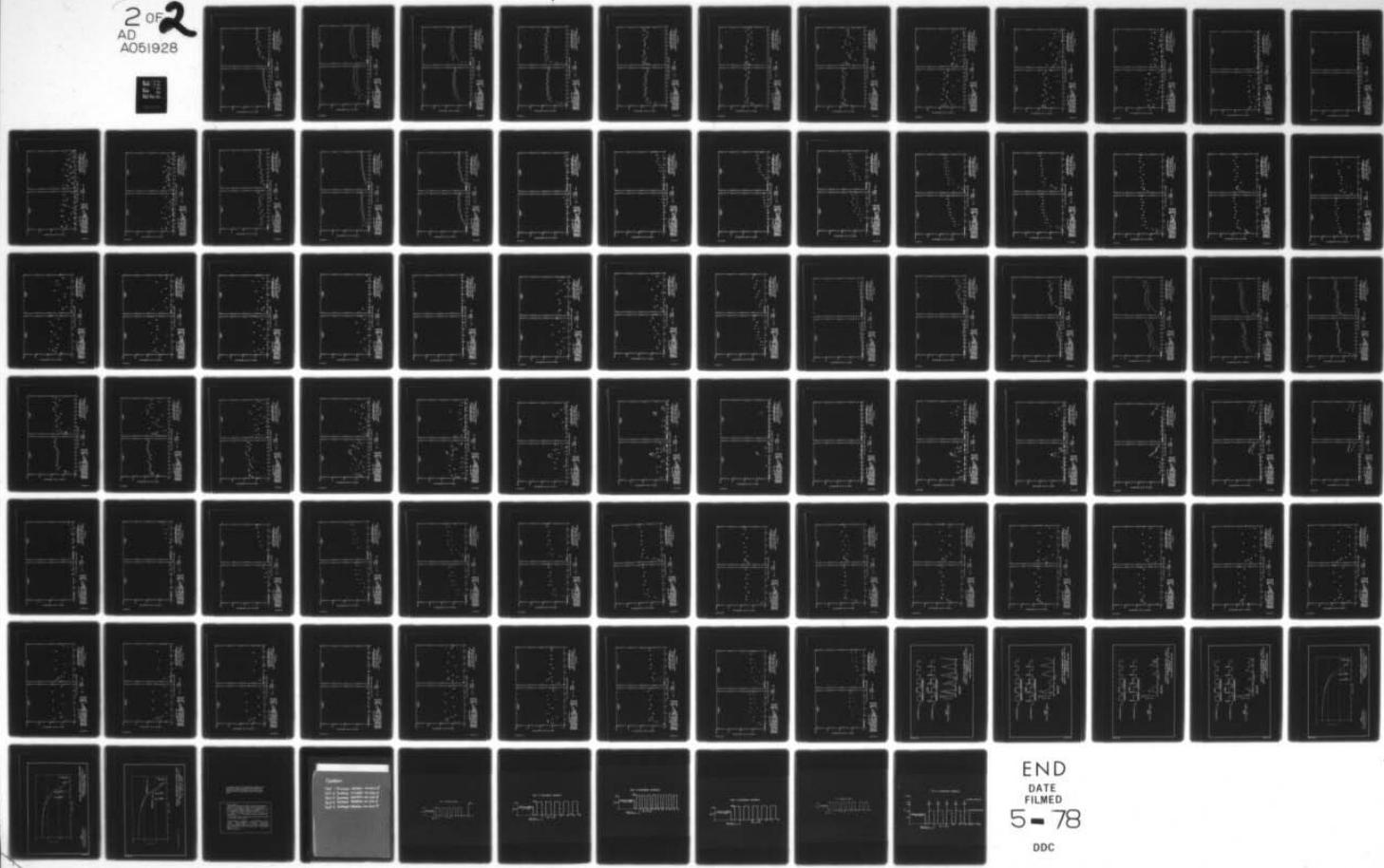
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WES-MP-H-77-14

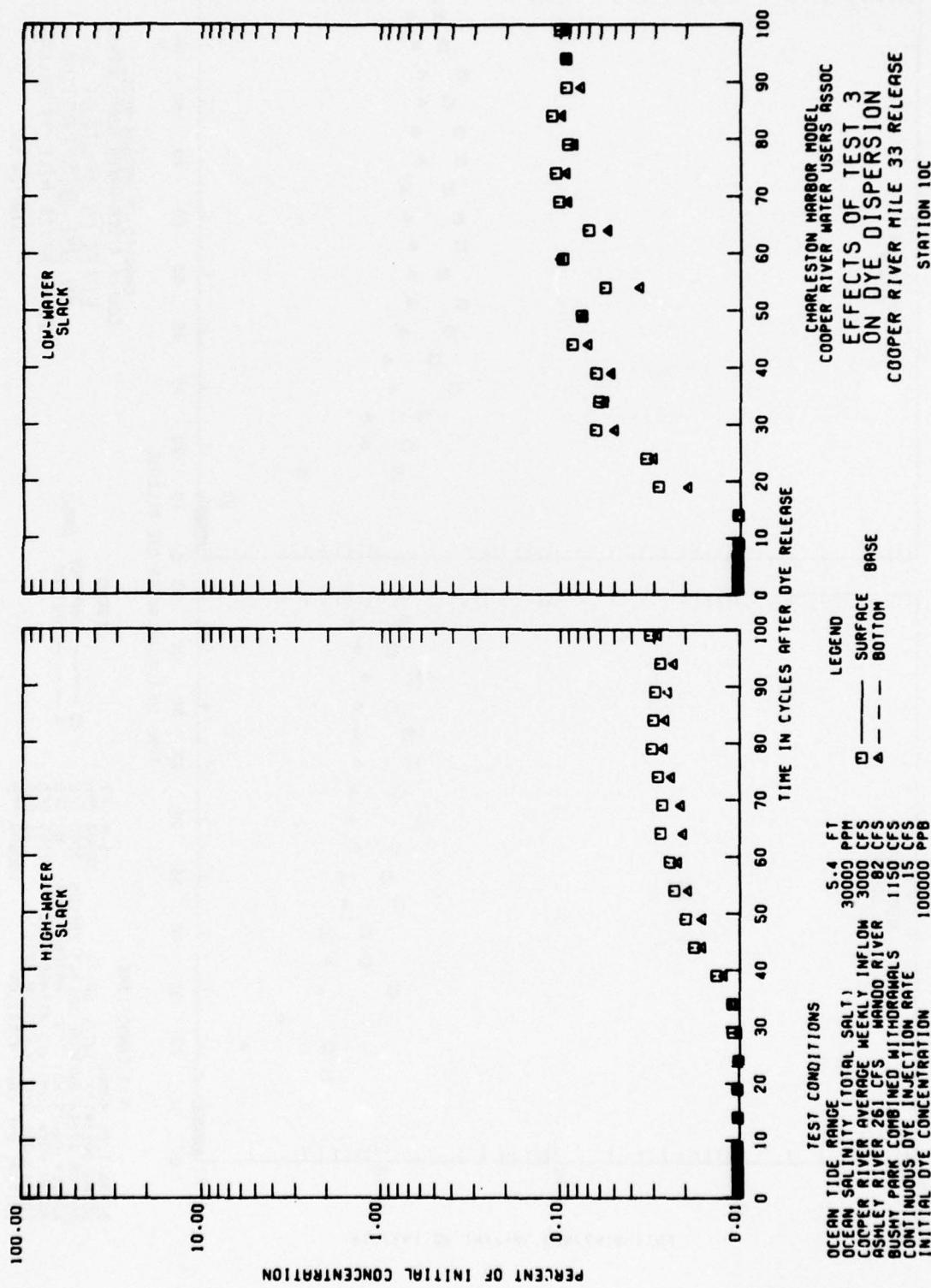
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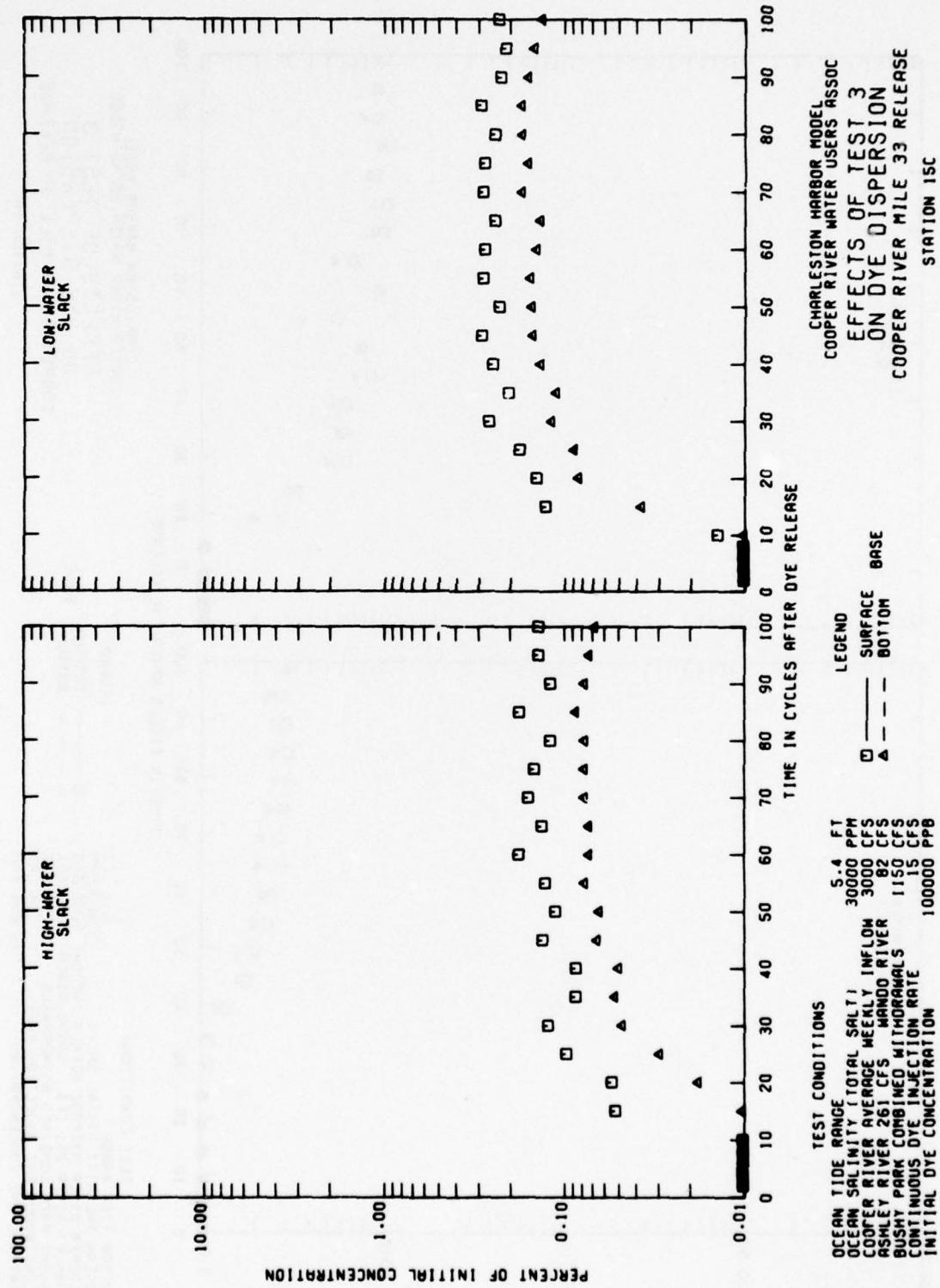
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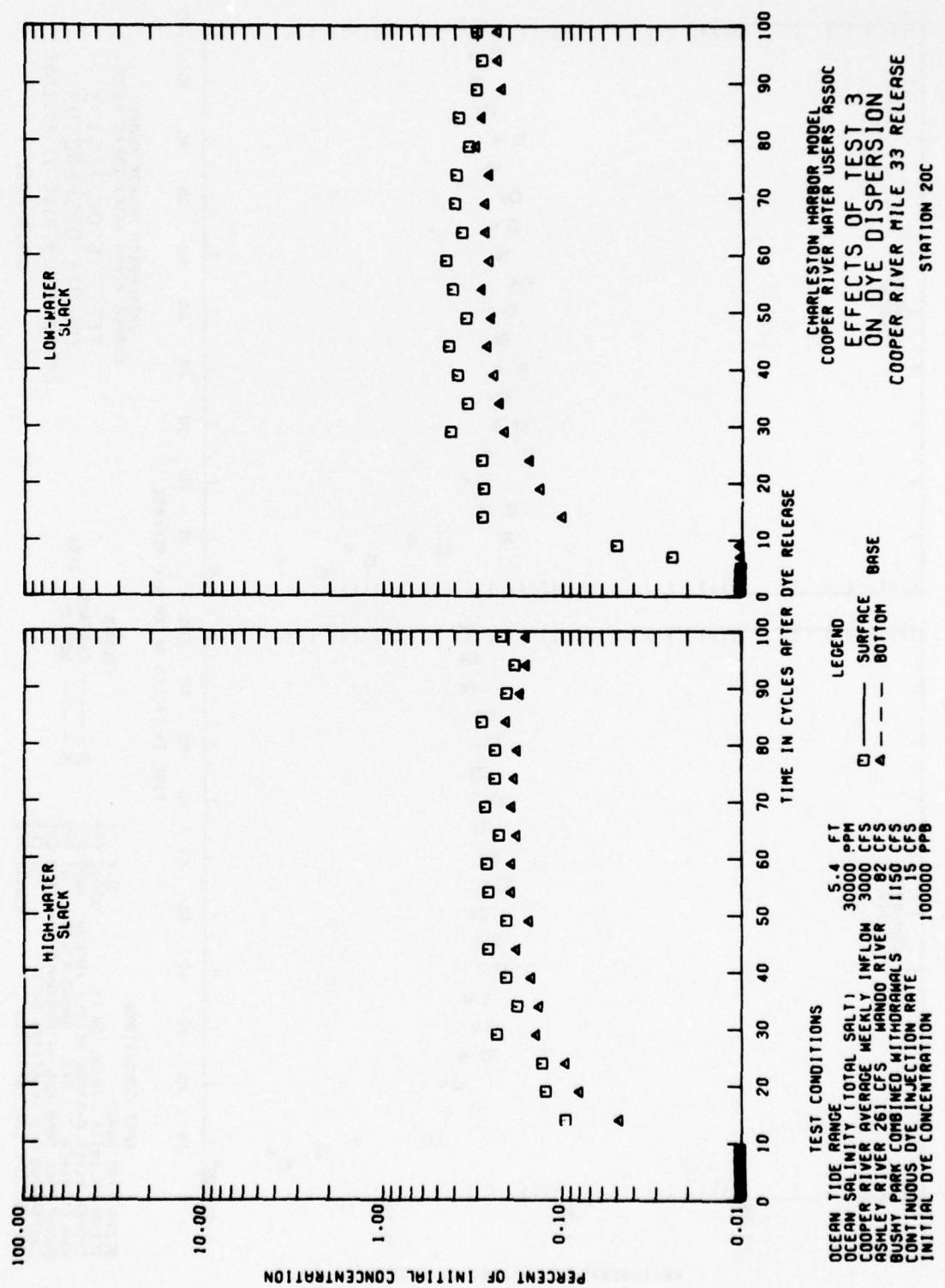
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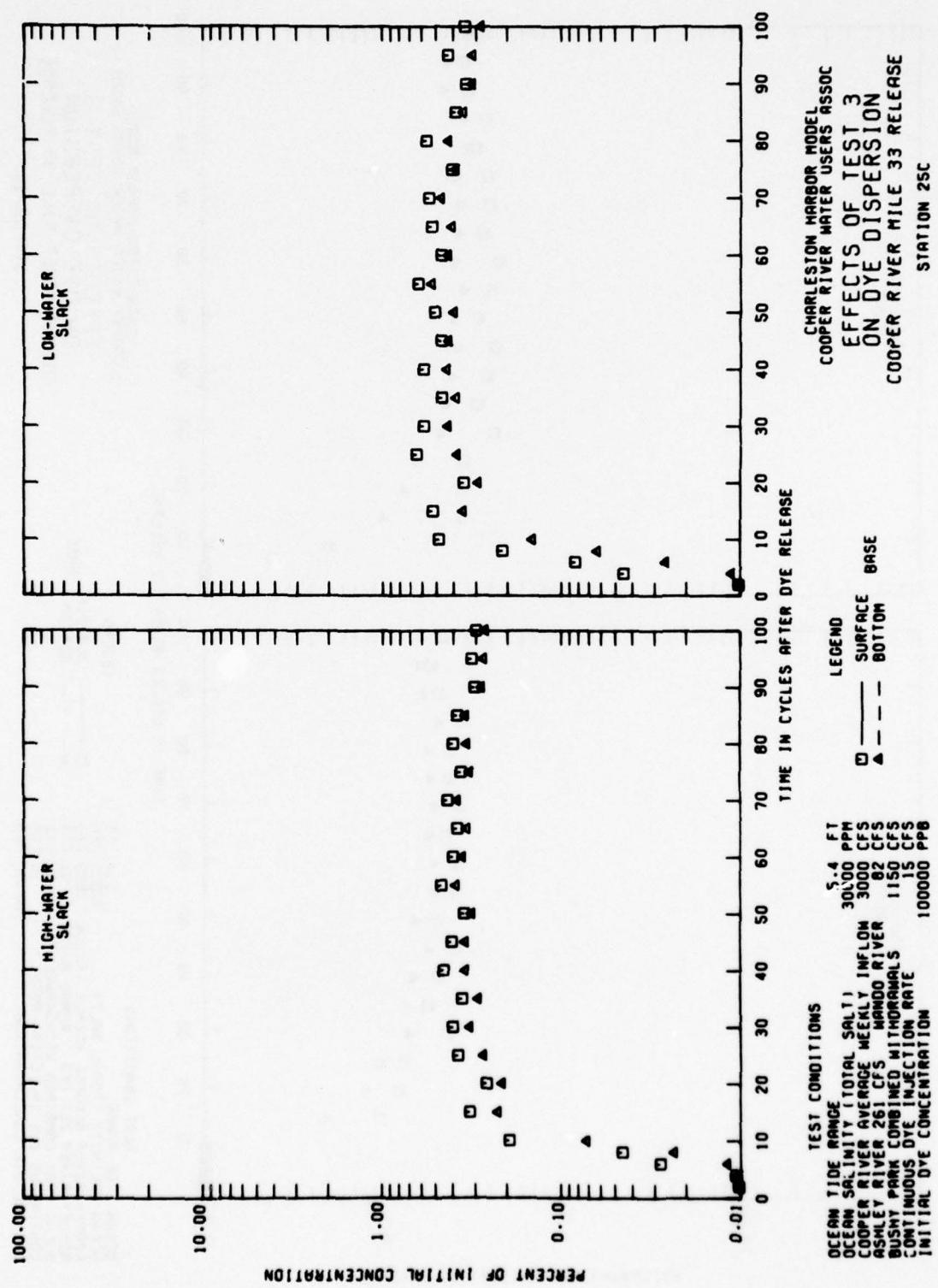


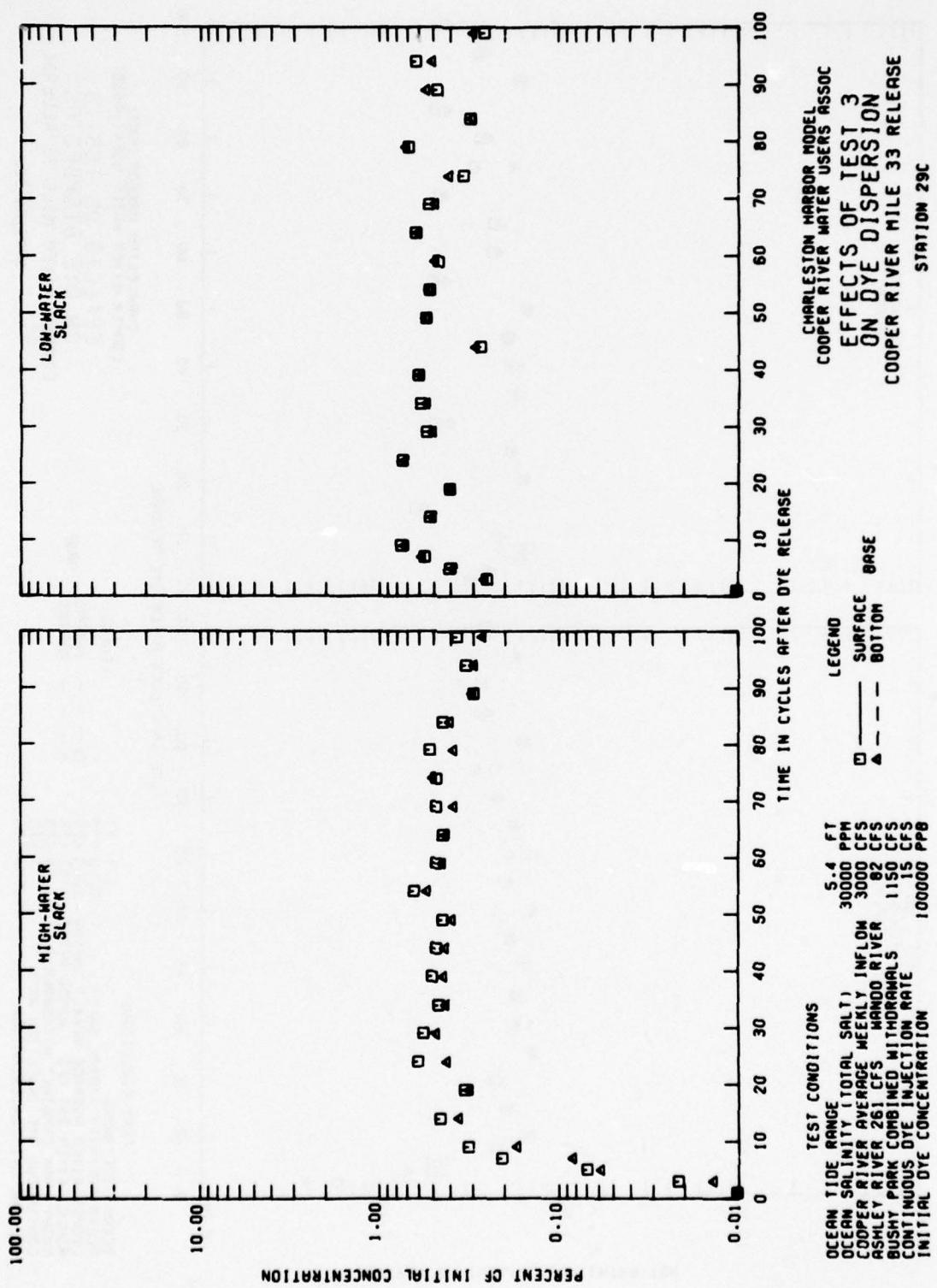
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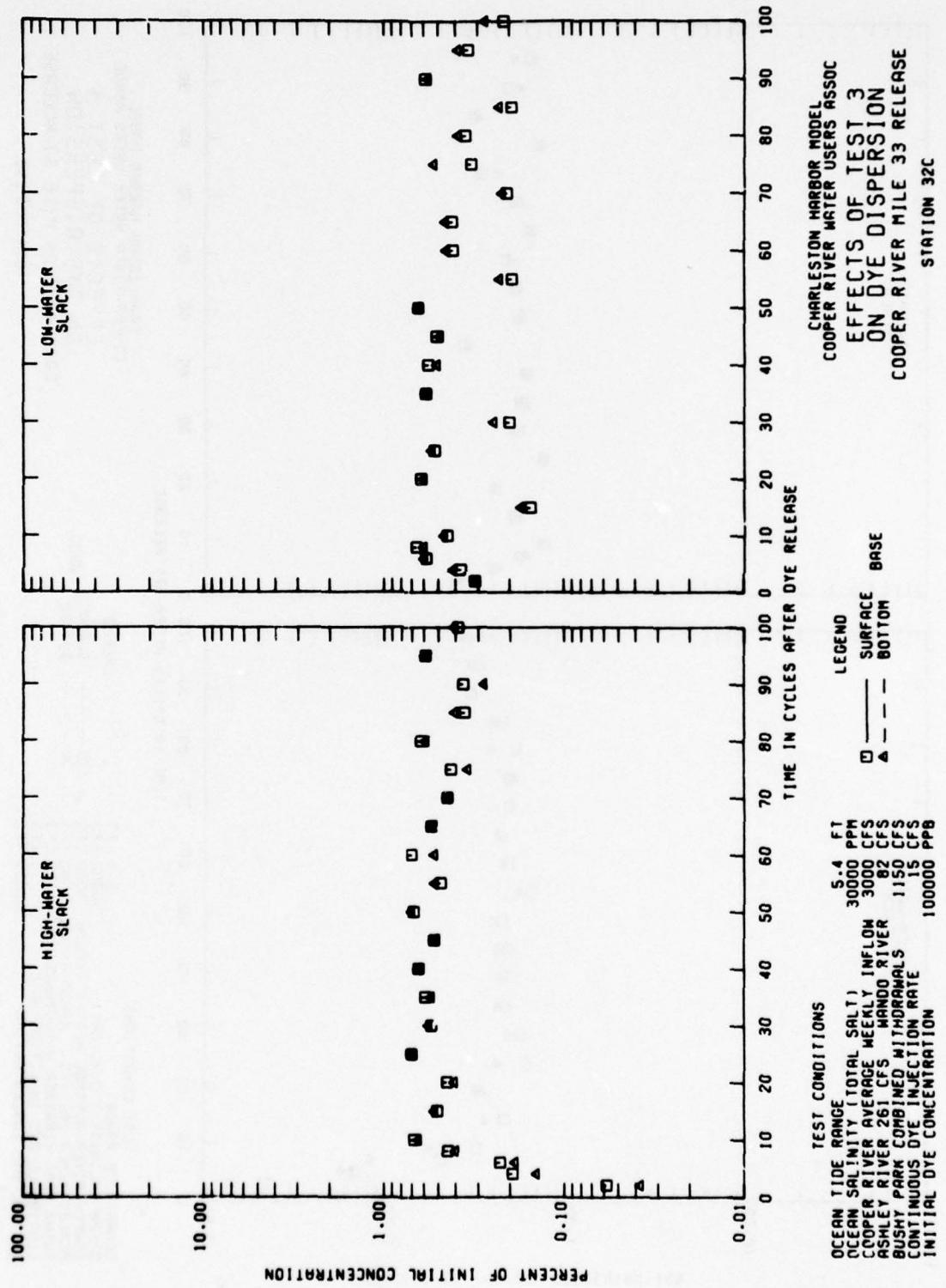


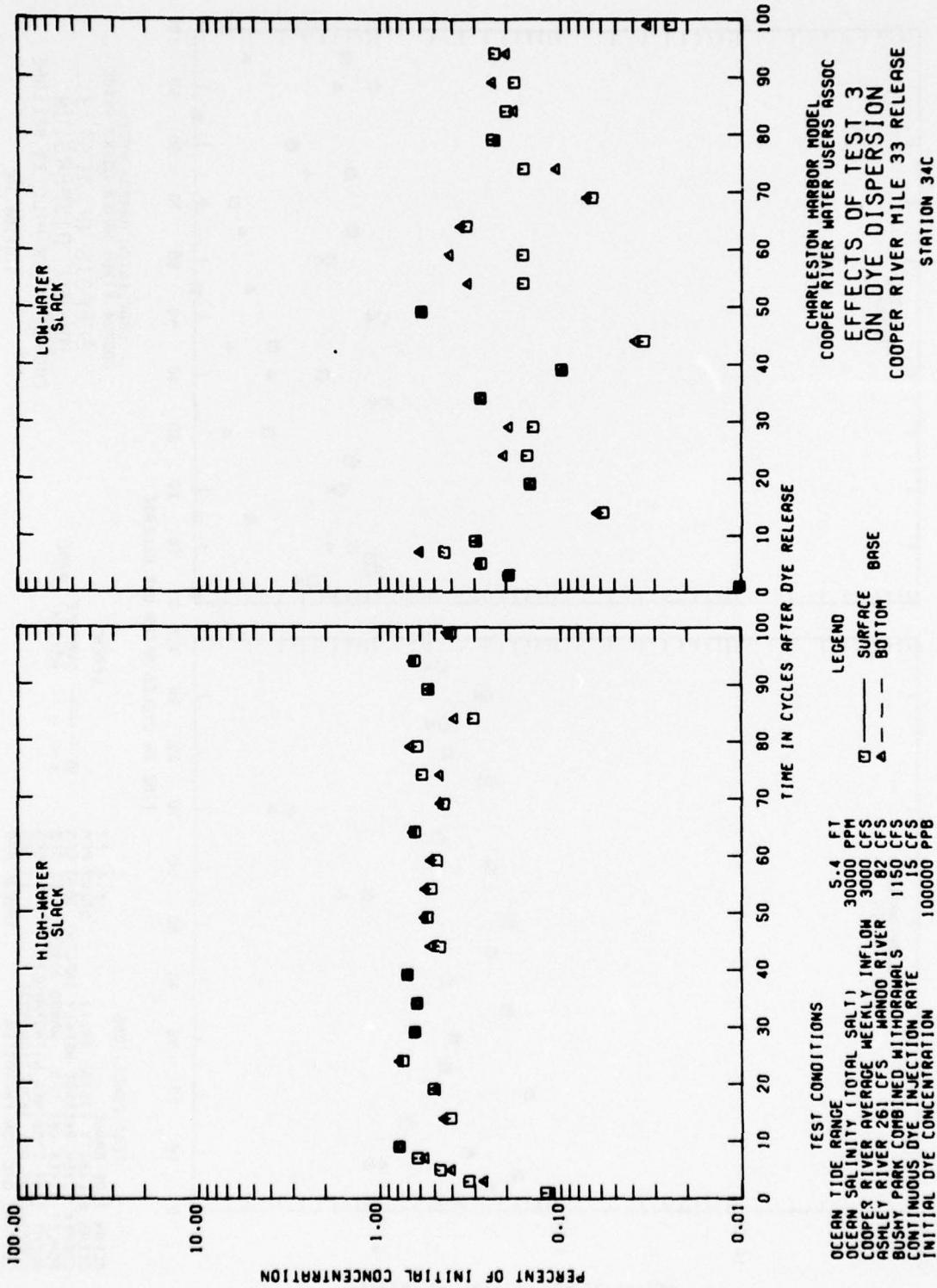


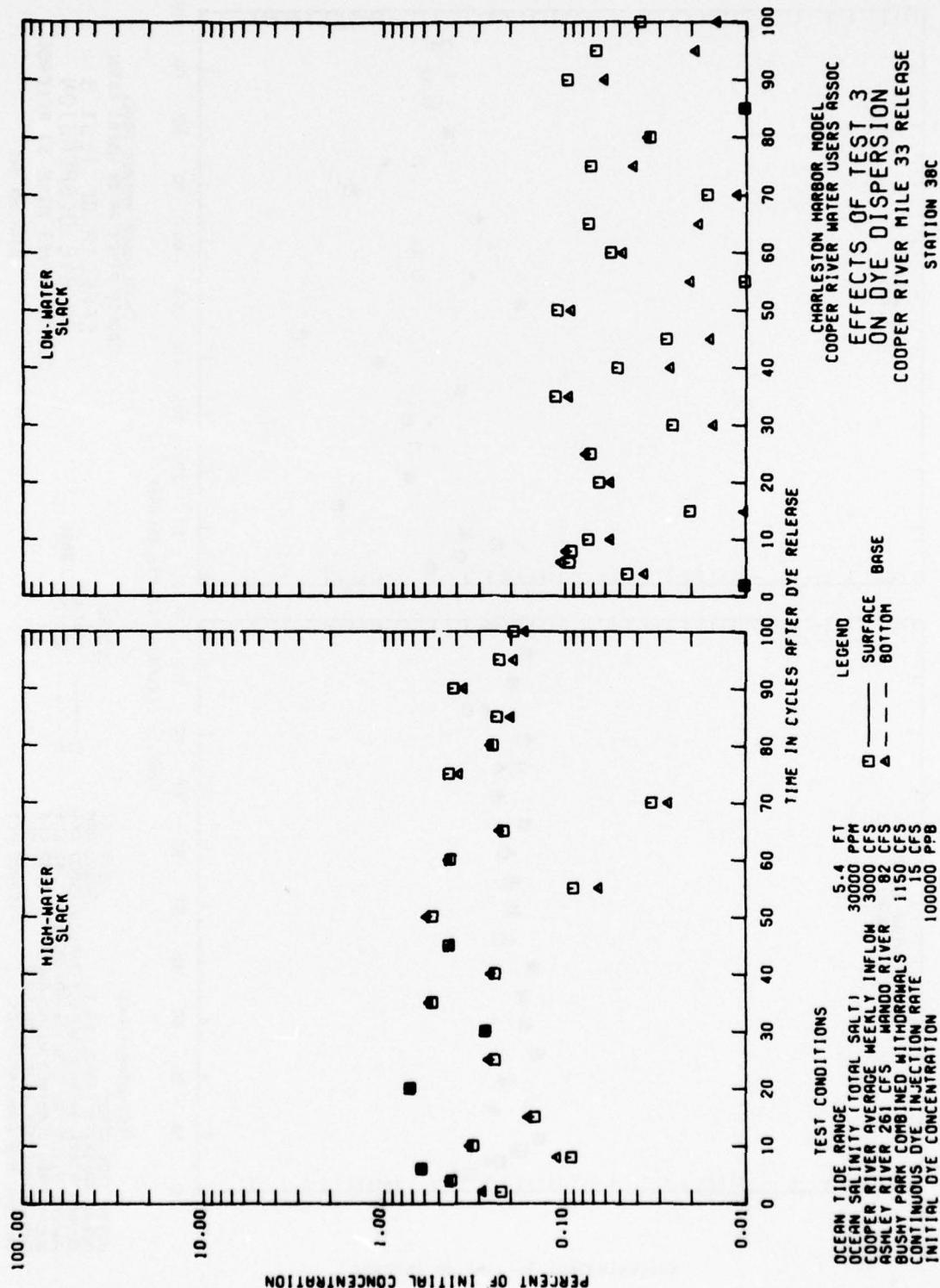


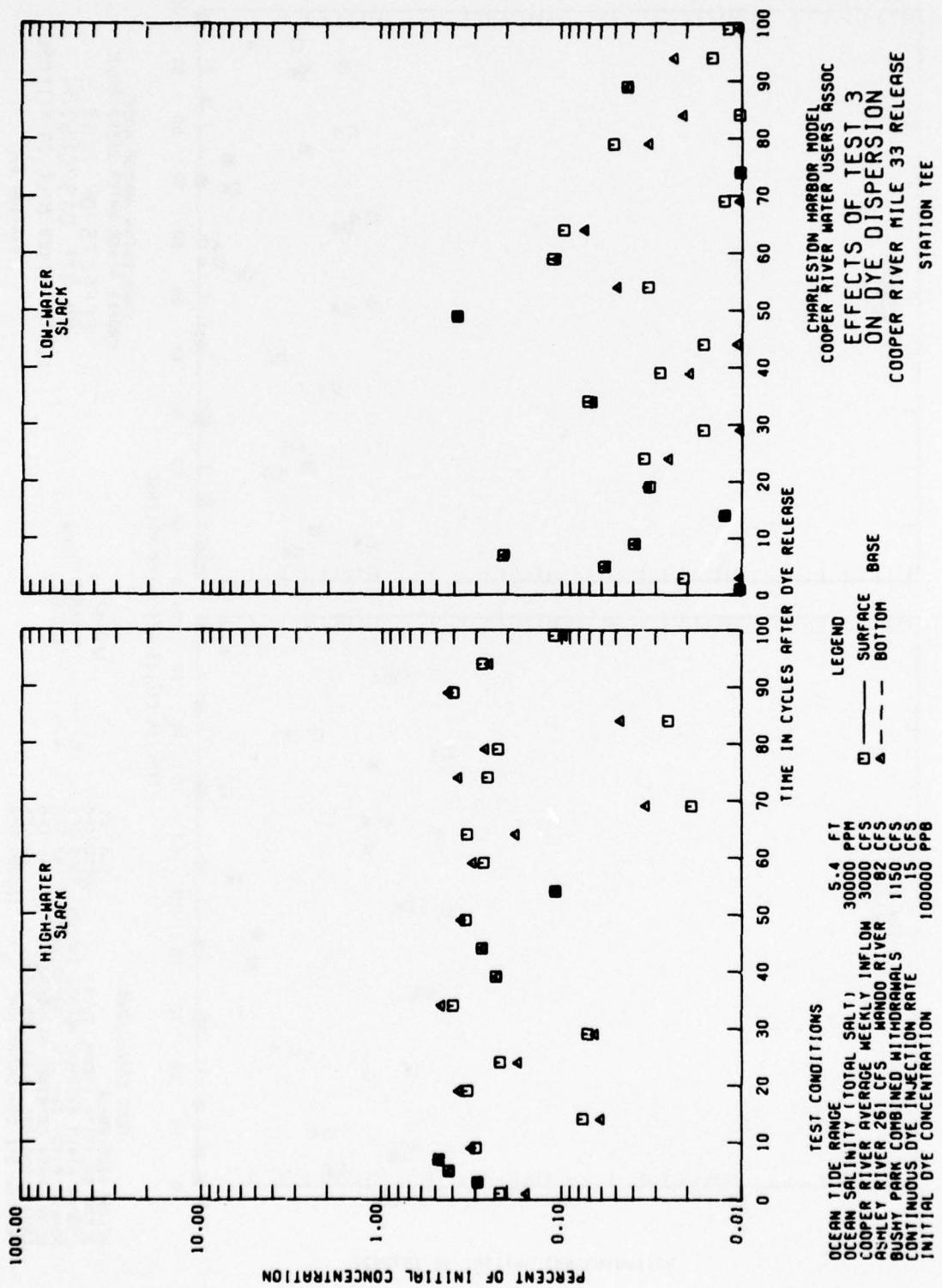


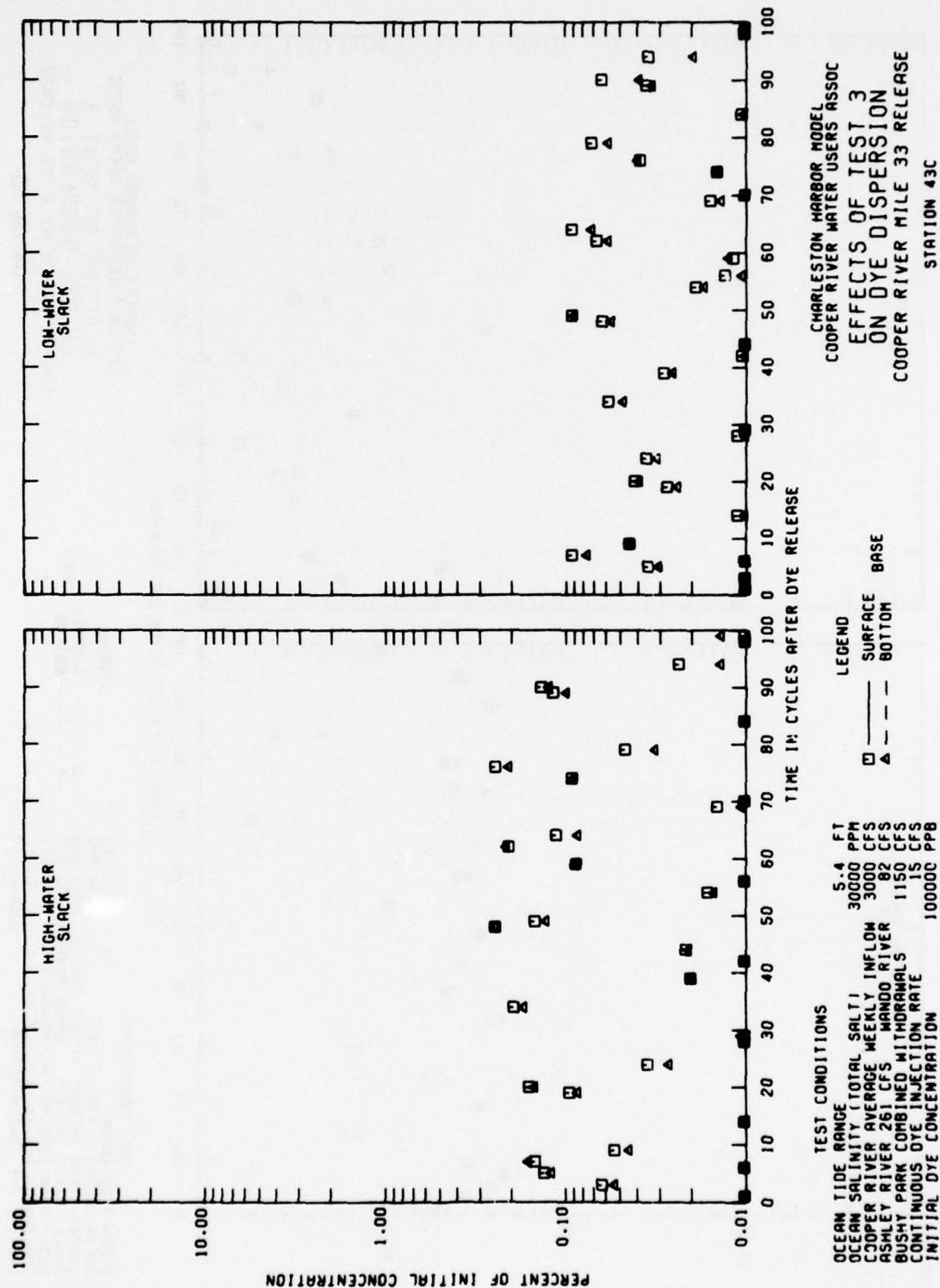


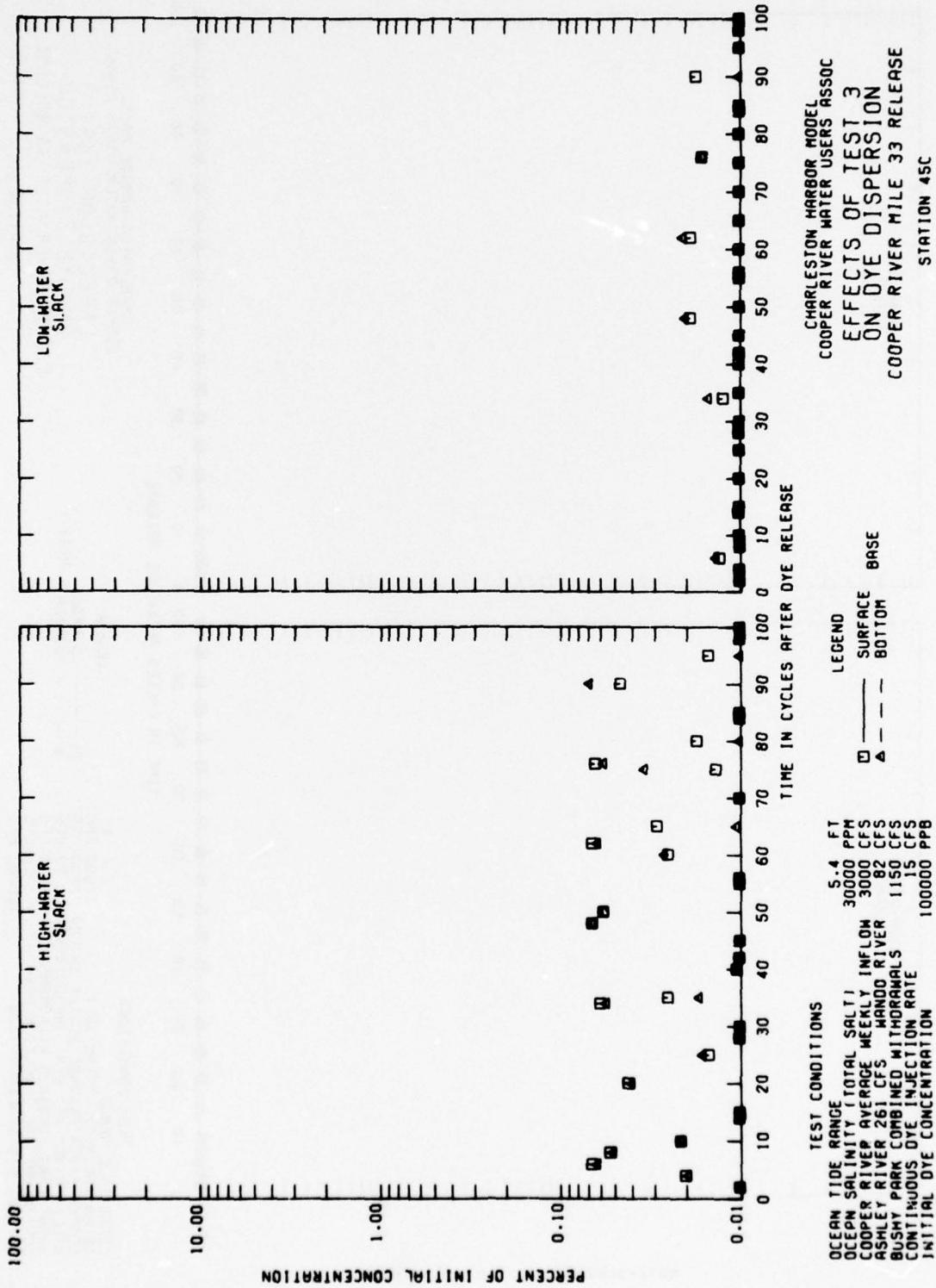












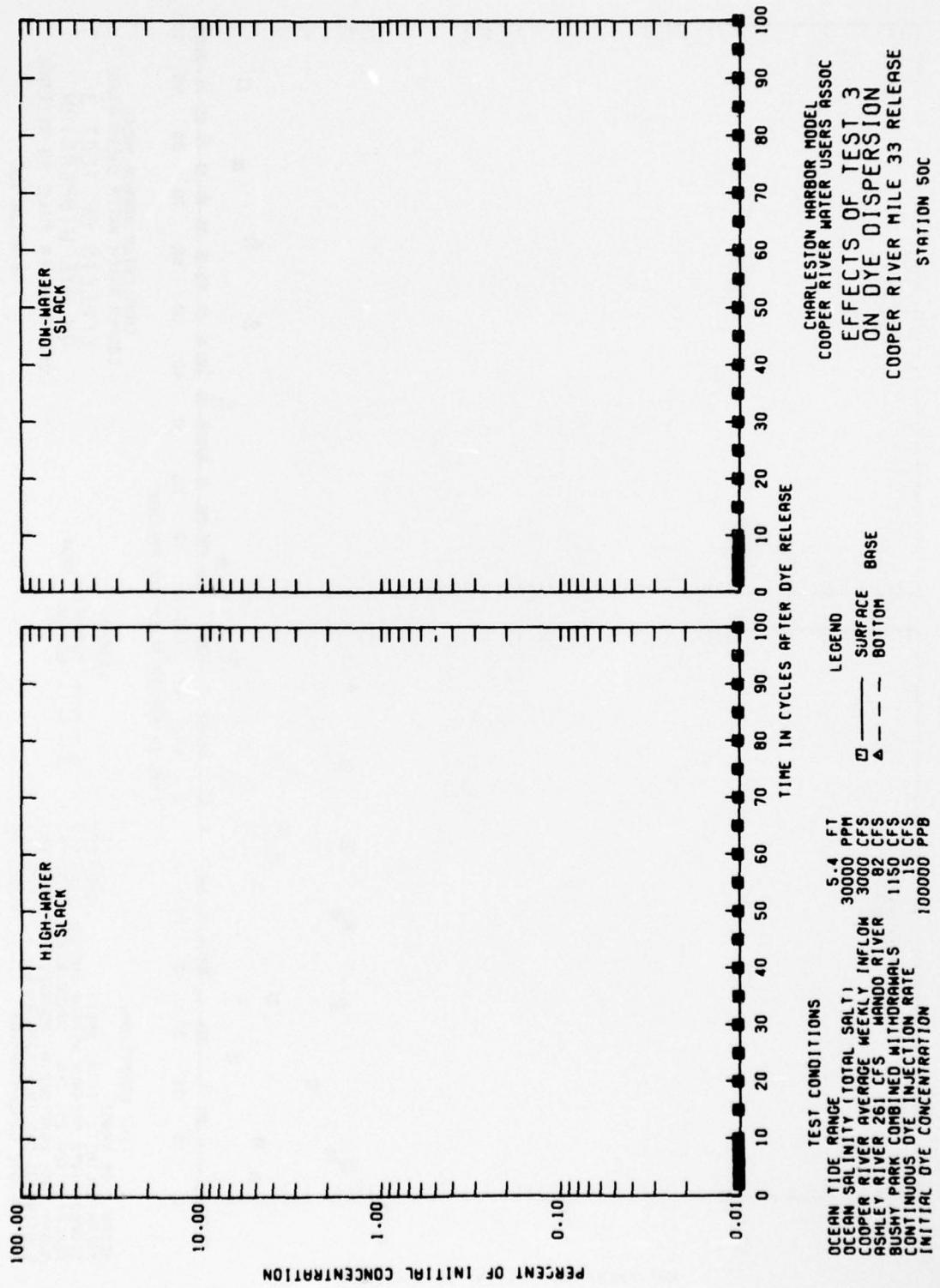
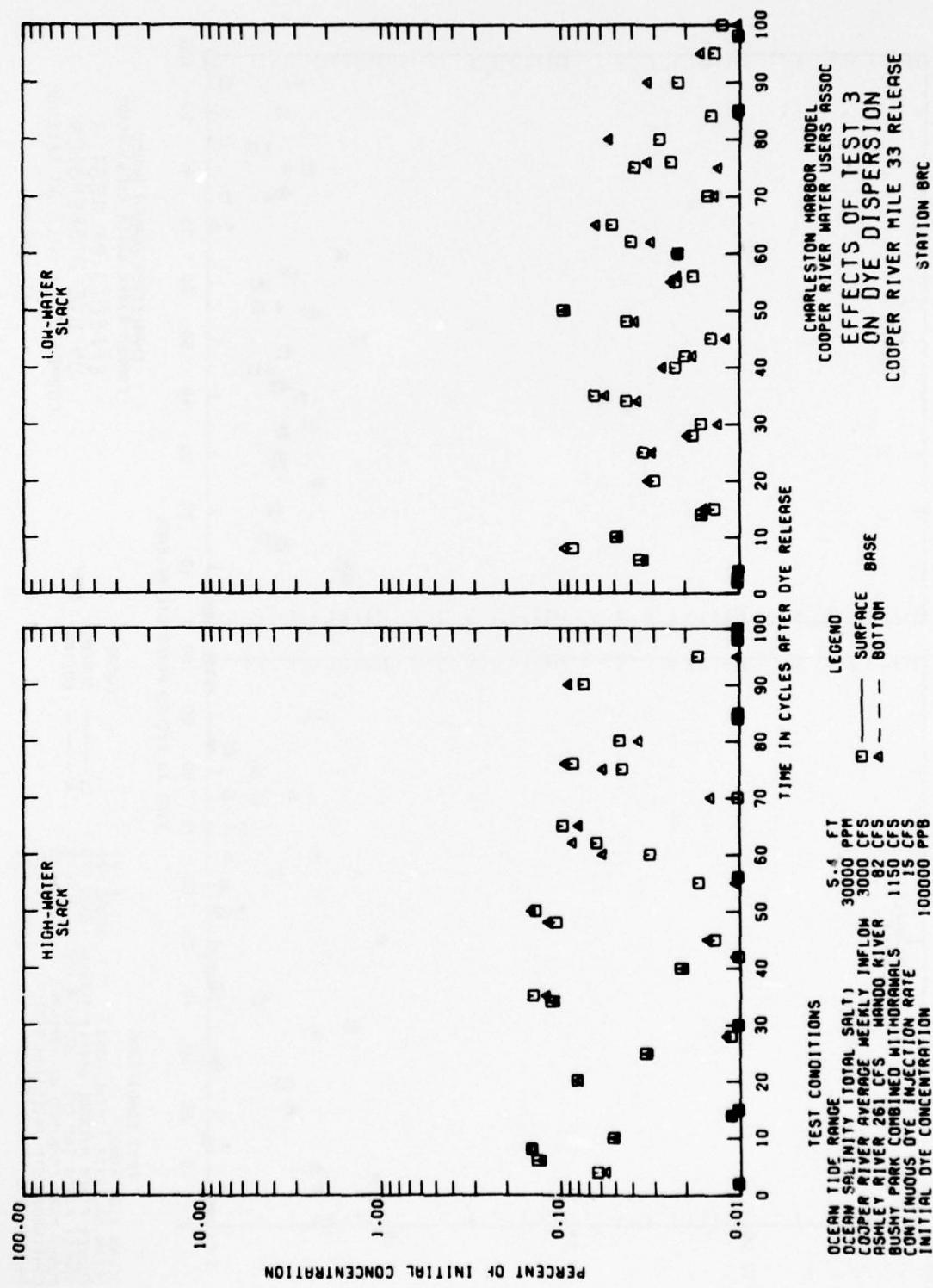


PLATE 50



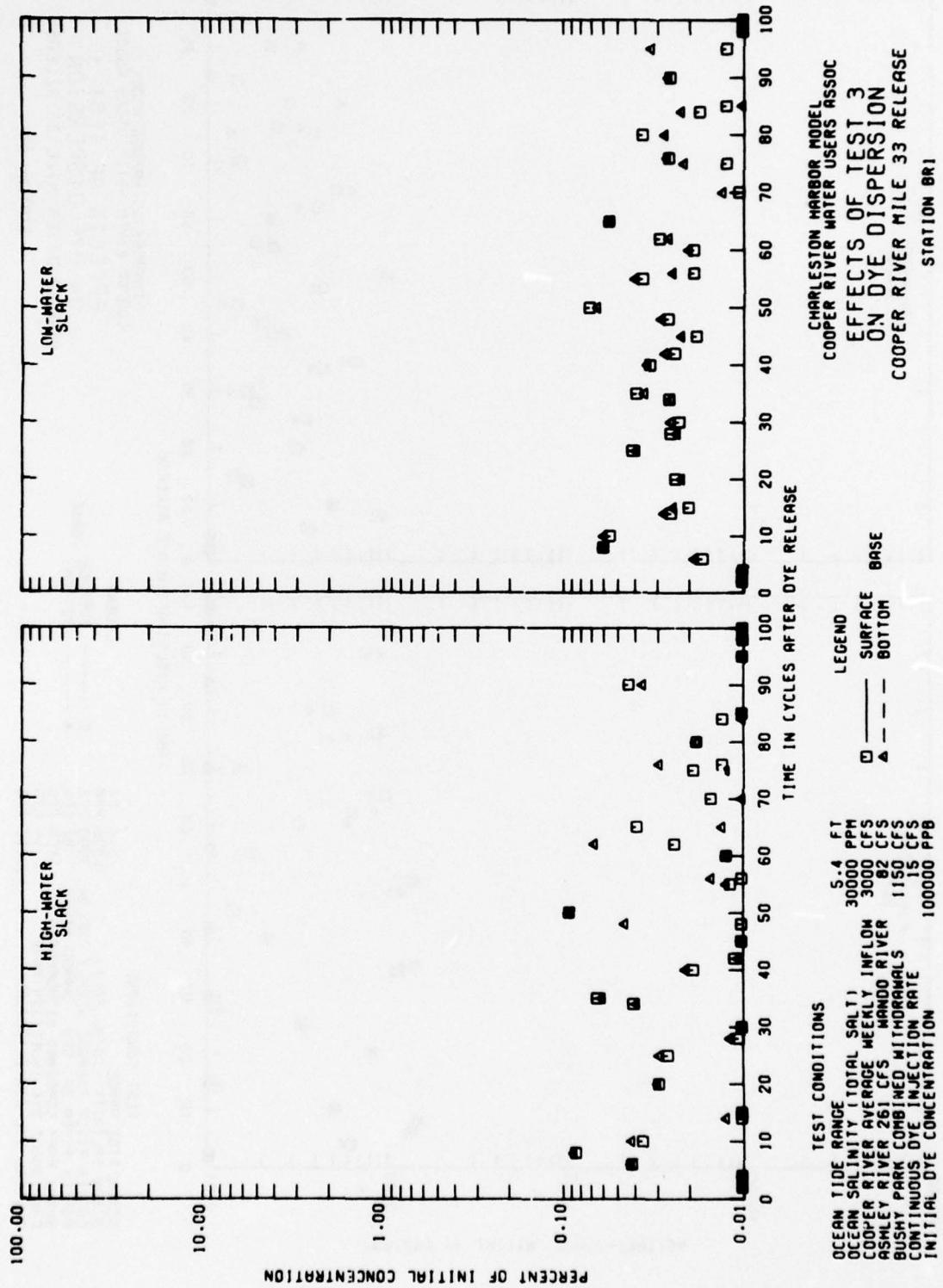
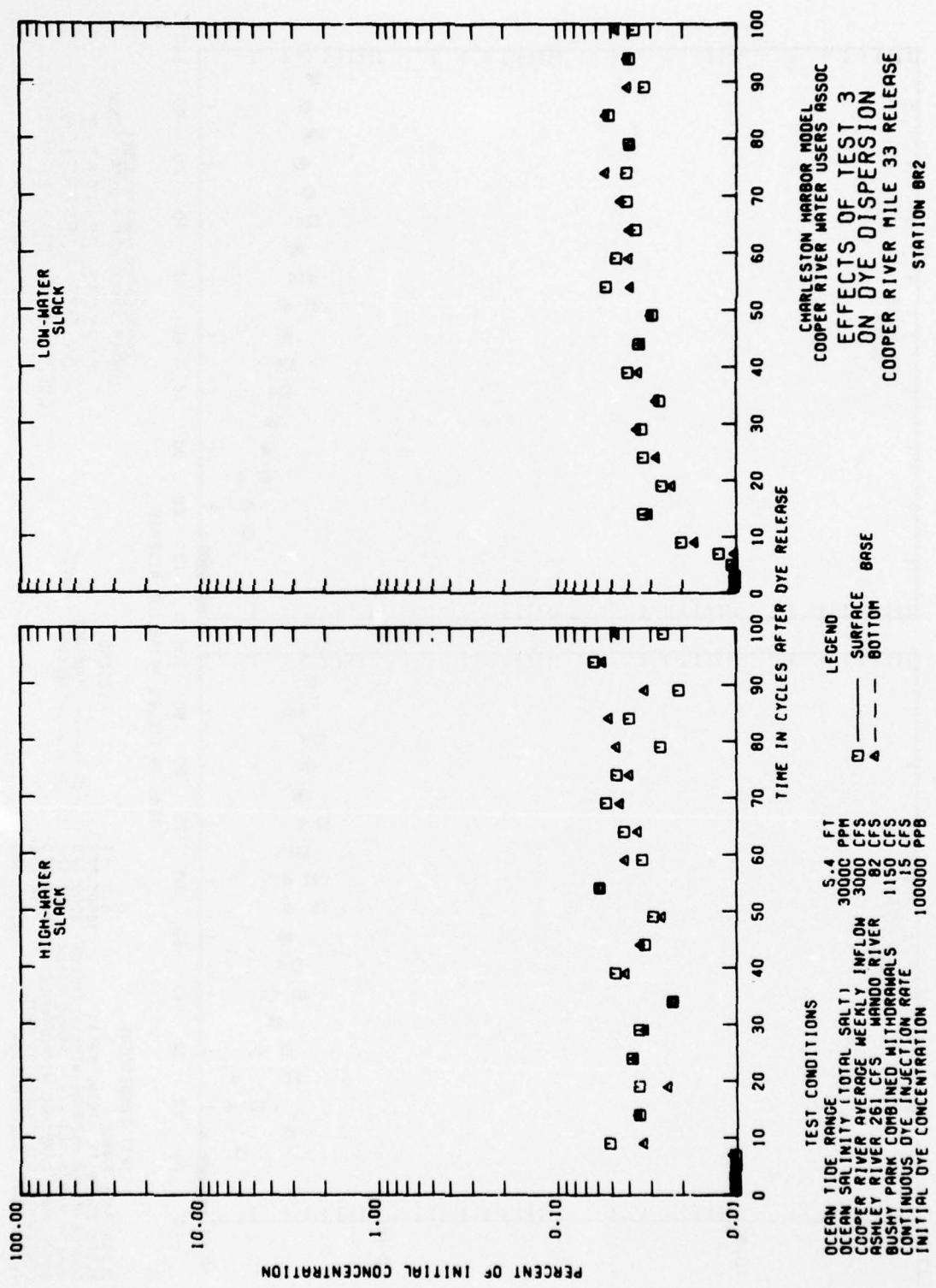


PLATE 52



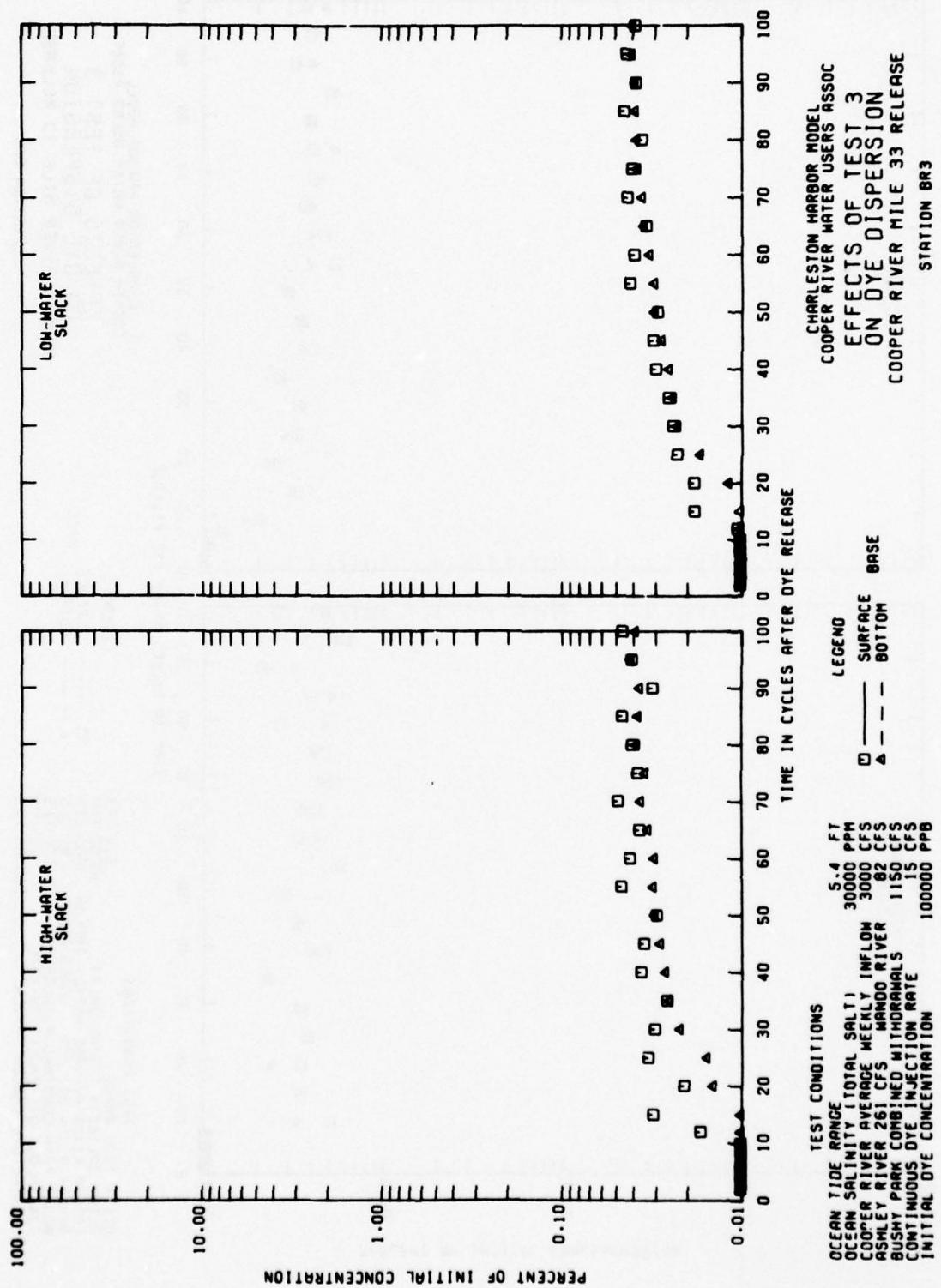
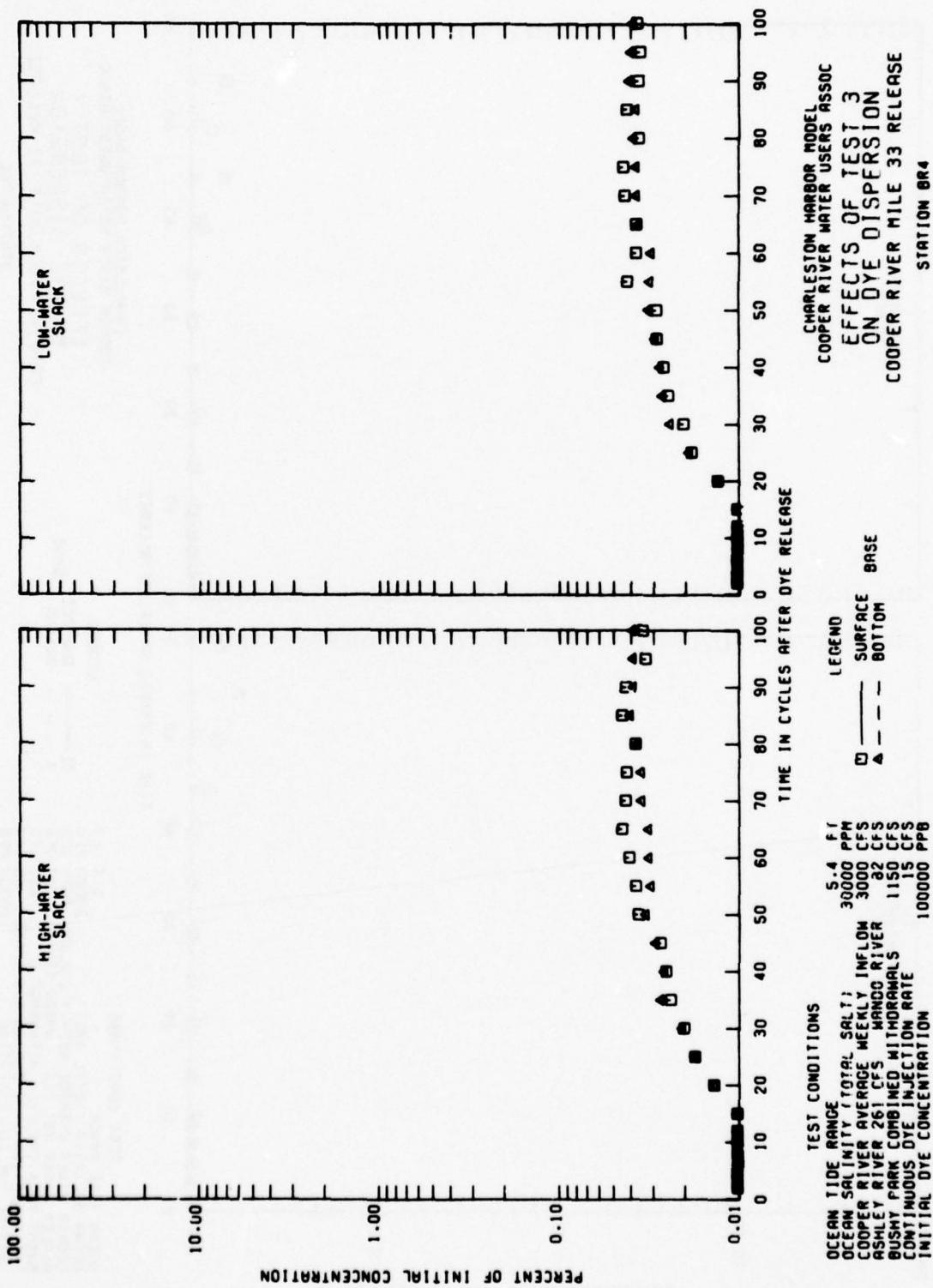
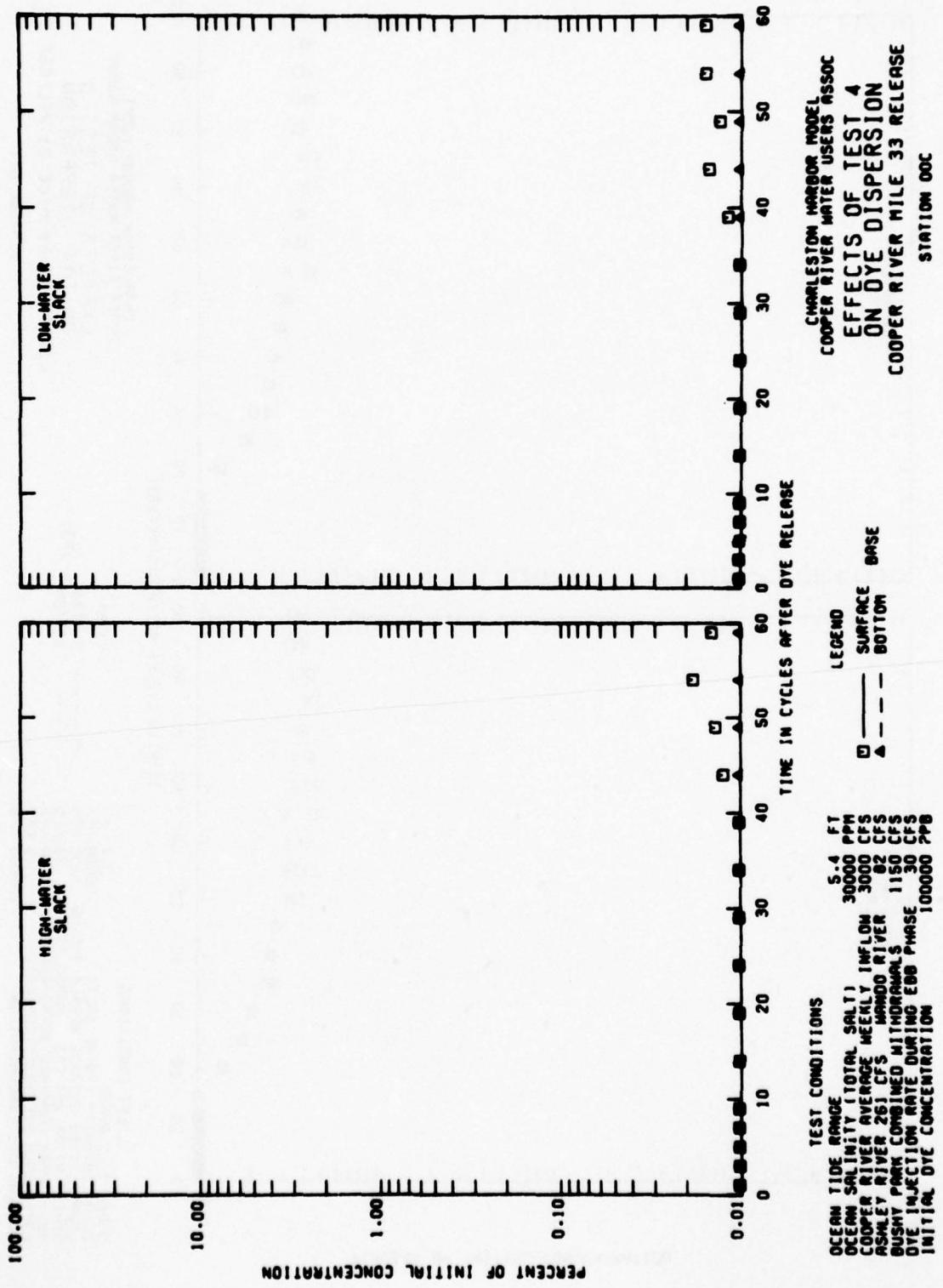
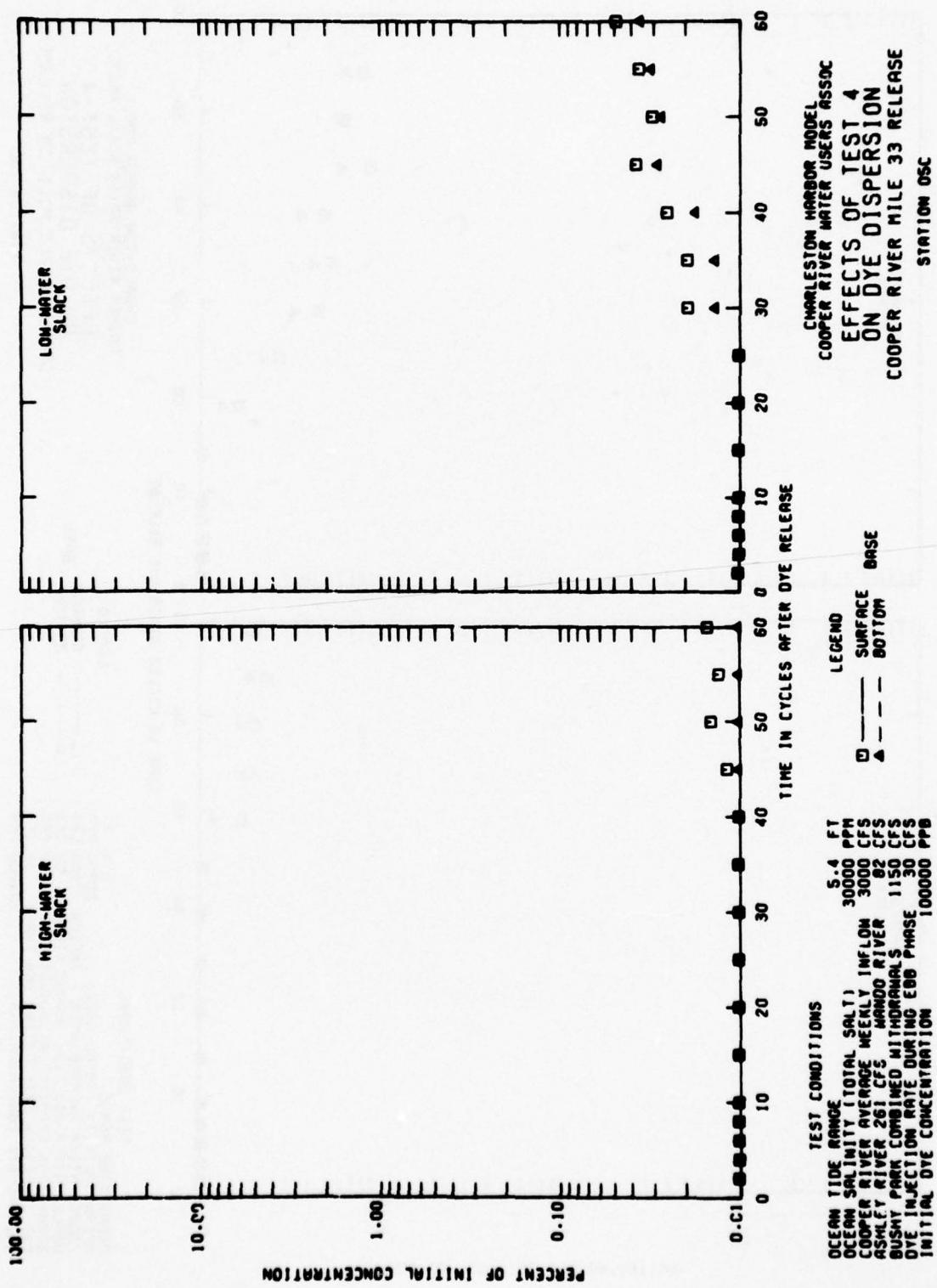


PLATE 54







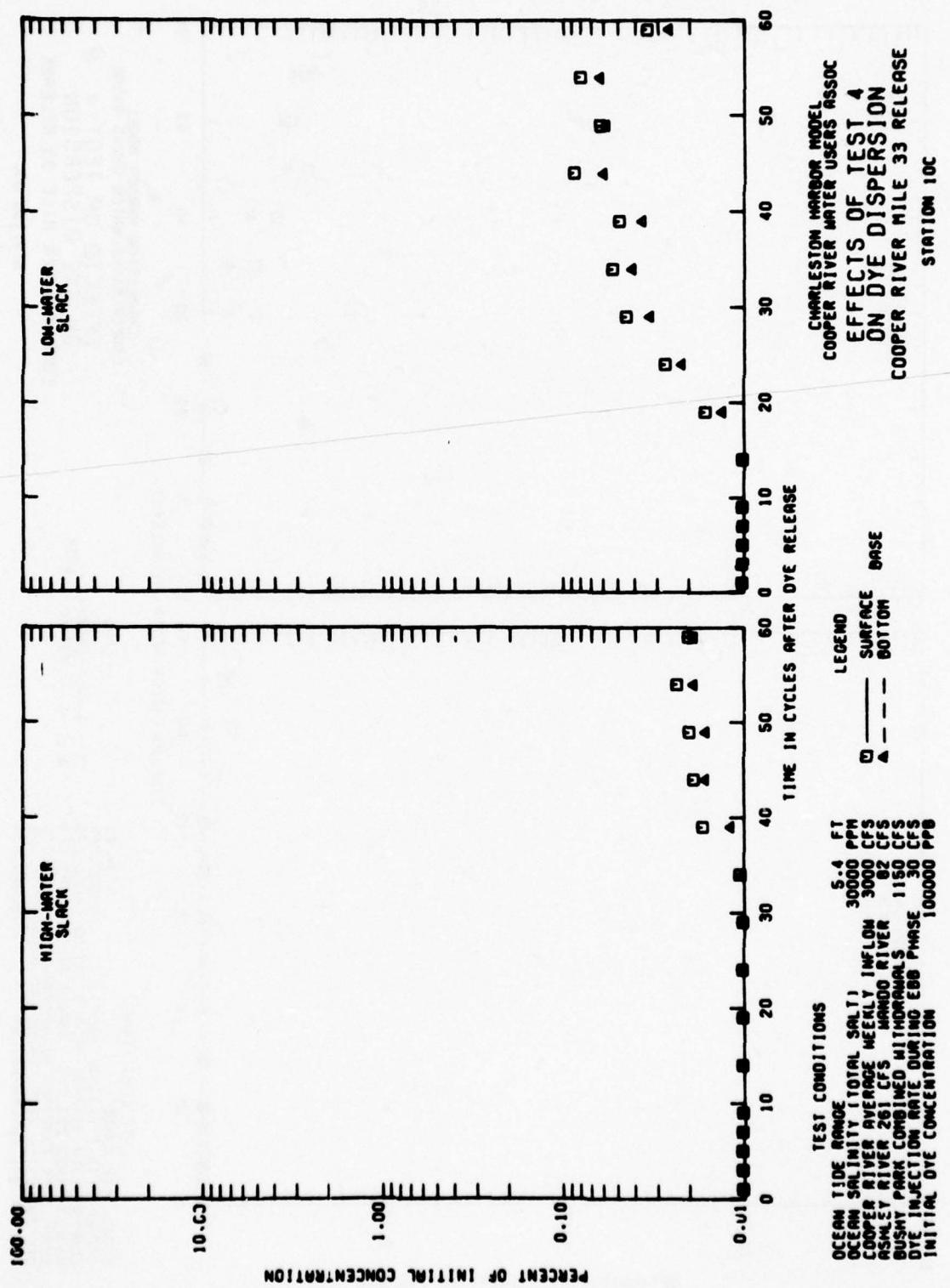
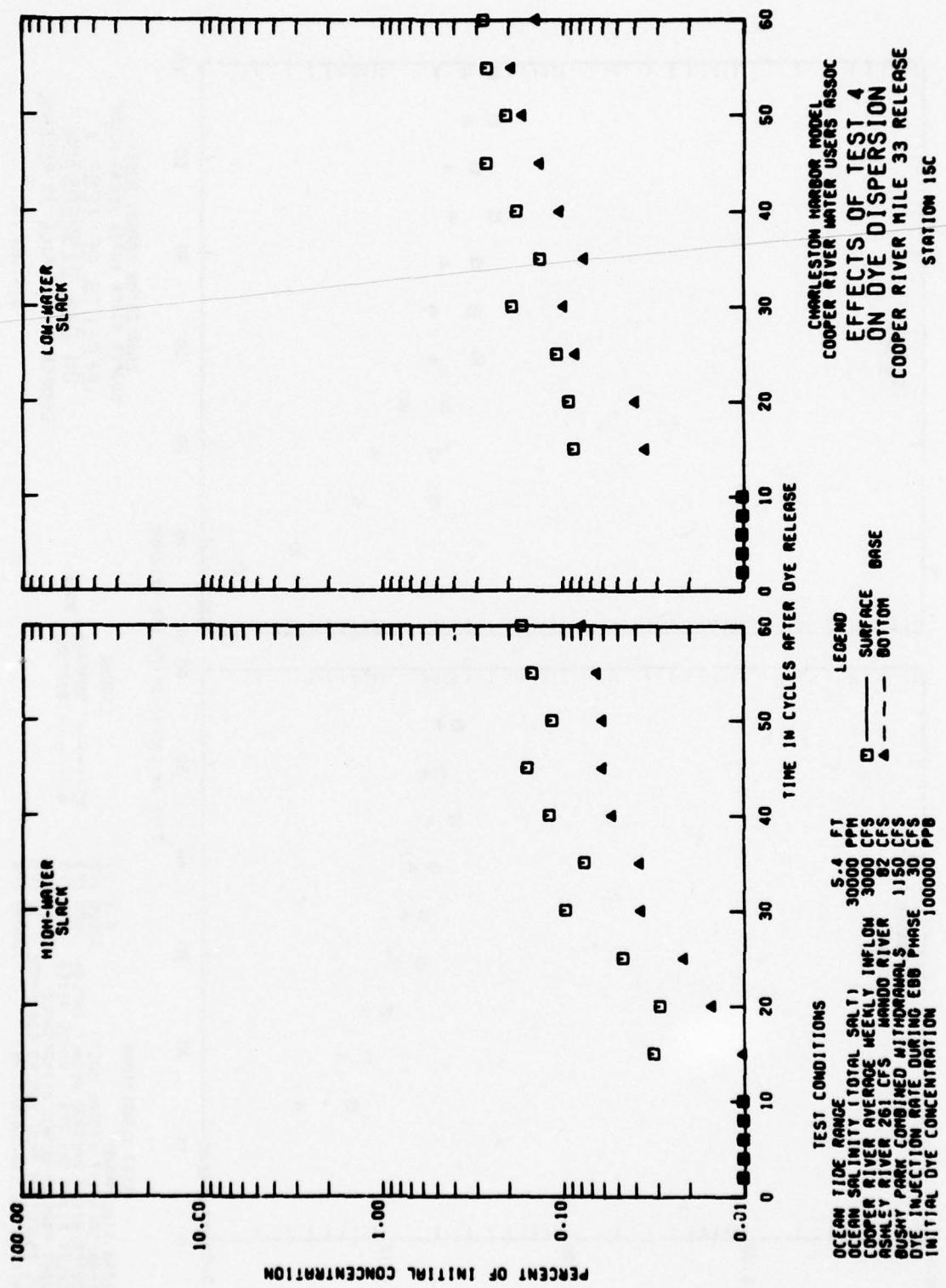
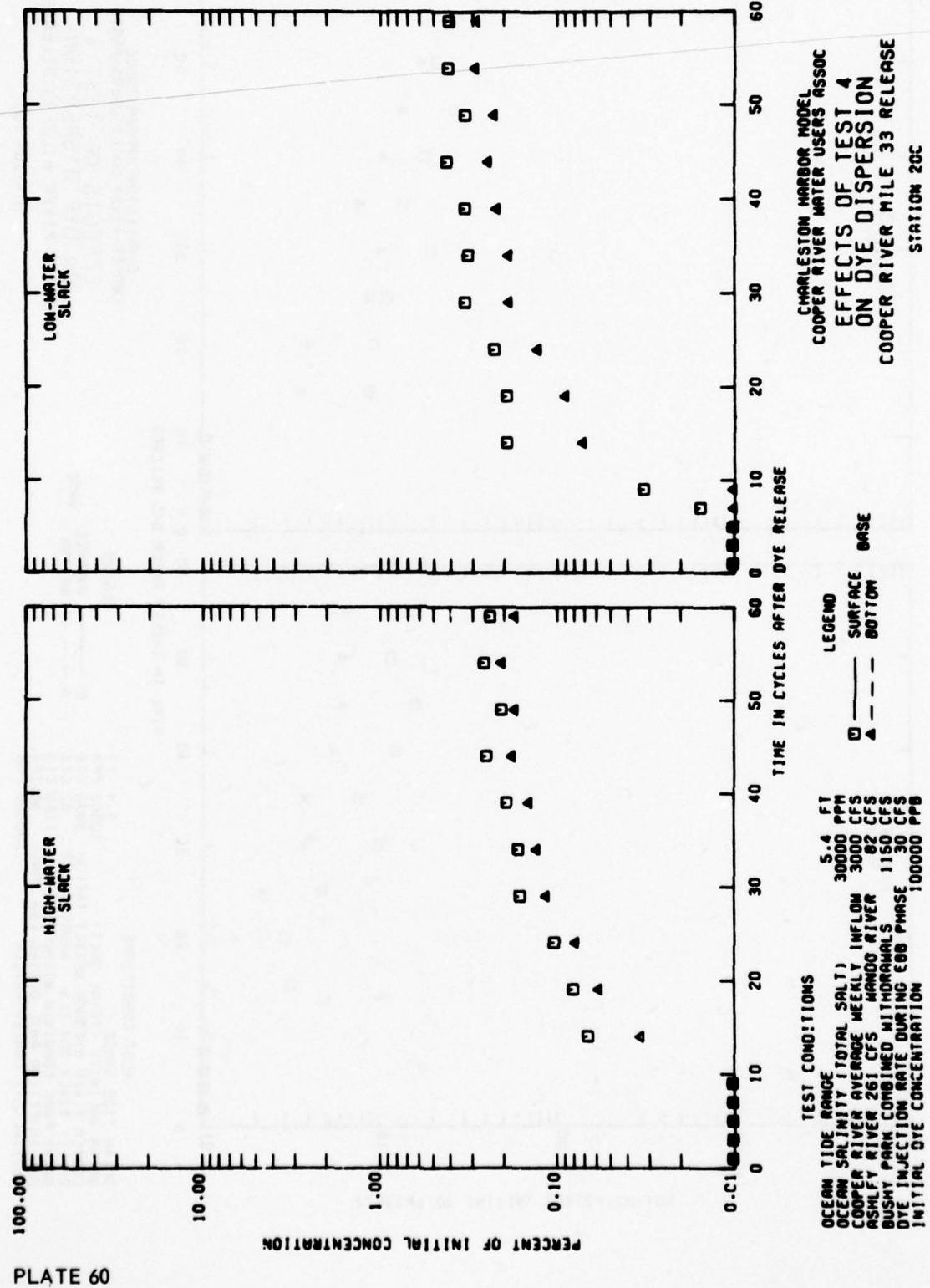
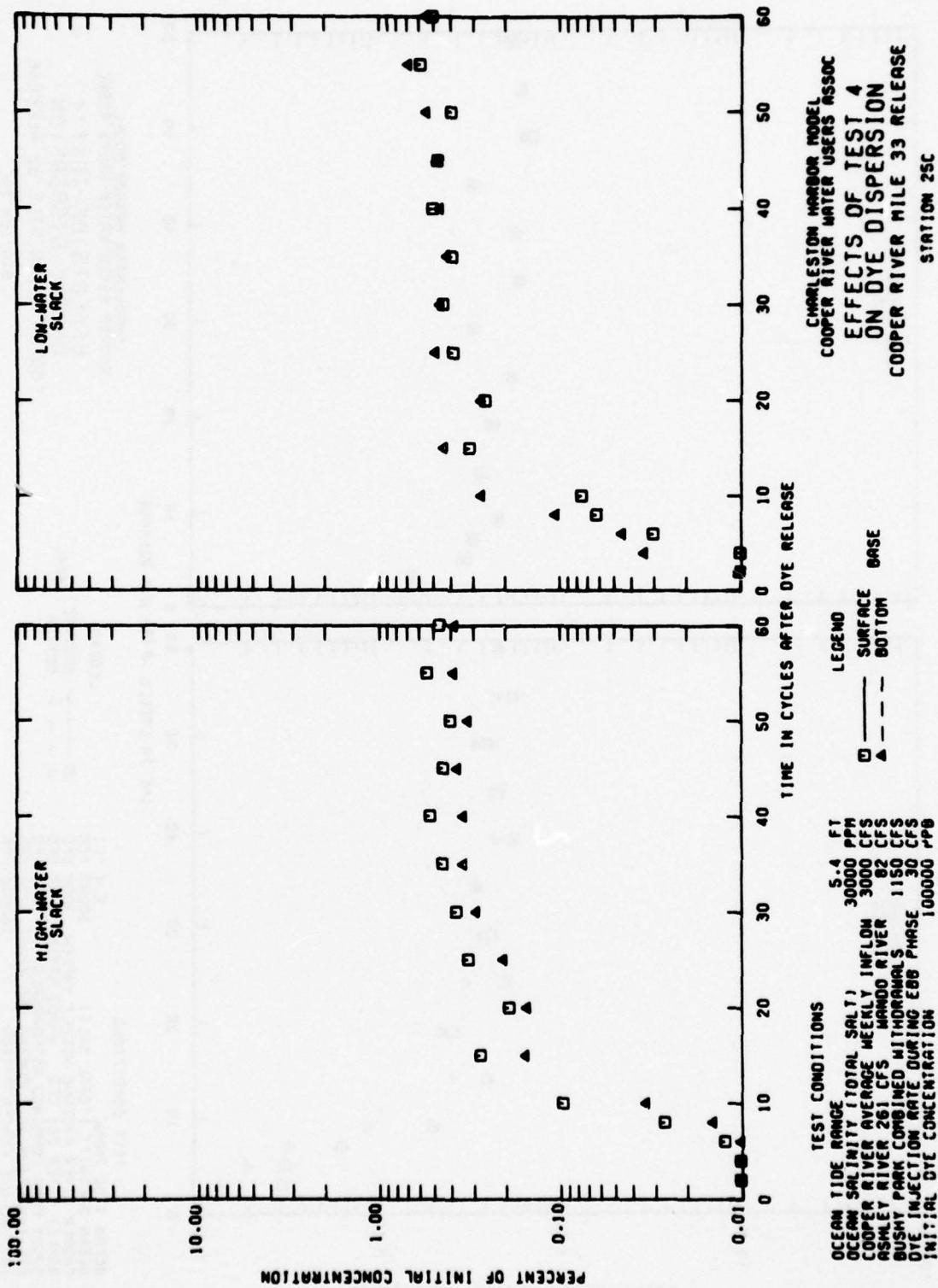
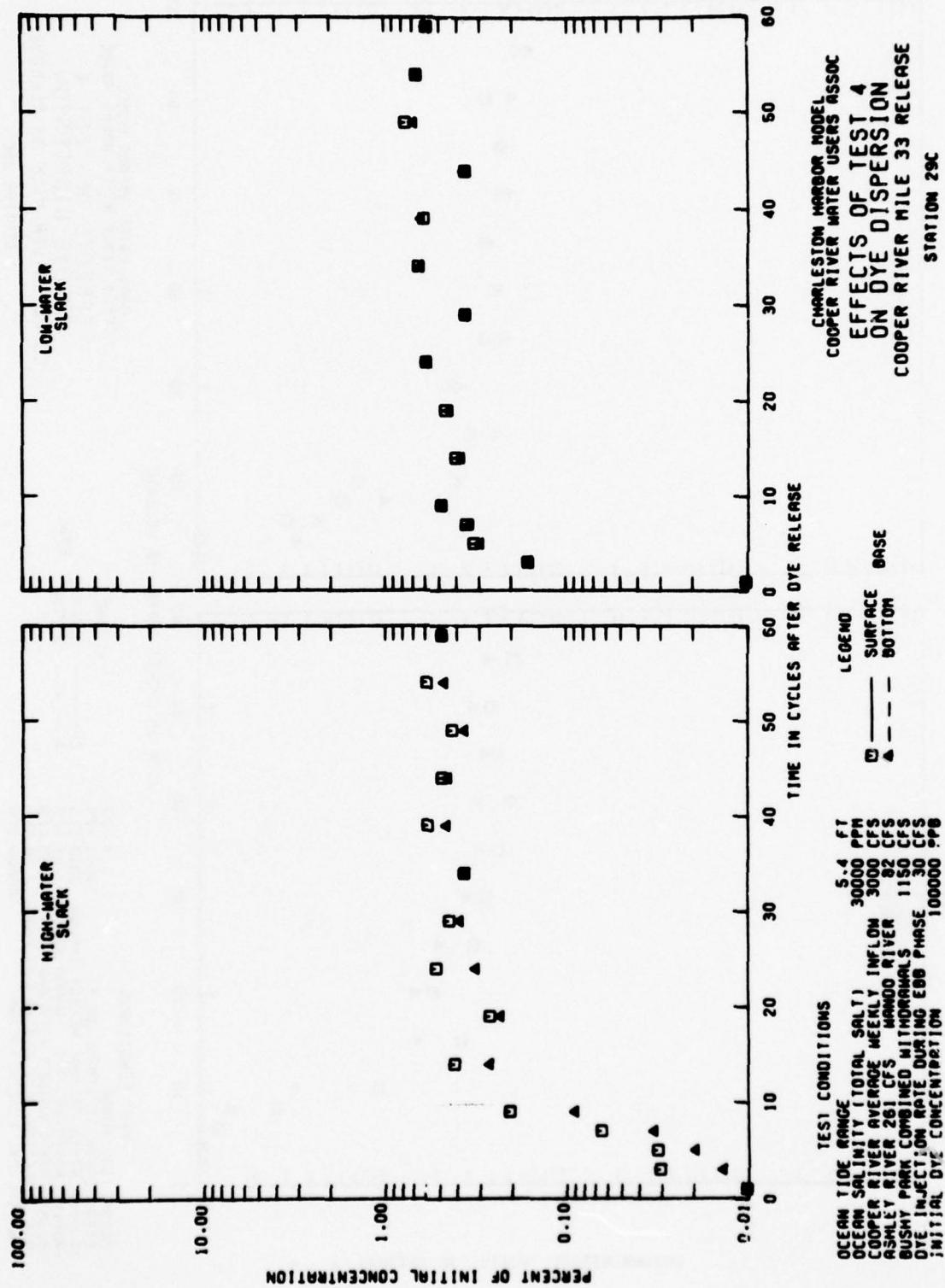


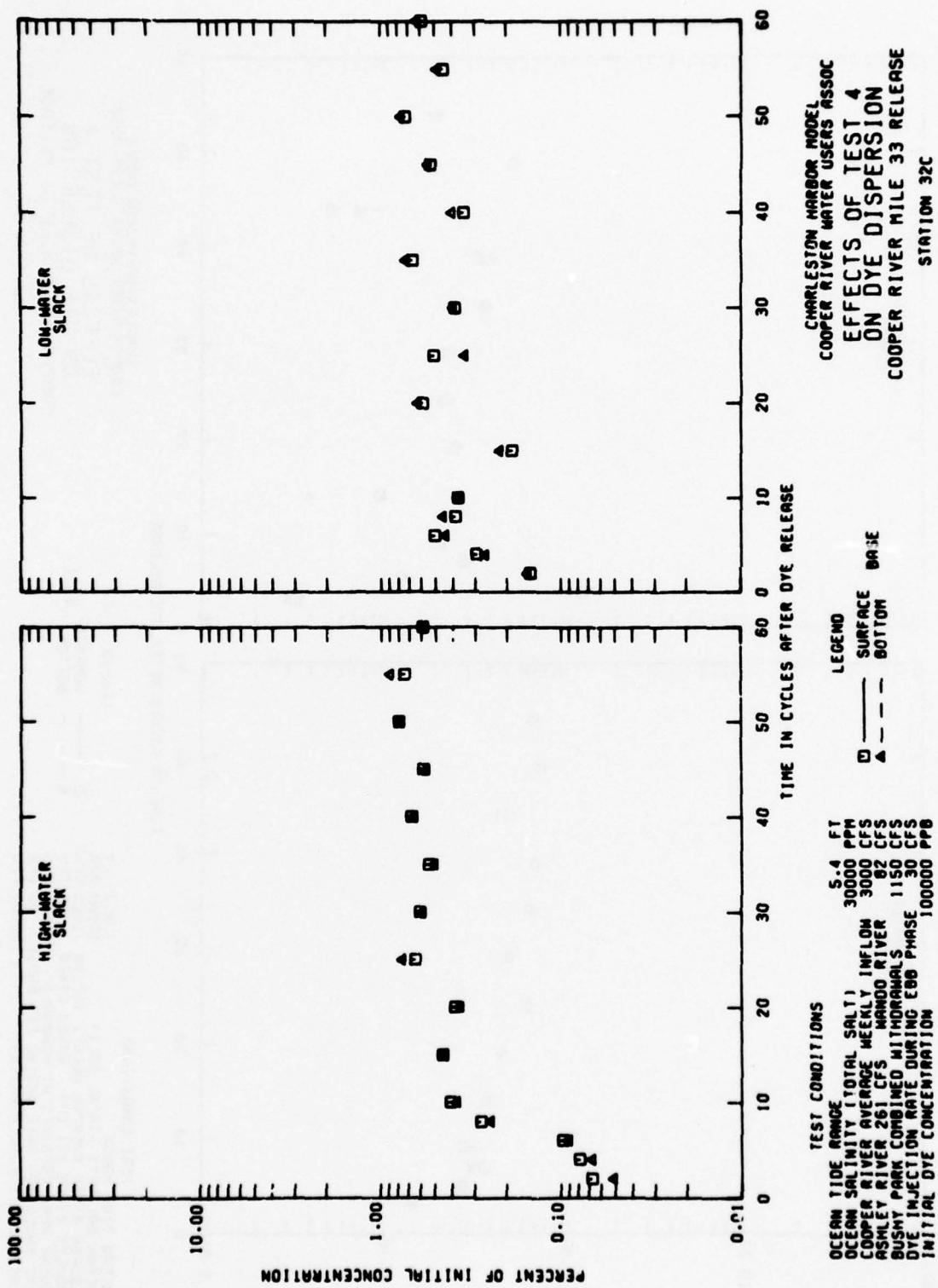
PLATE 58











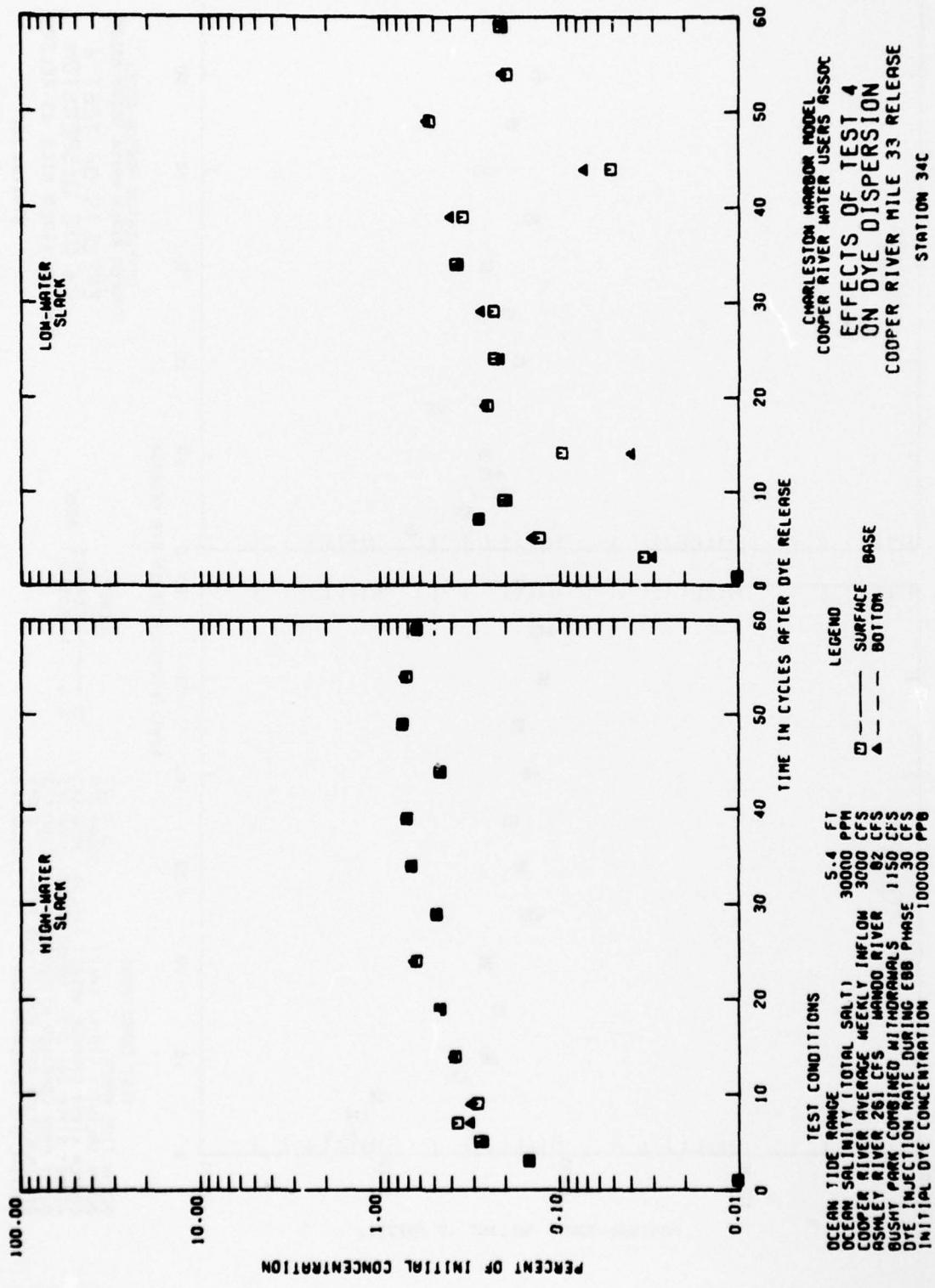
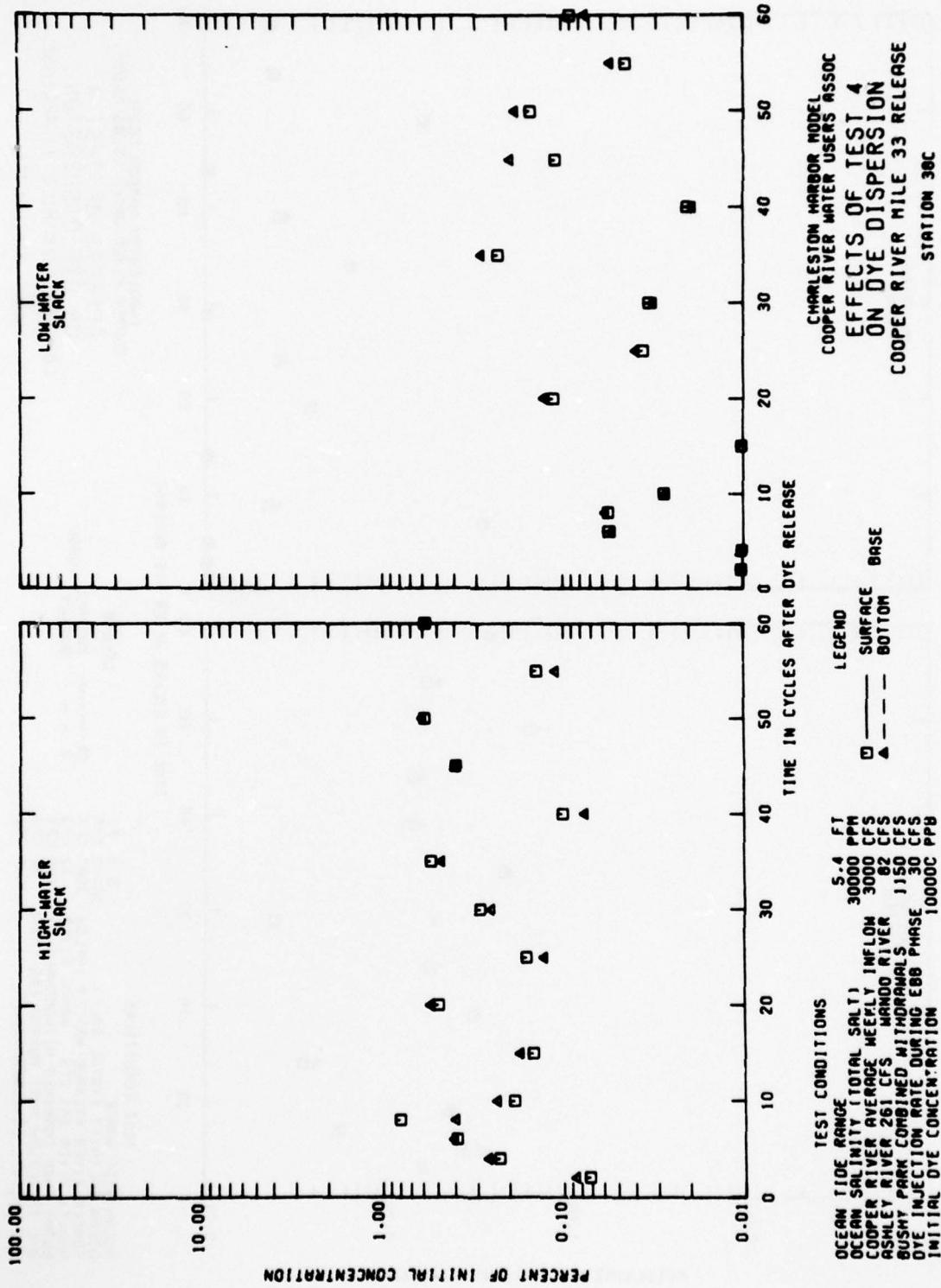


PLATE 64



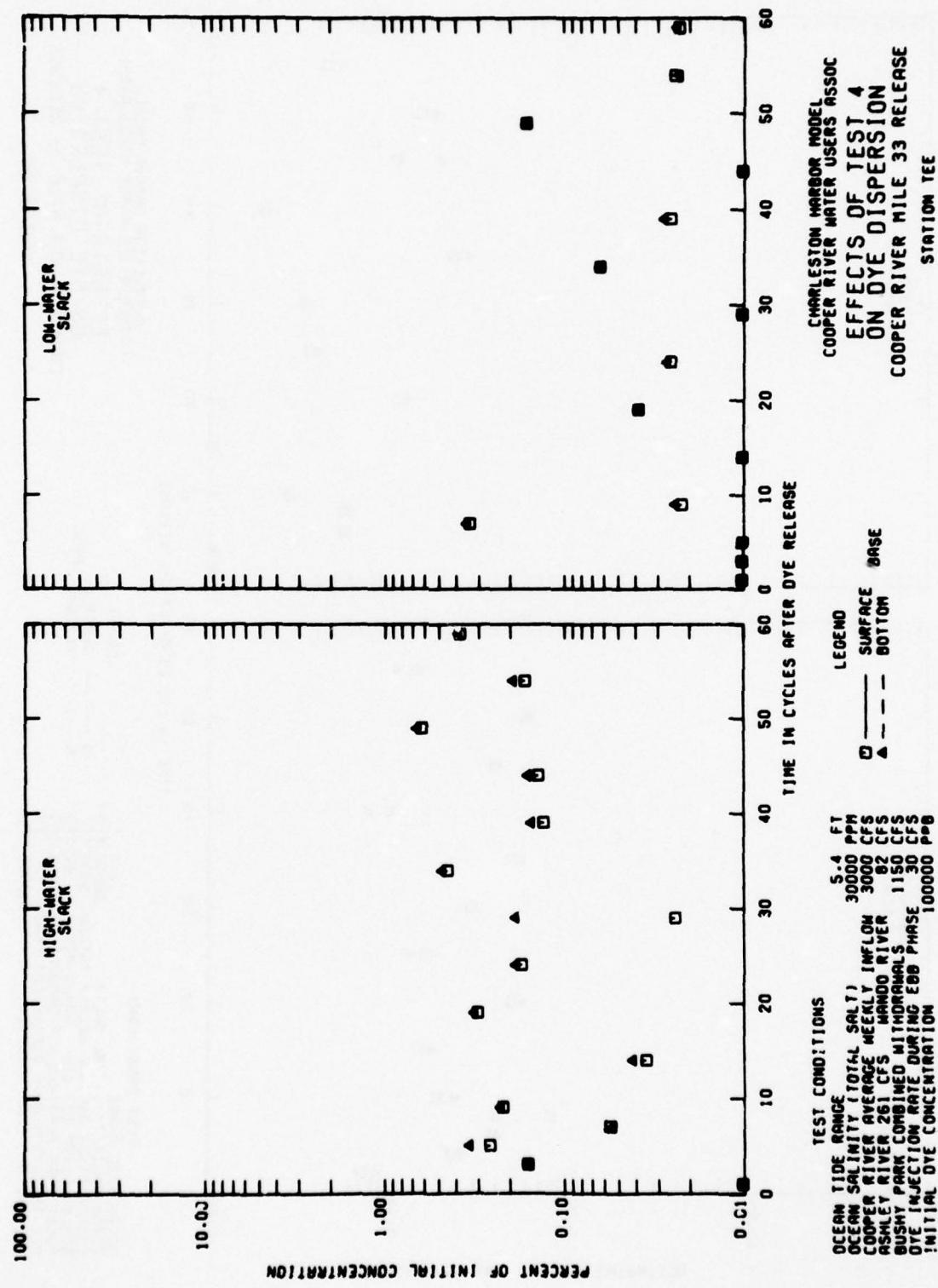
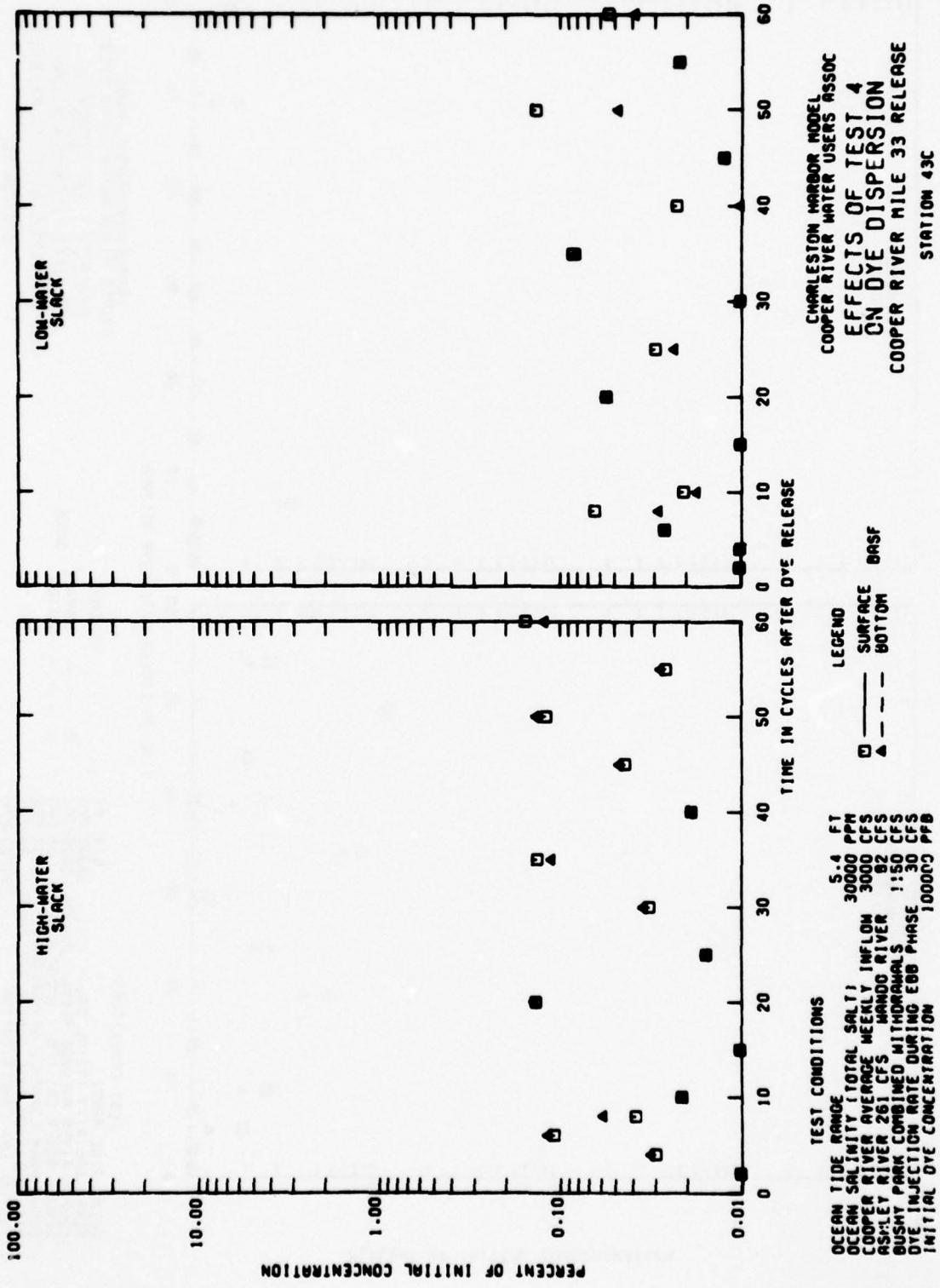
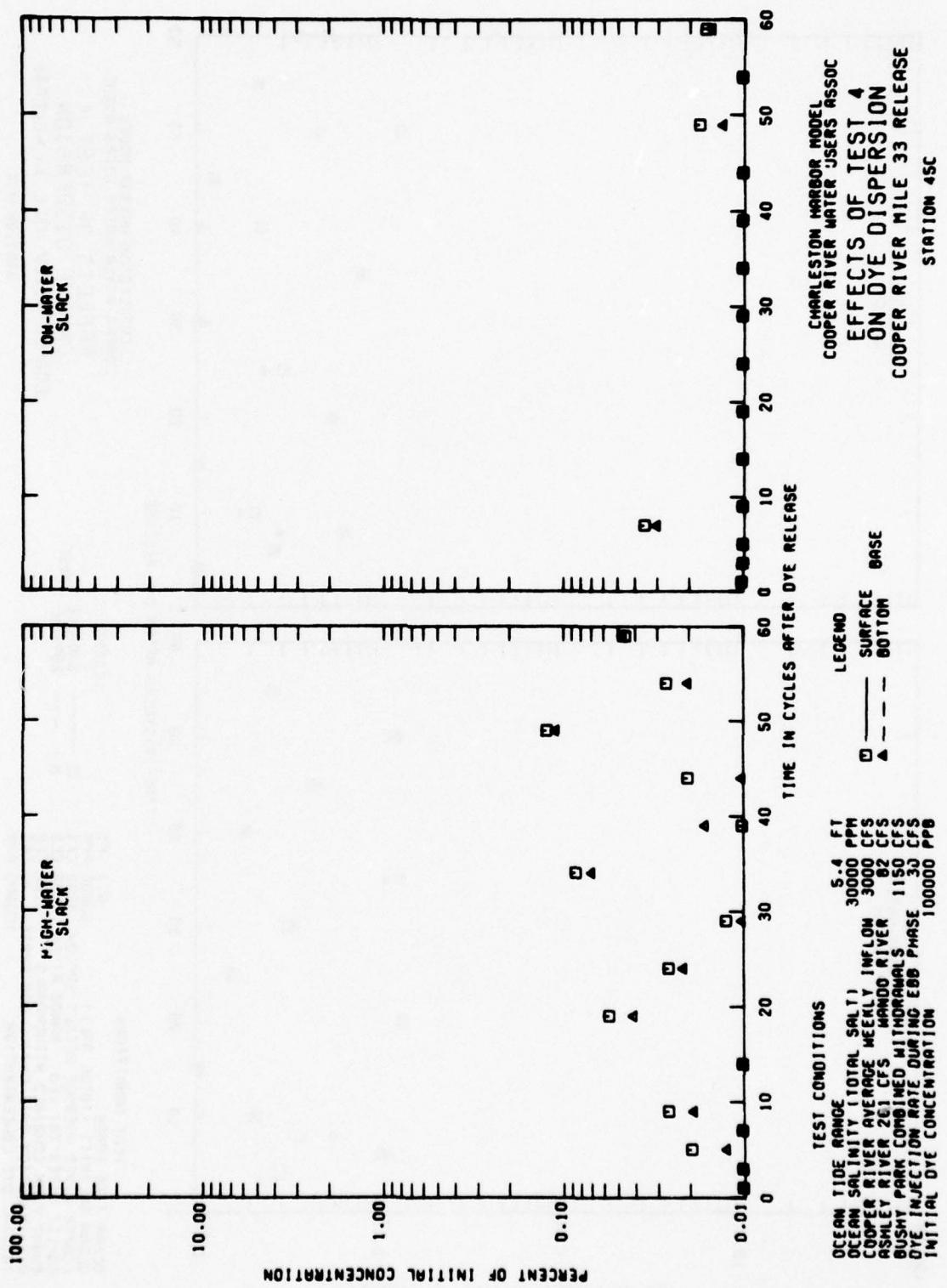
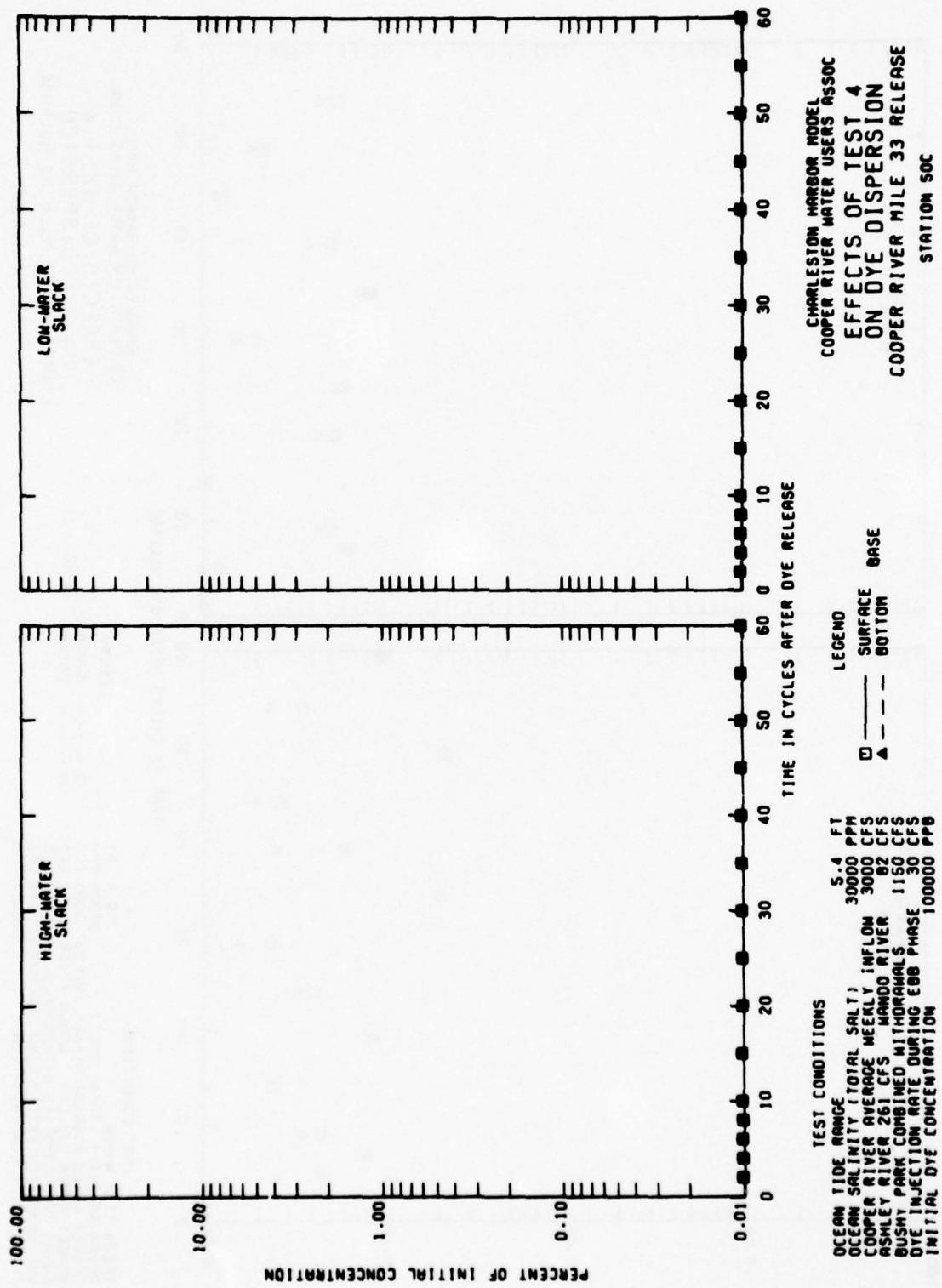


PLATE 66







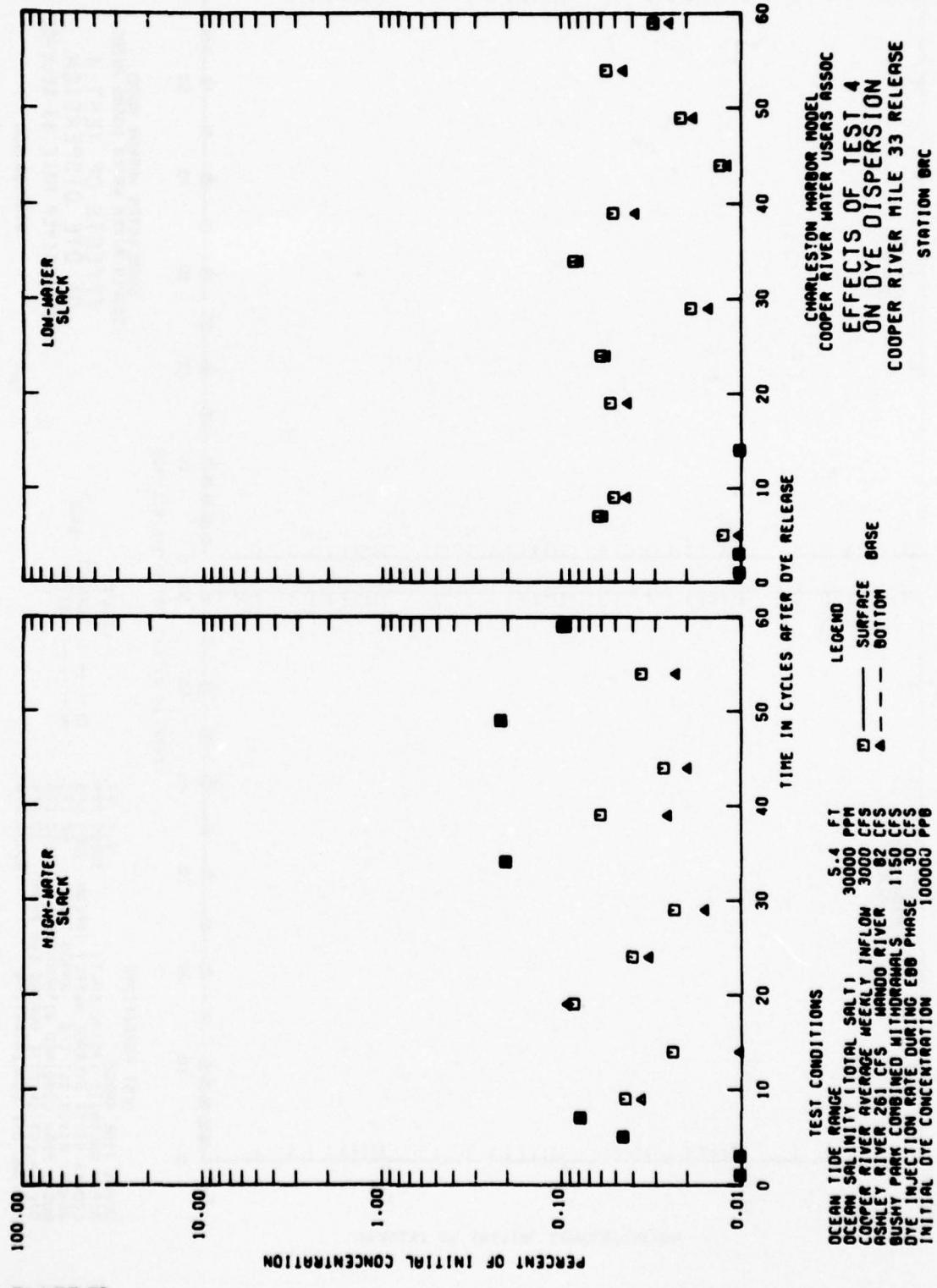
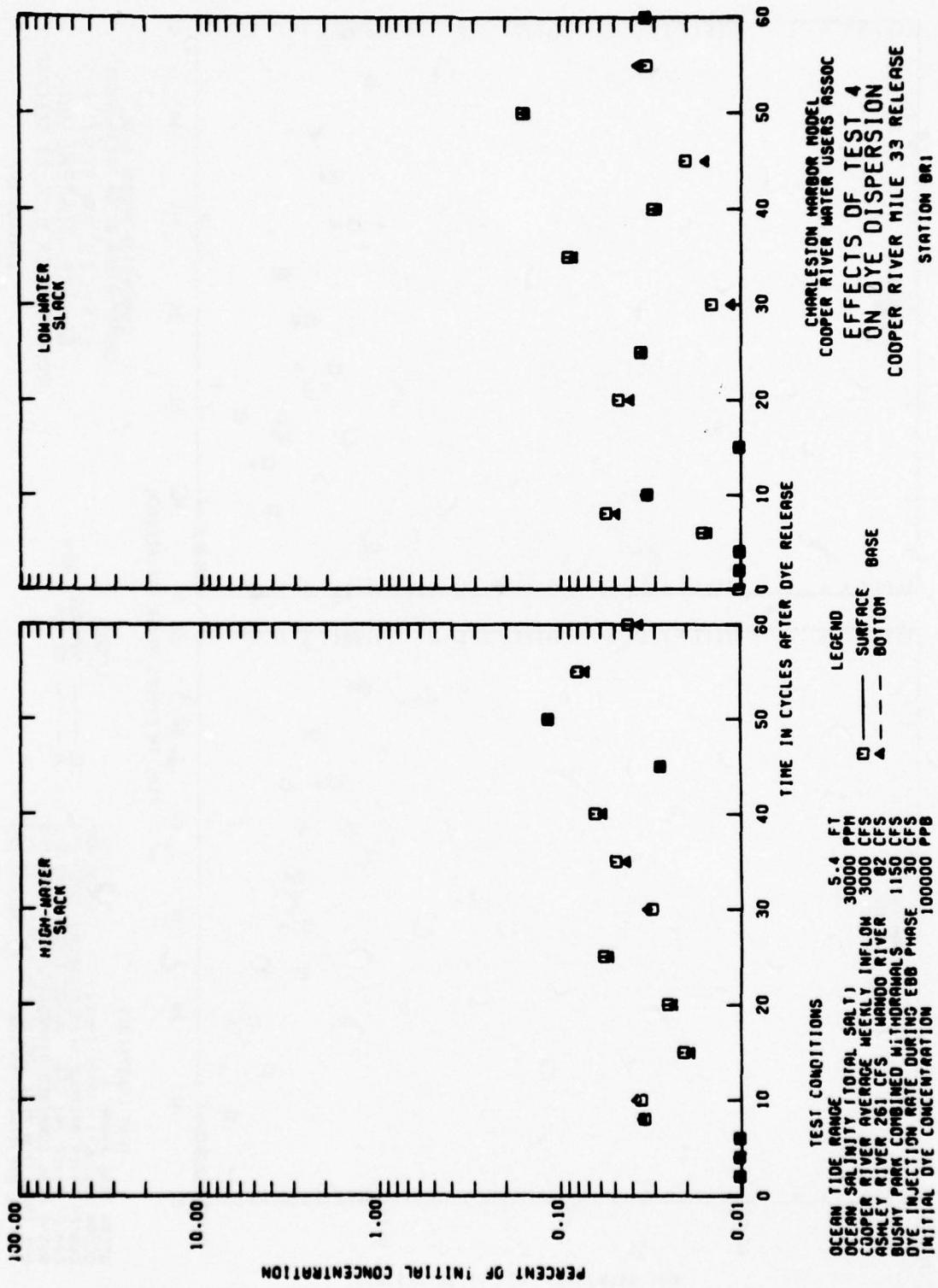
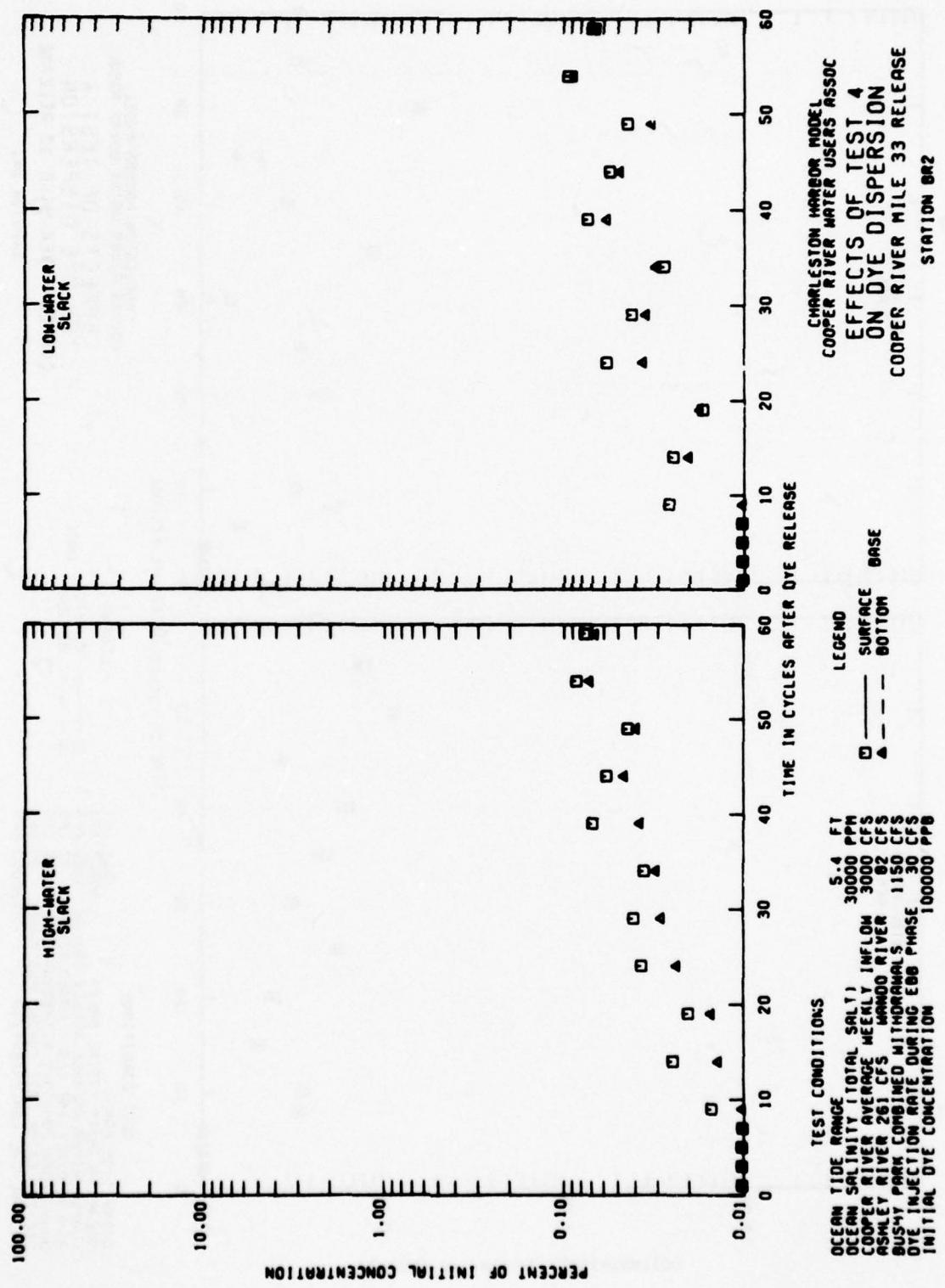
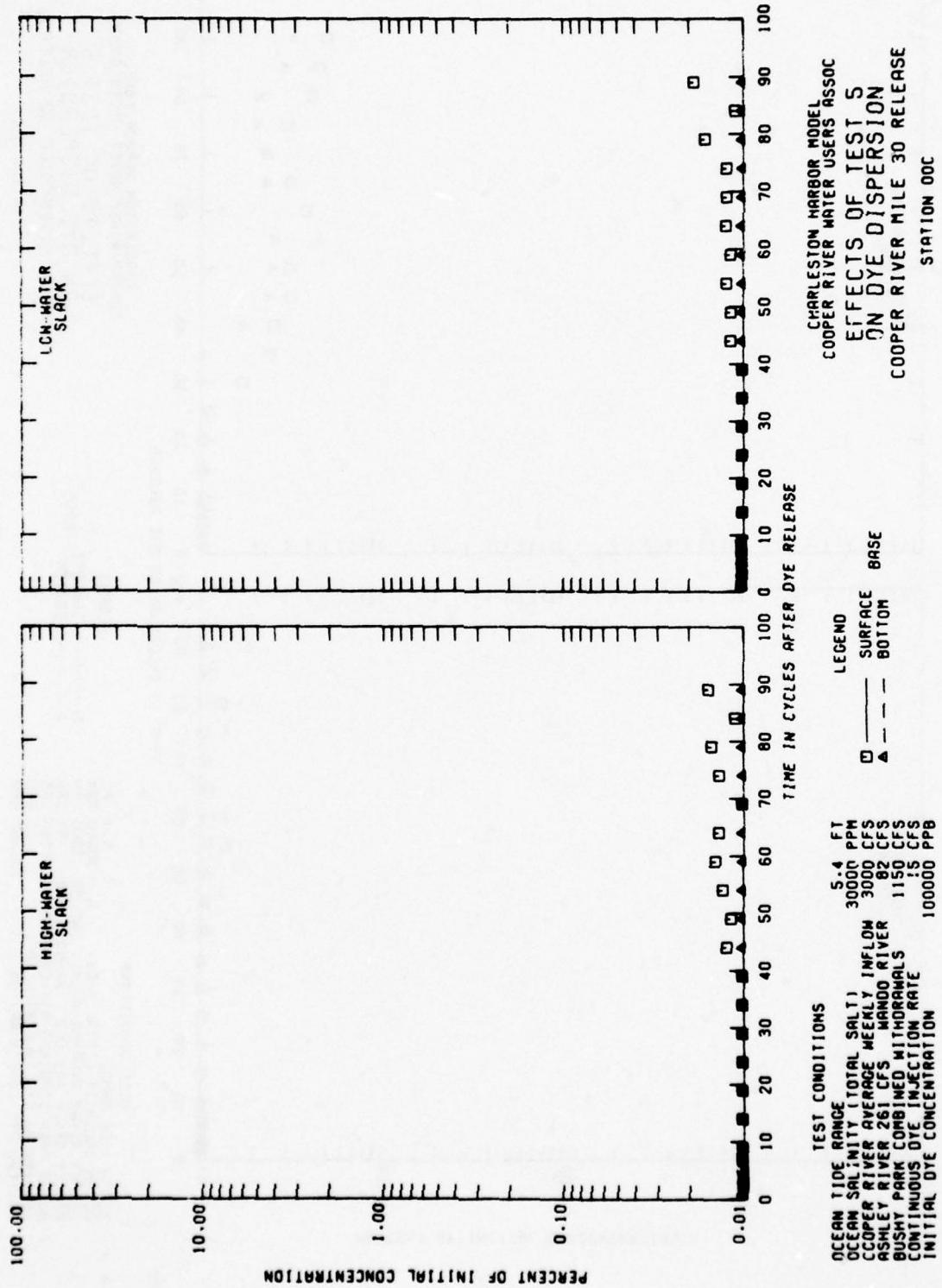
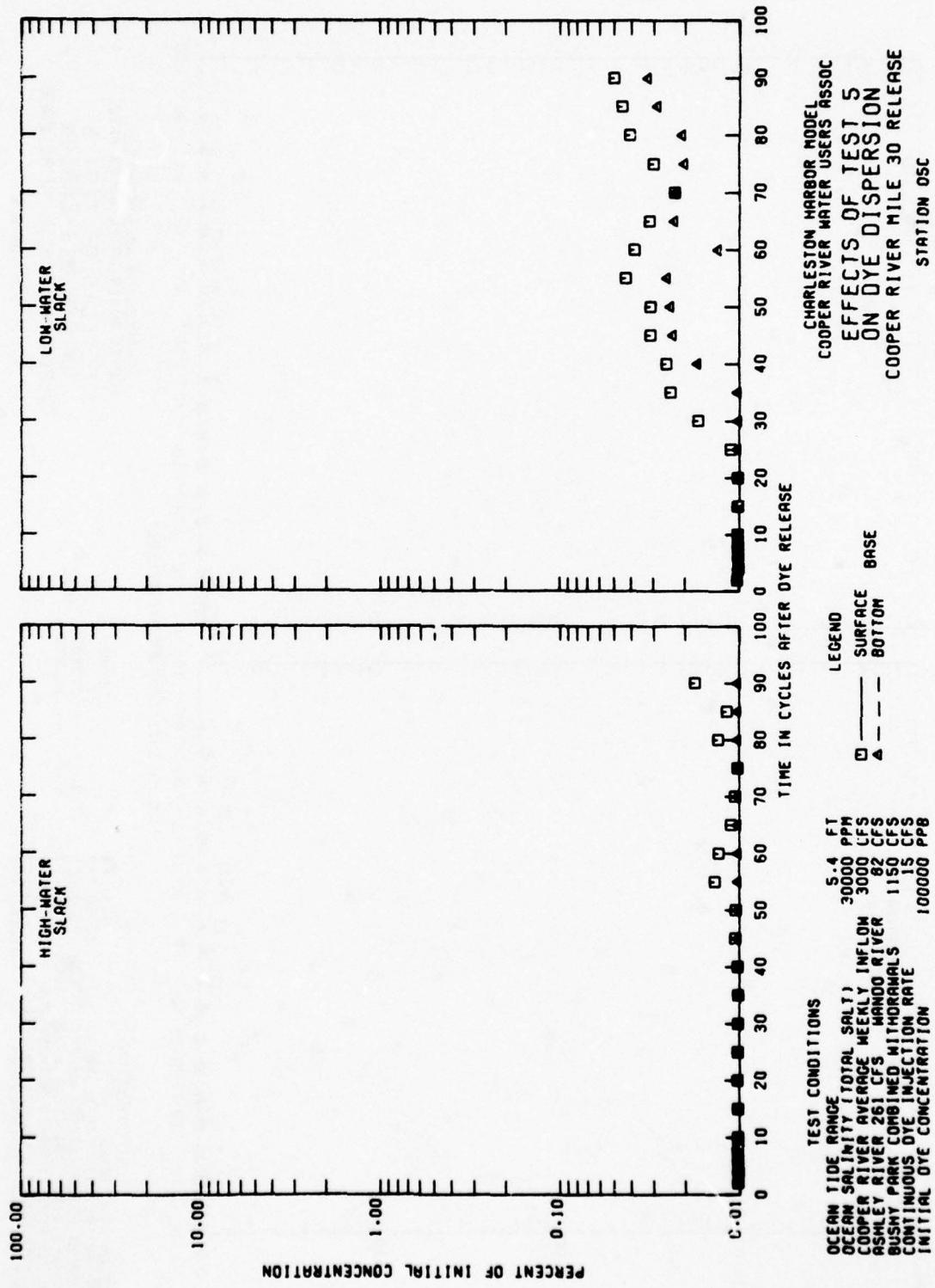


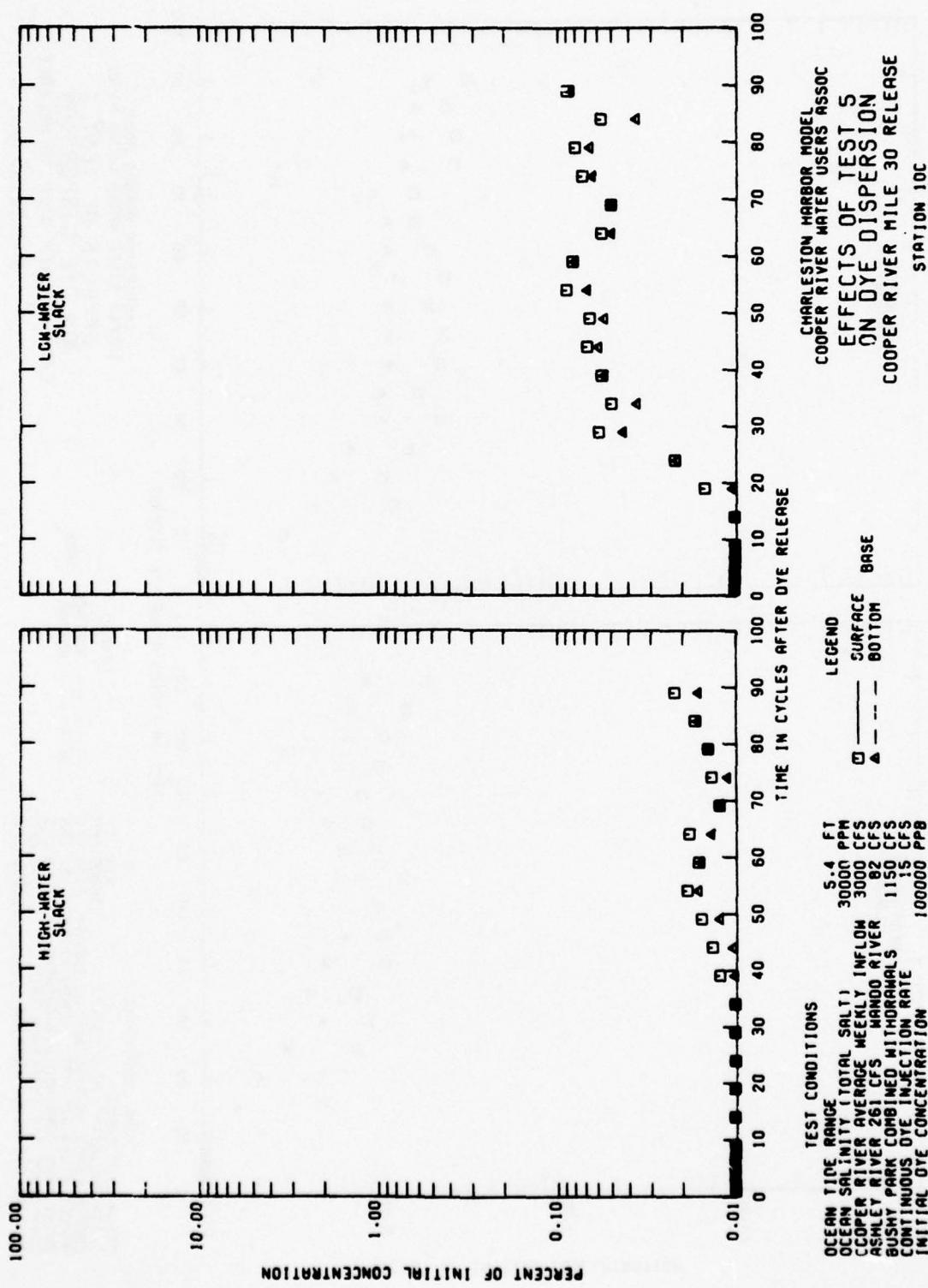
PLATE 70

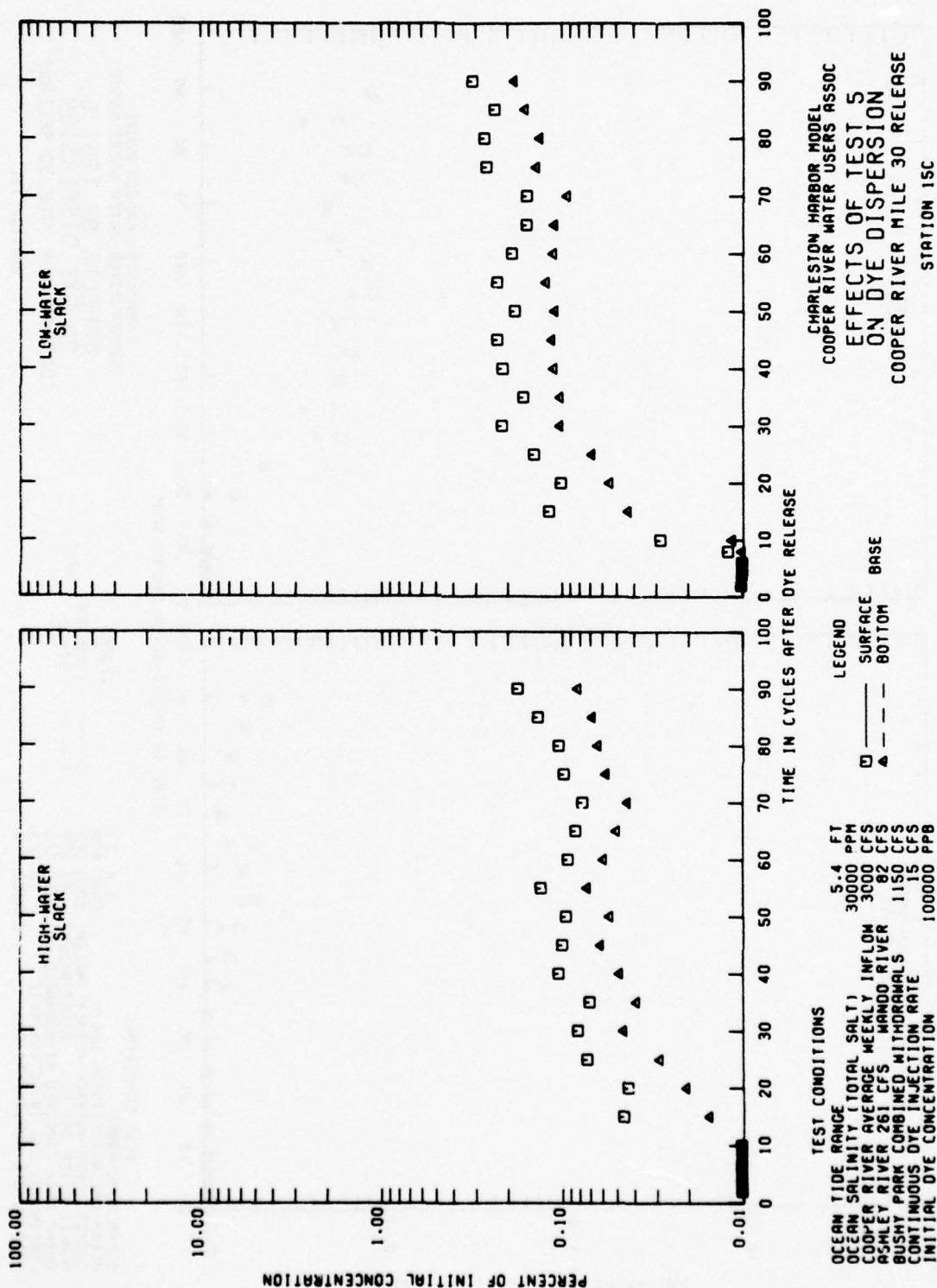


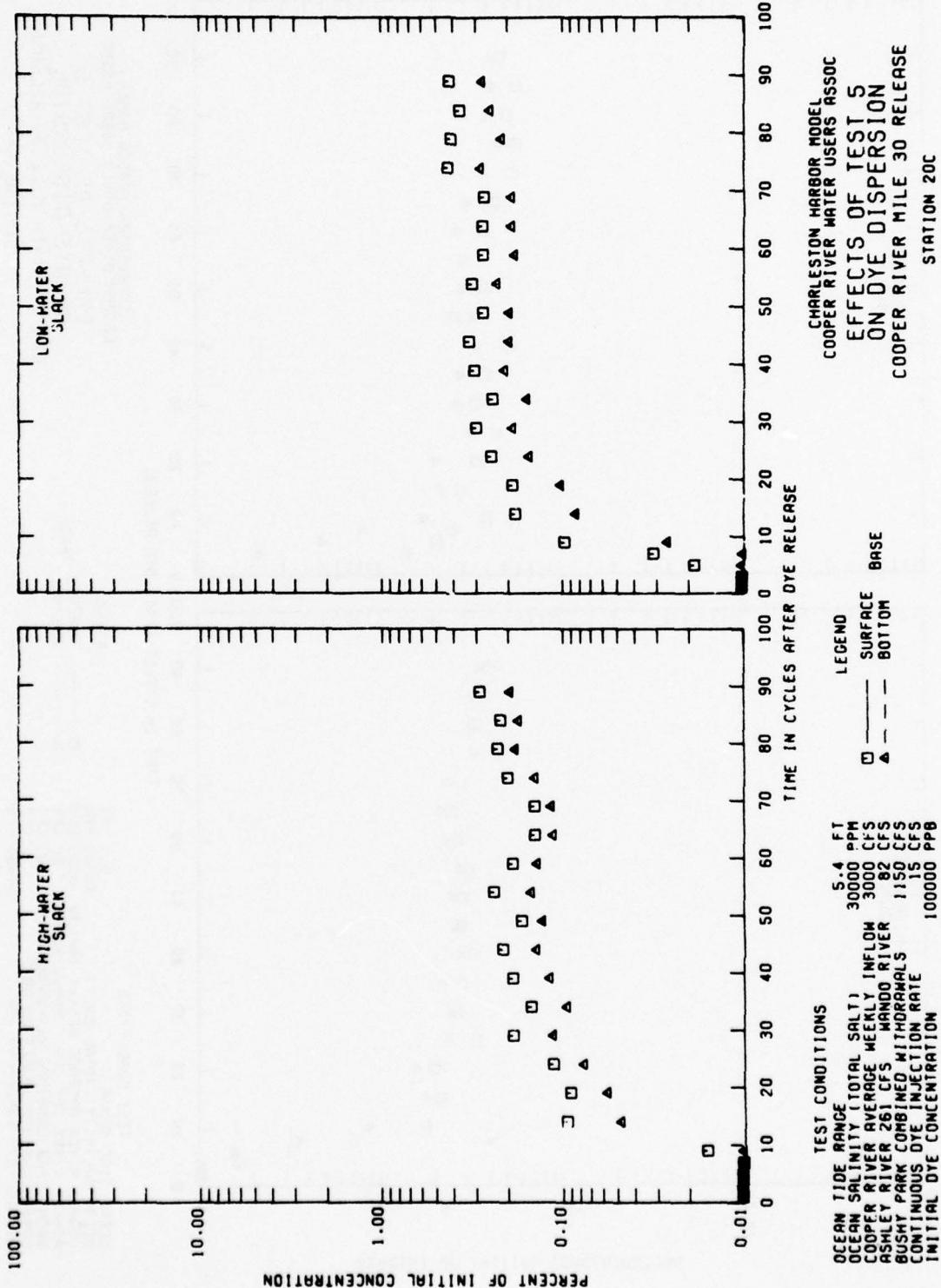


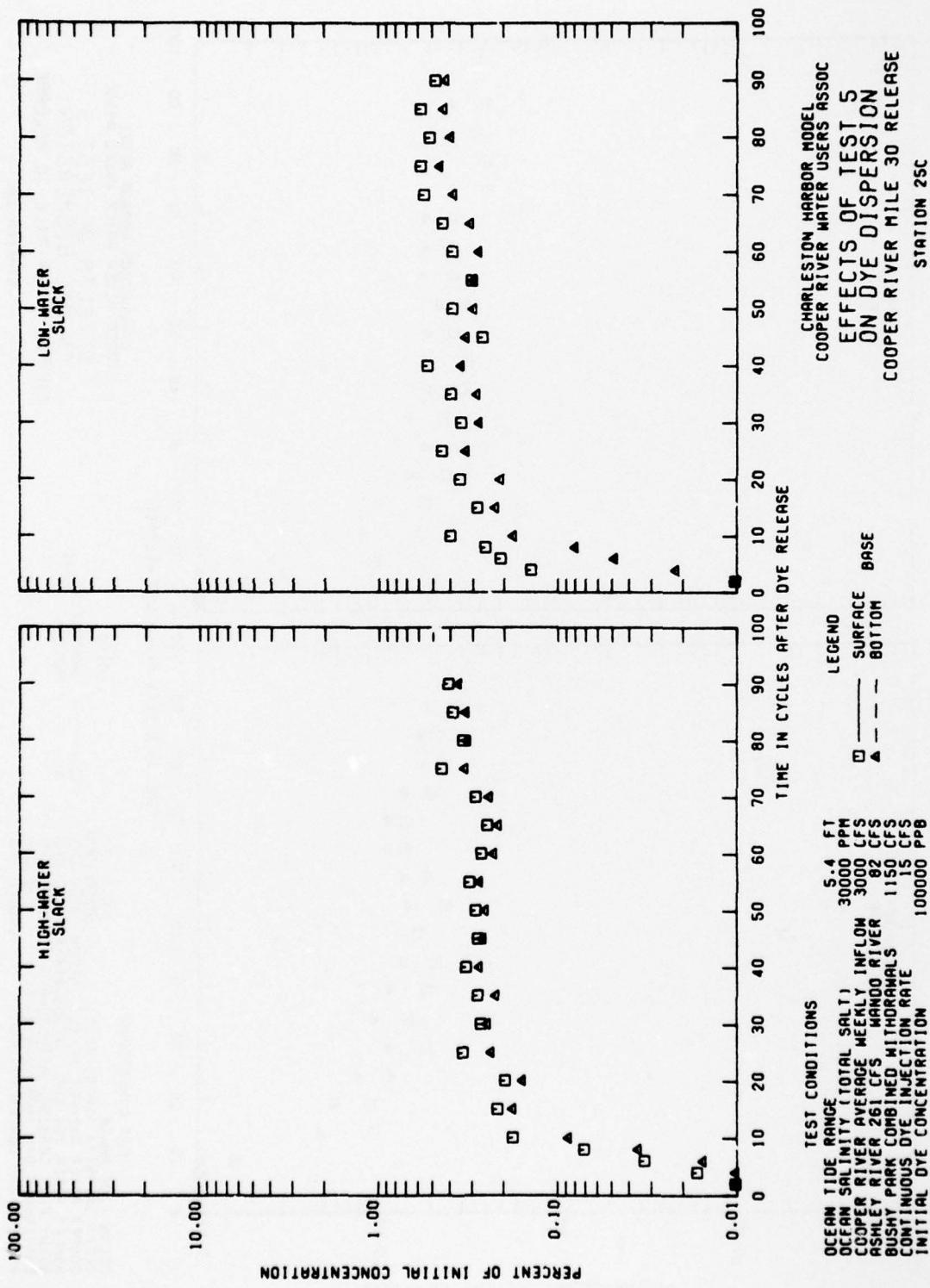


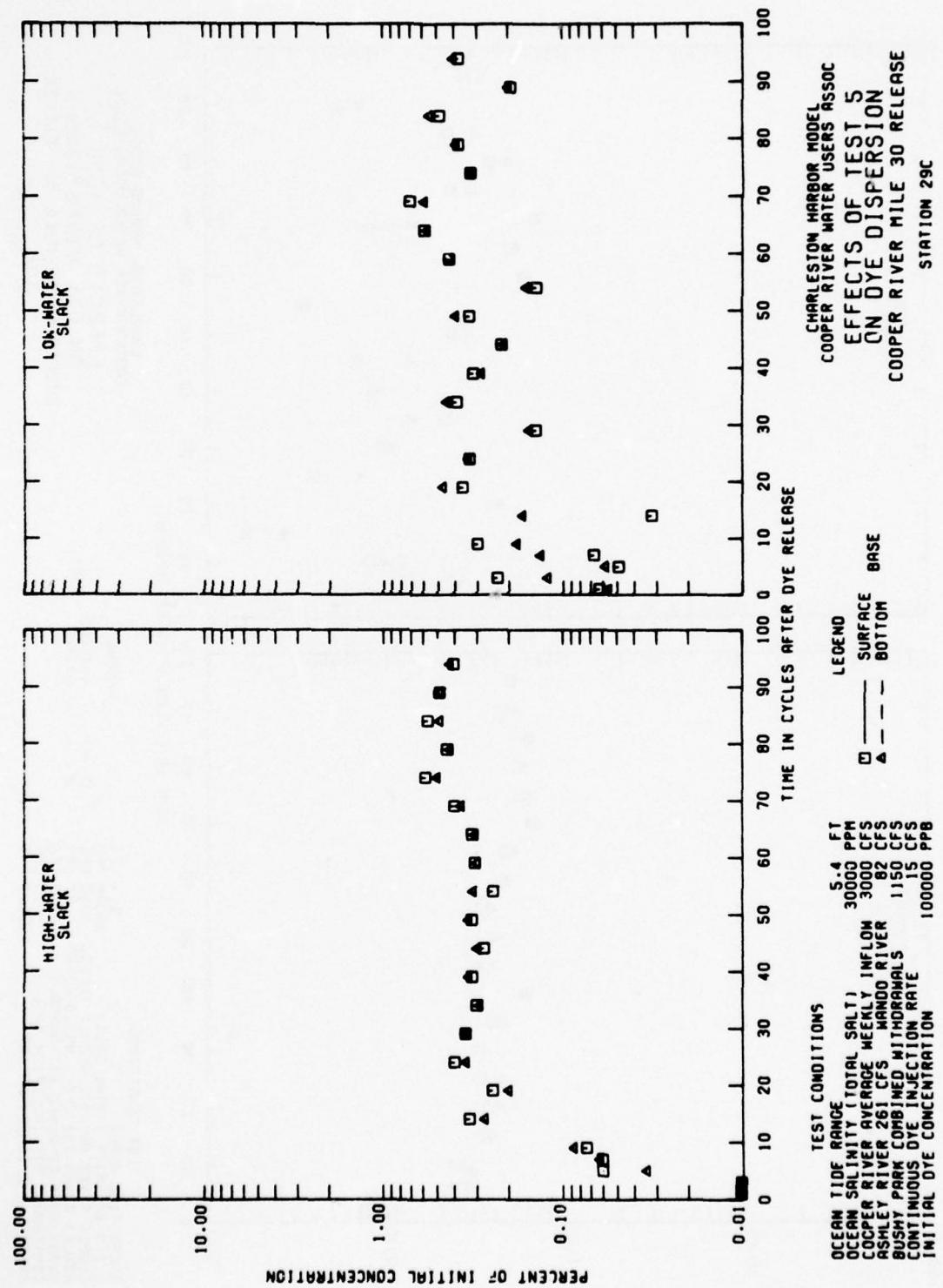












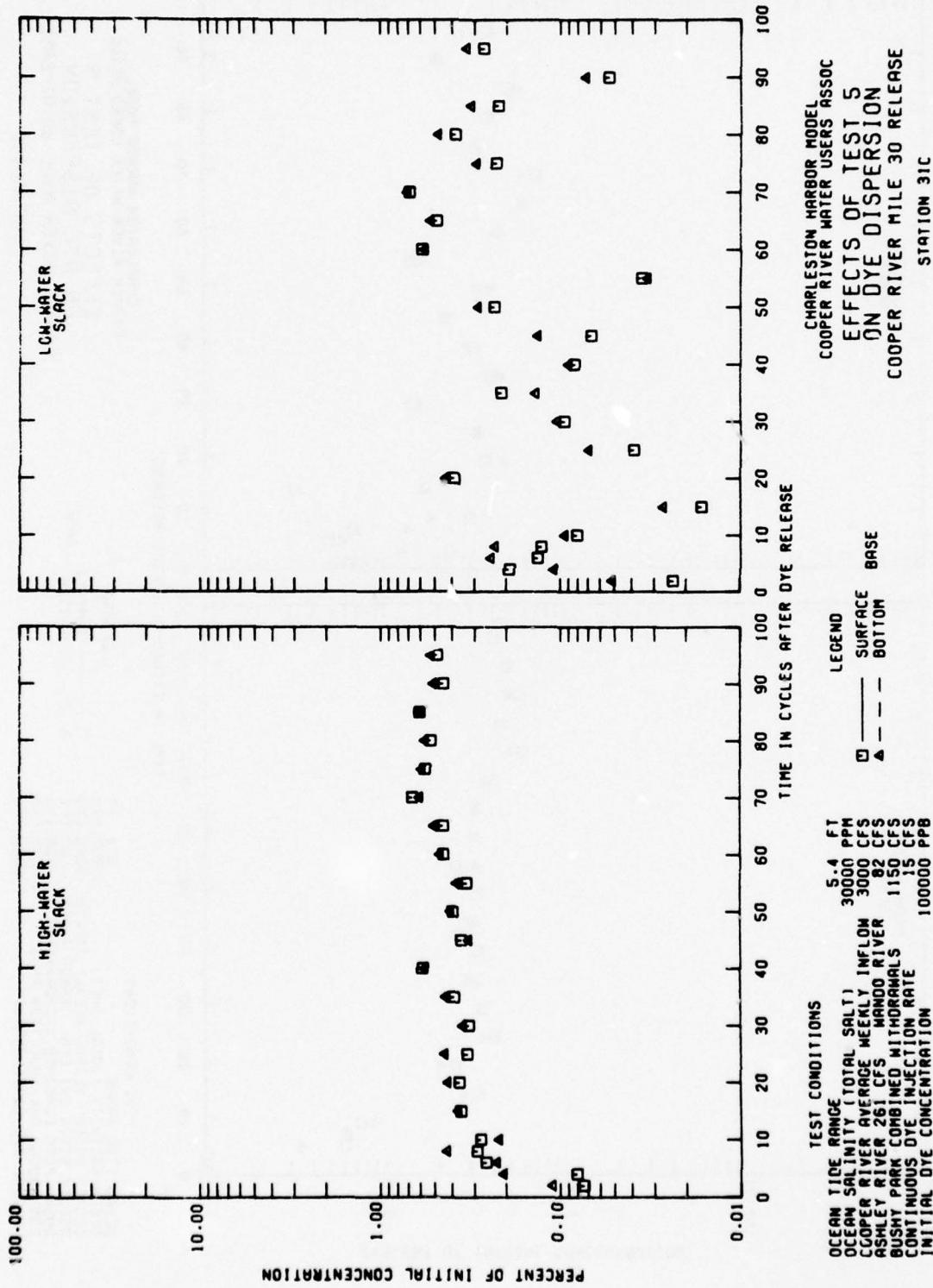
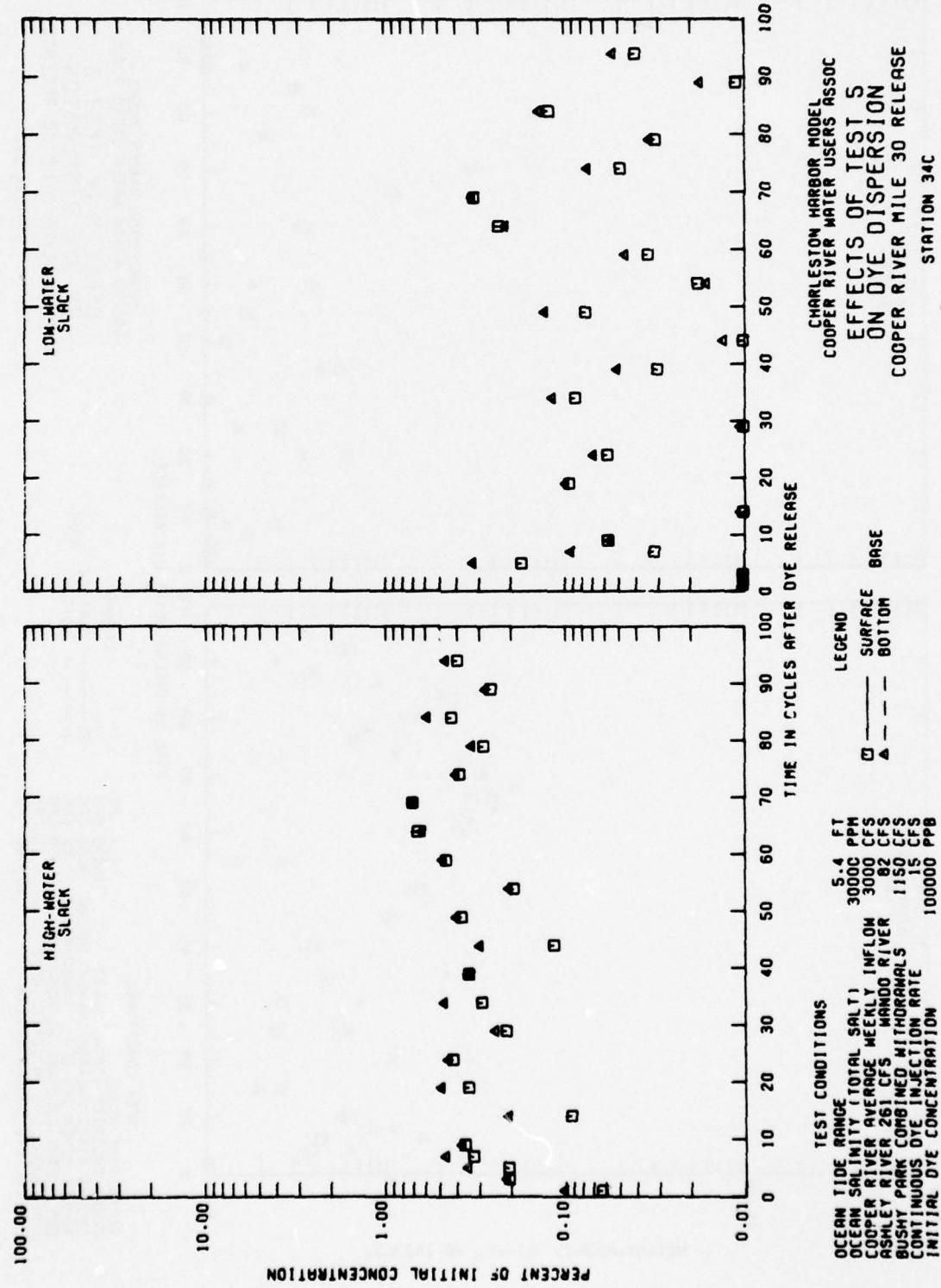
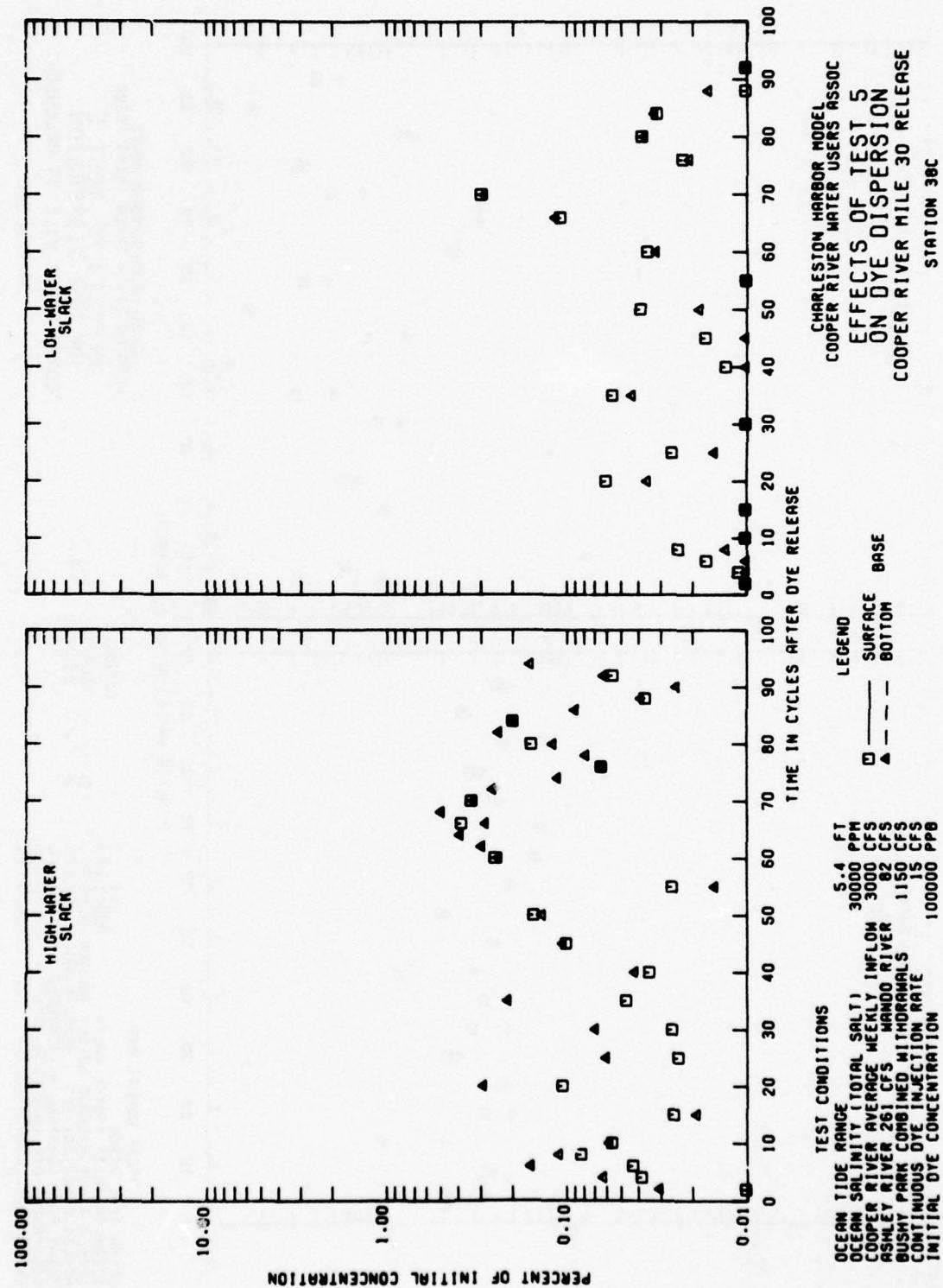
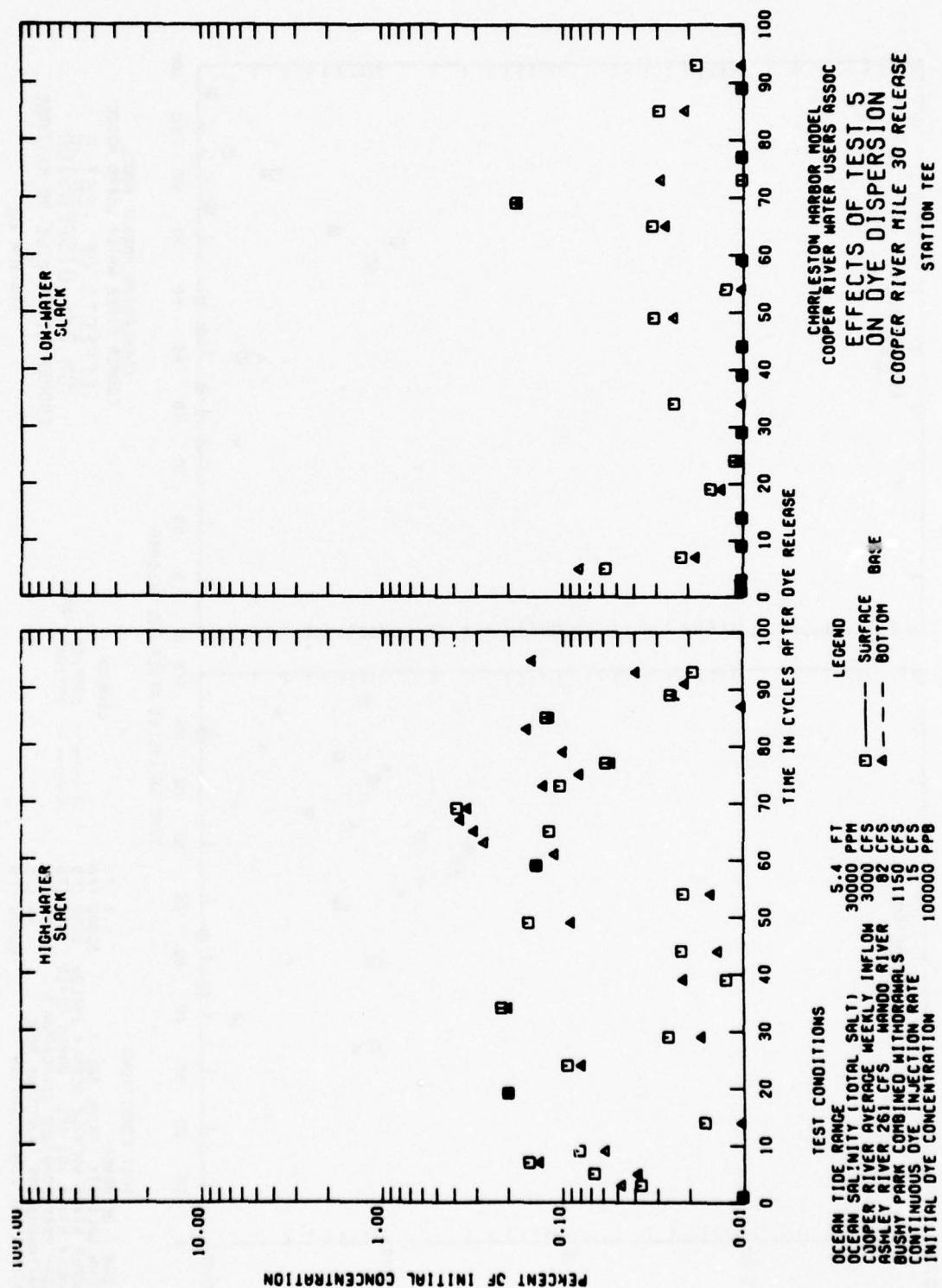


PLATE 80



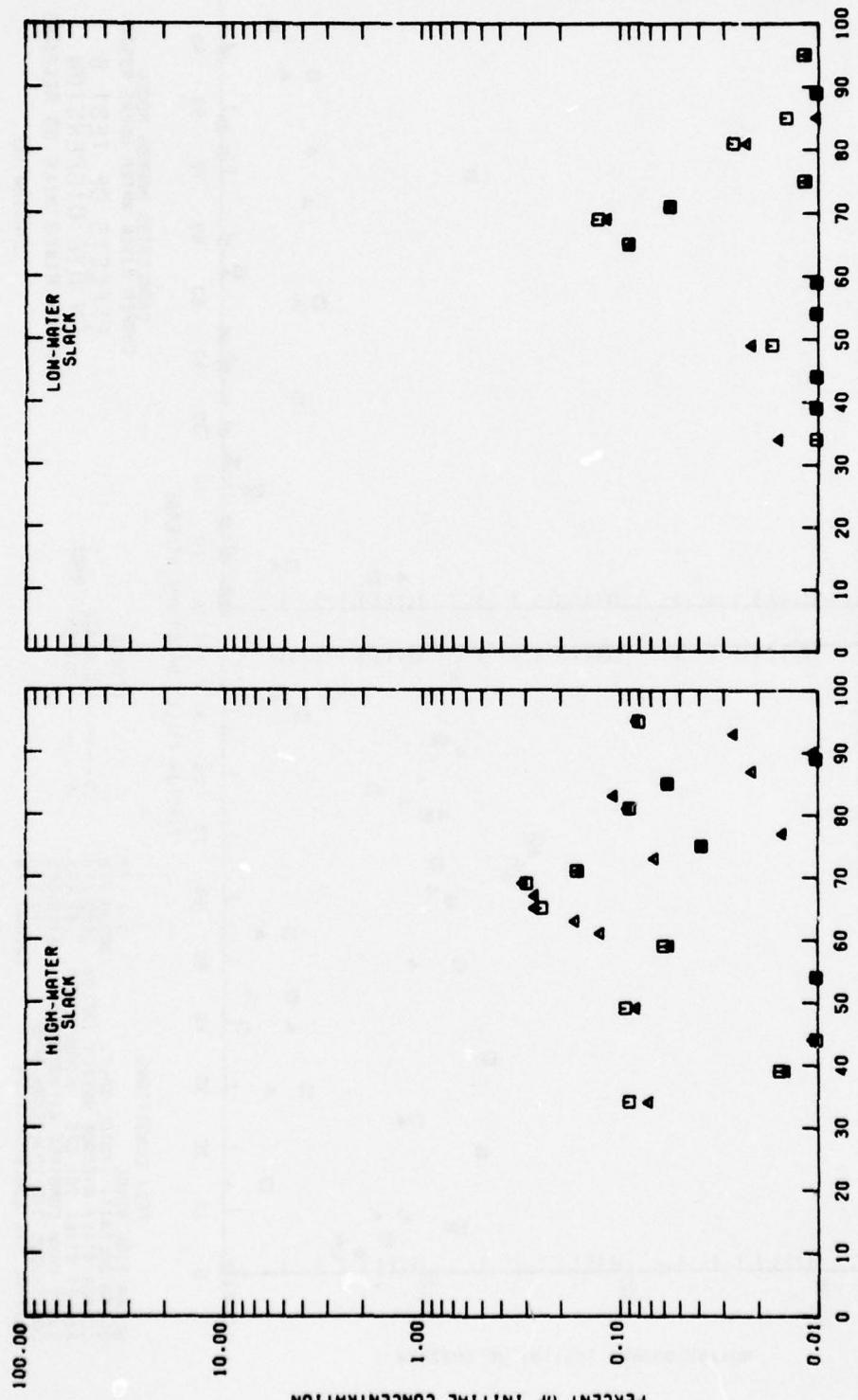




CHARLESTON HARBOR MODEL
 COOPER RIVER WATER USERS ASSOC
 EFFECTS OF TEST 5
 ON DYE DISPERSION
 COOPER RIVER MILE 30 RELEASE
 STATION 41C

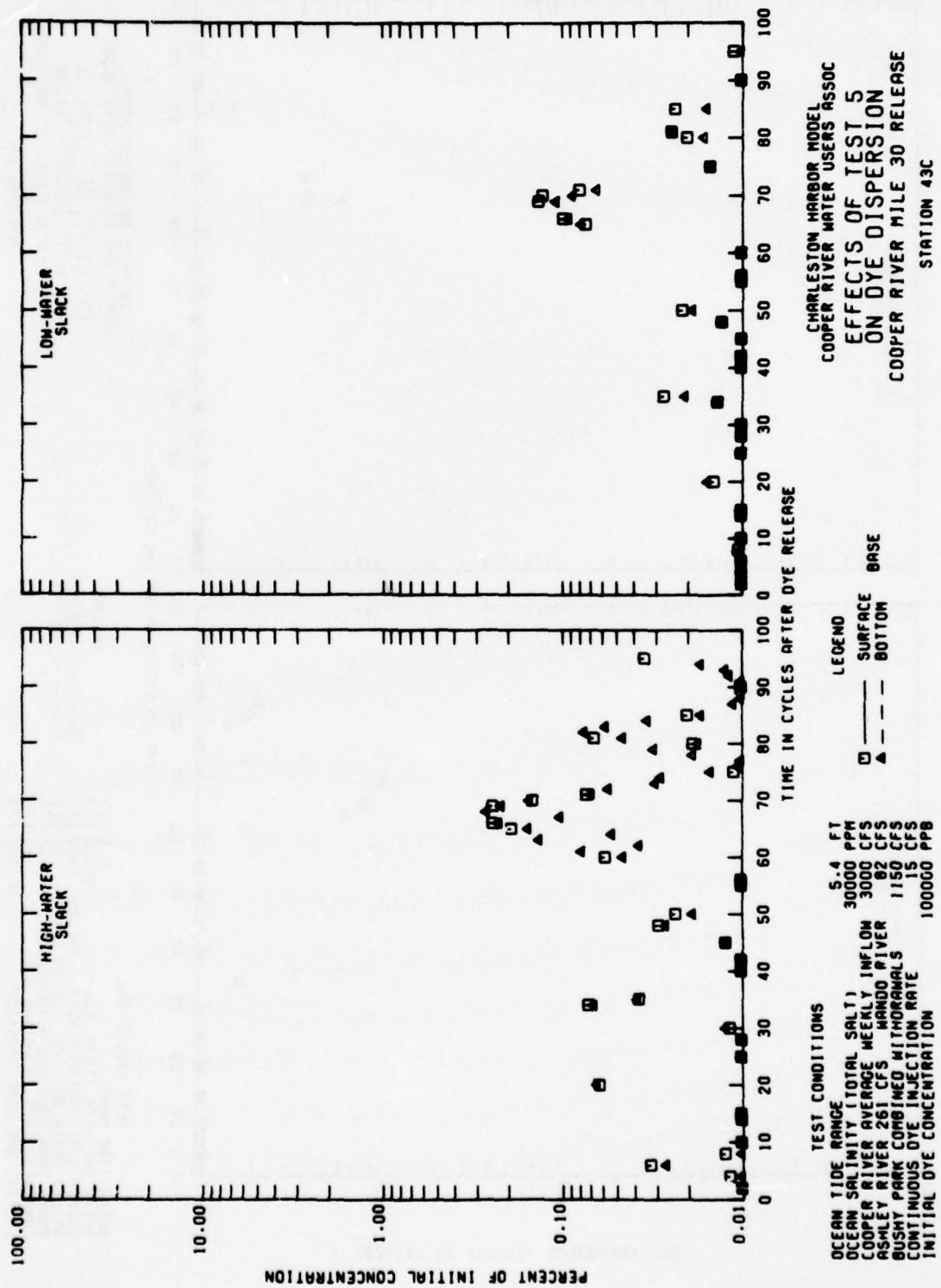
TEST CONDITIONS
 OCEAN TIDE RANGE 5.4 FT
 OCEAN SALINITY (TOTAL SALT) 30000 PPM
 COOPER RIVER AVERAGE WEEKLY INFLOW 3000 CFS
 ASHLEY RIVER 26 CFS
 Wando River 82 CFS
 BUSHEY PARK COMBINED WITHDRAWALS 1150 CFS
 CONTINUOUS DYE INJECTION RATE 15 CFS
 INITIAL DYE CONCENTRATION 100000 PPM

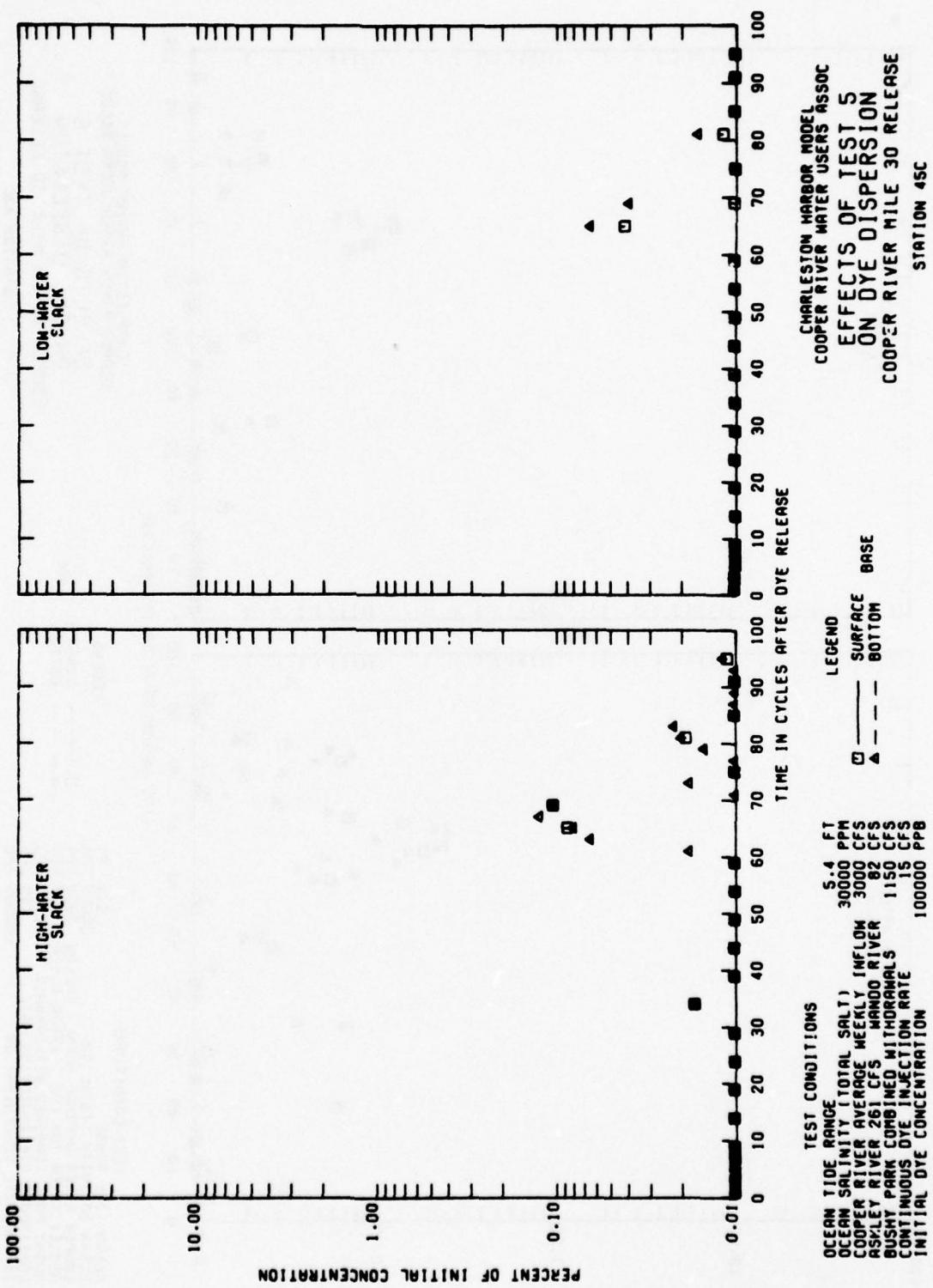
TIME IN CYCLES AFTER DYE RELEASE

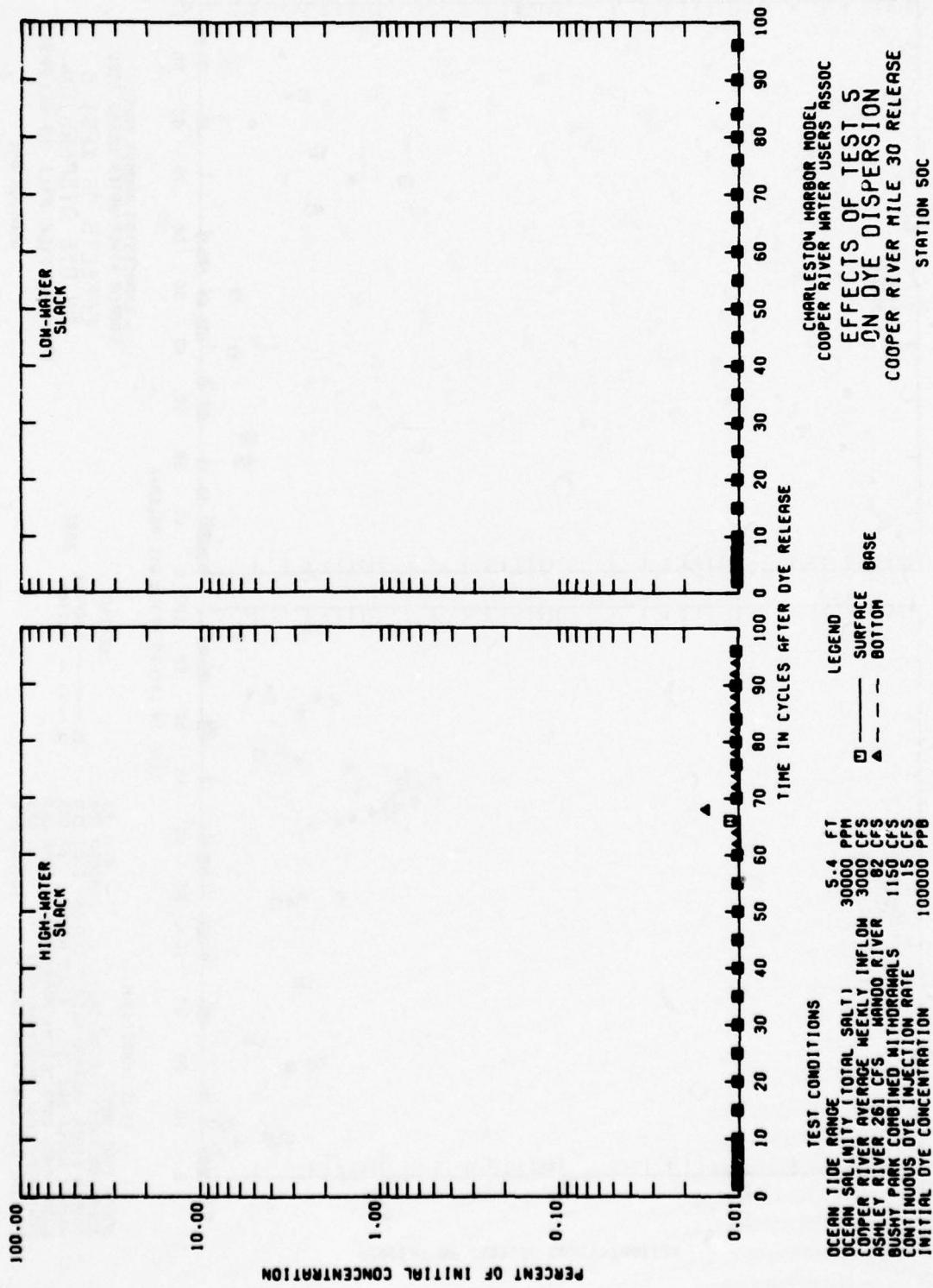


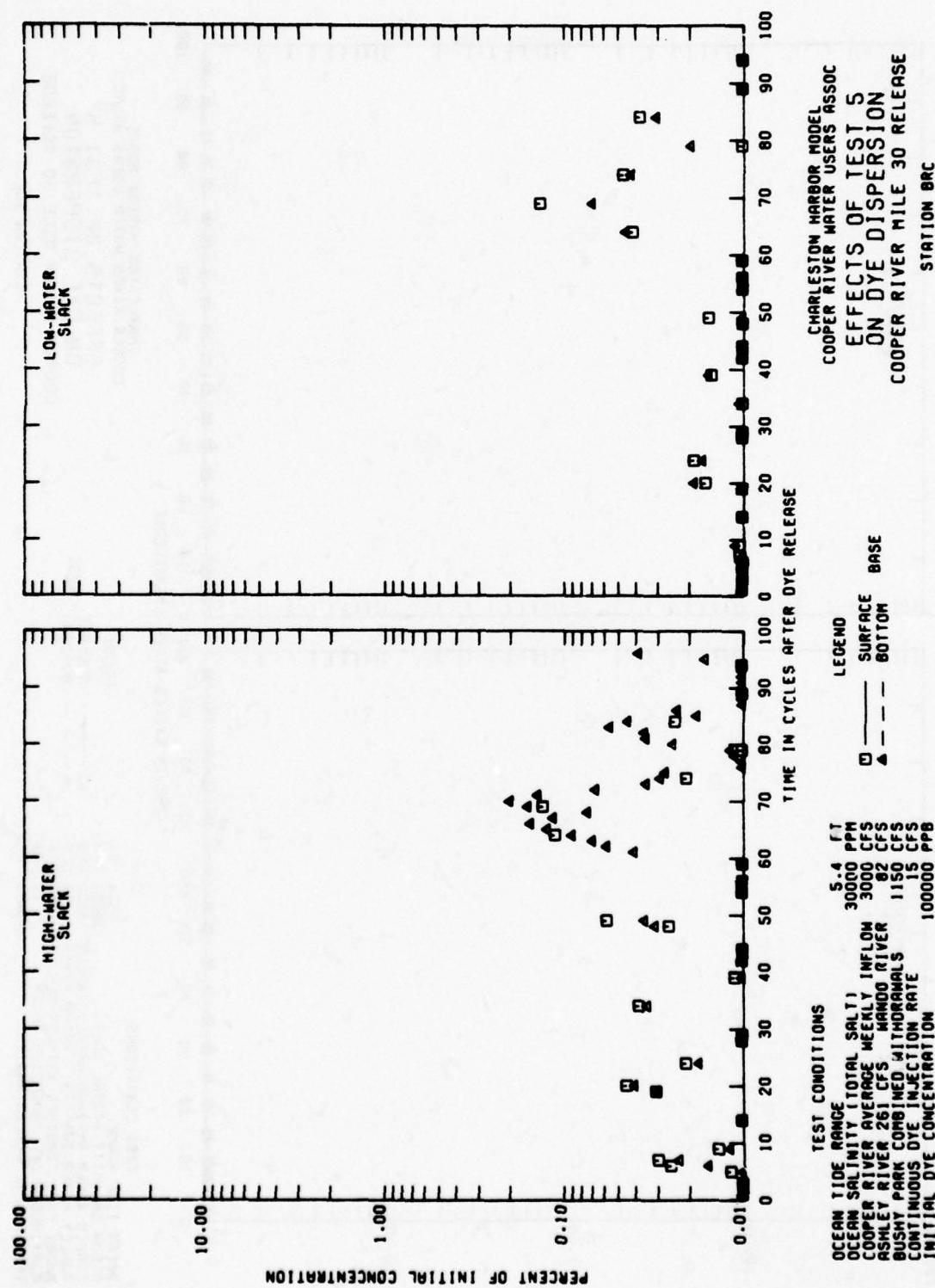
PERCENT OF INITIAL CONCENTRATION

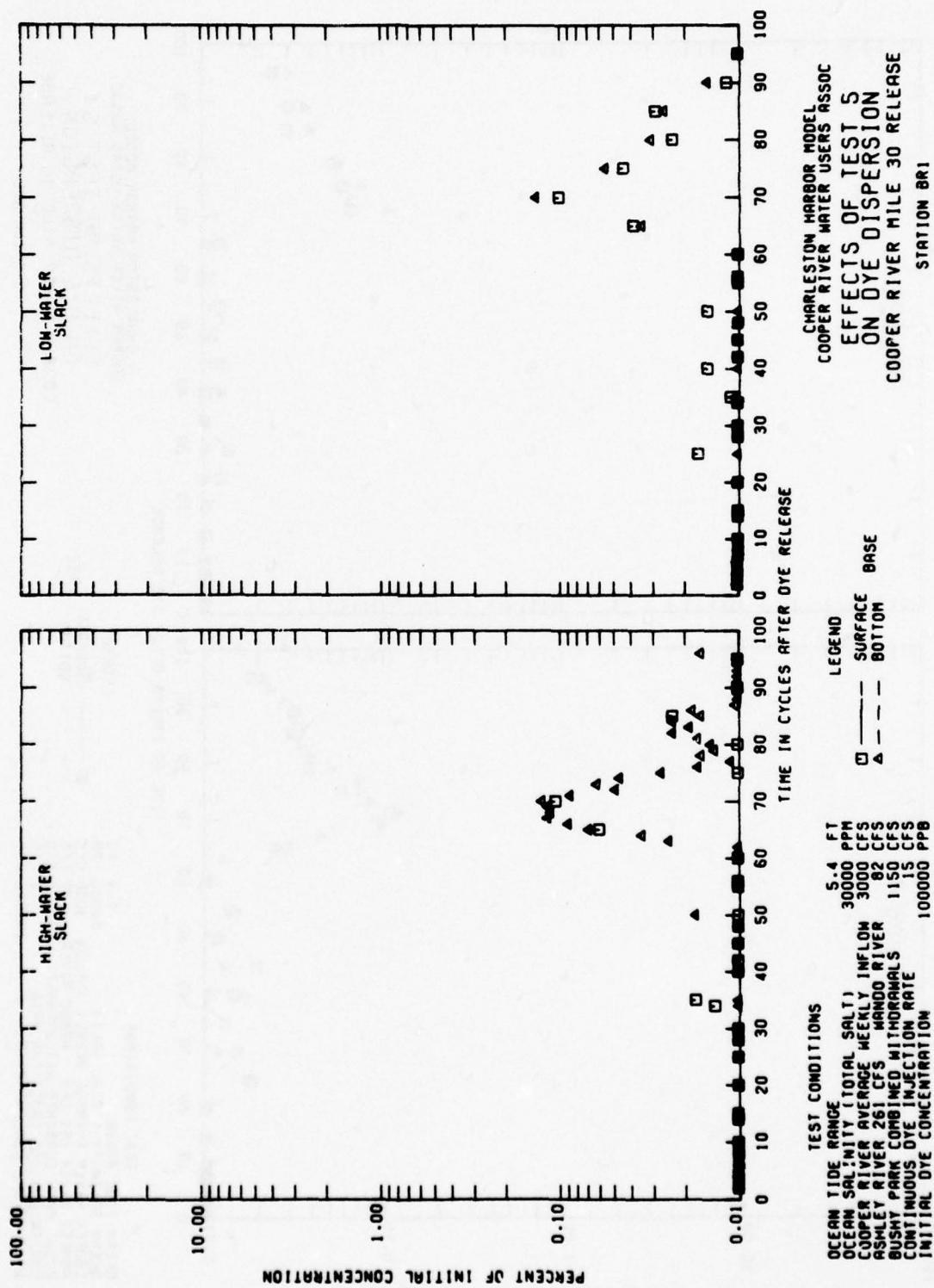
PLATE 84











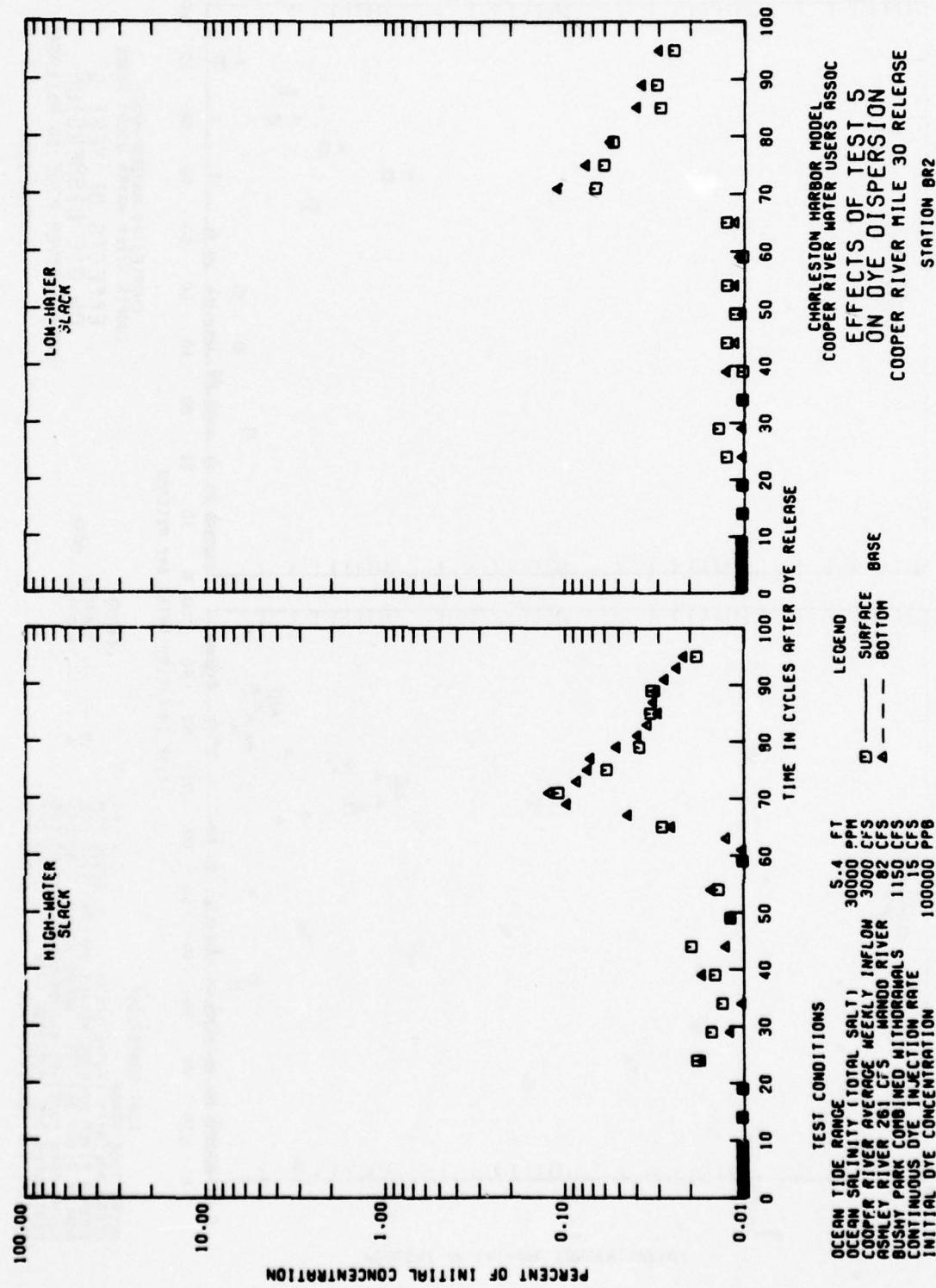
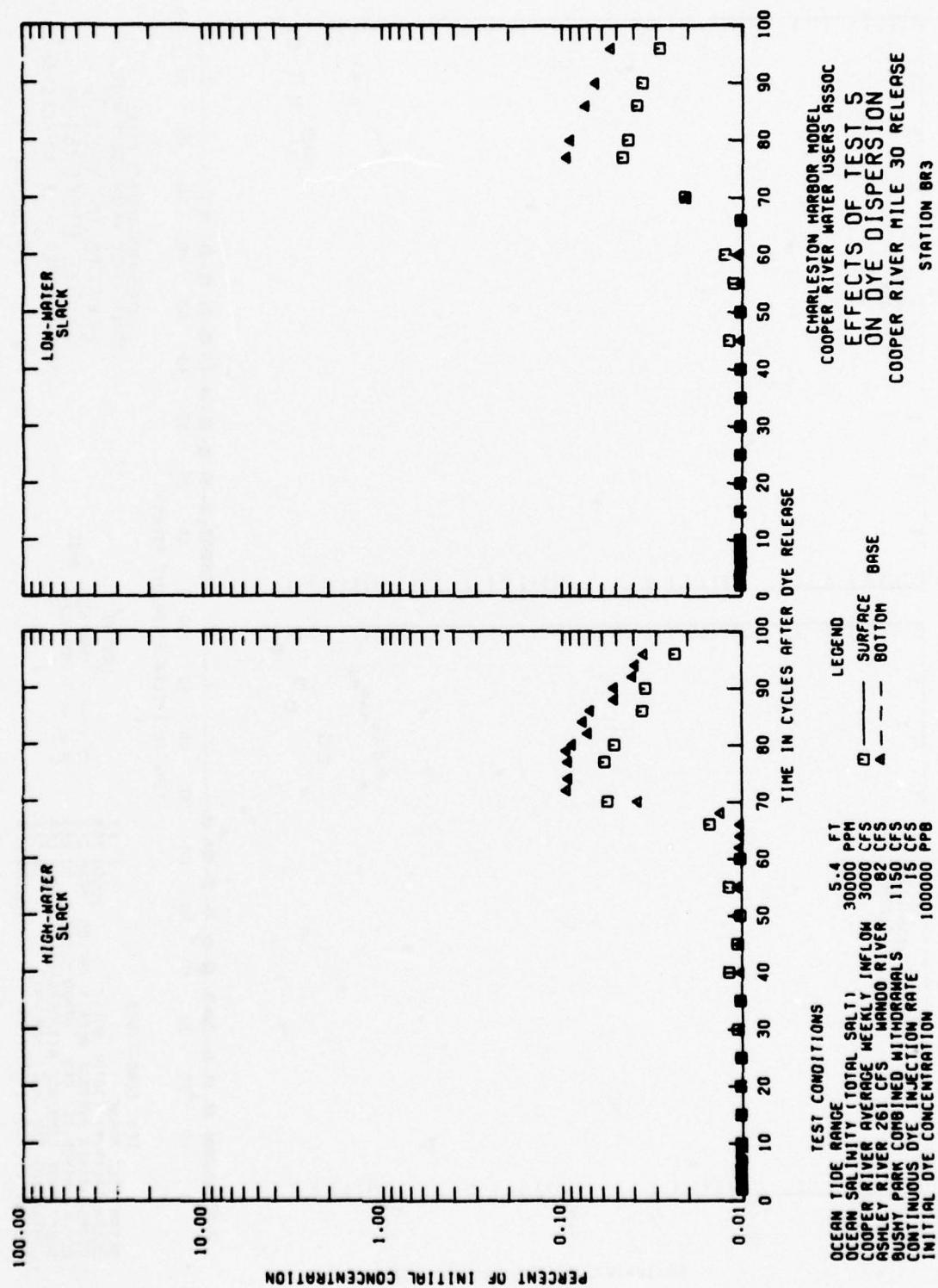
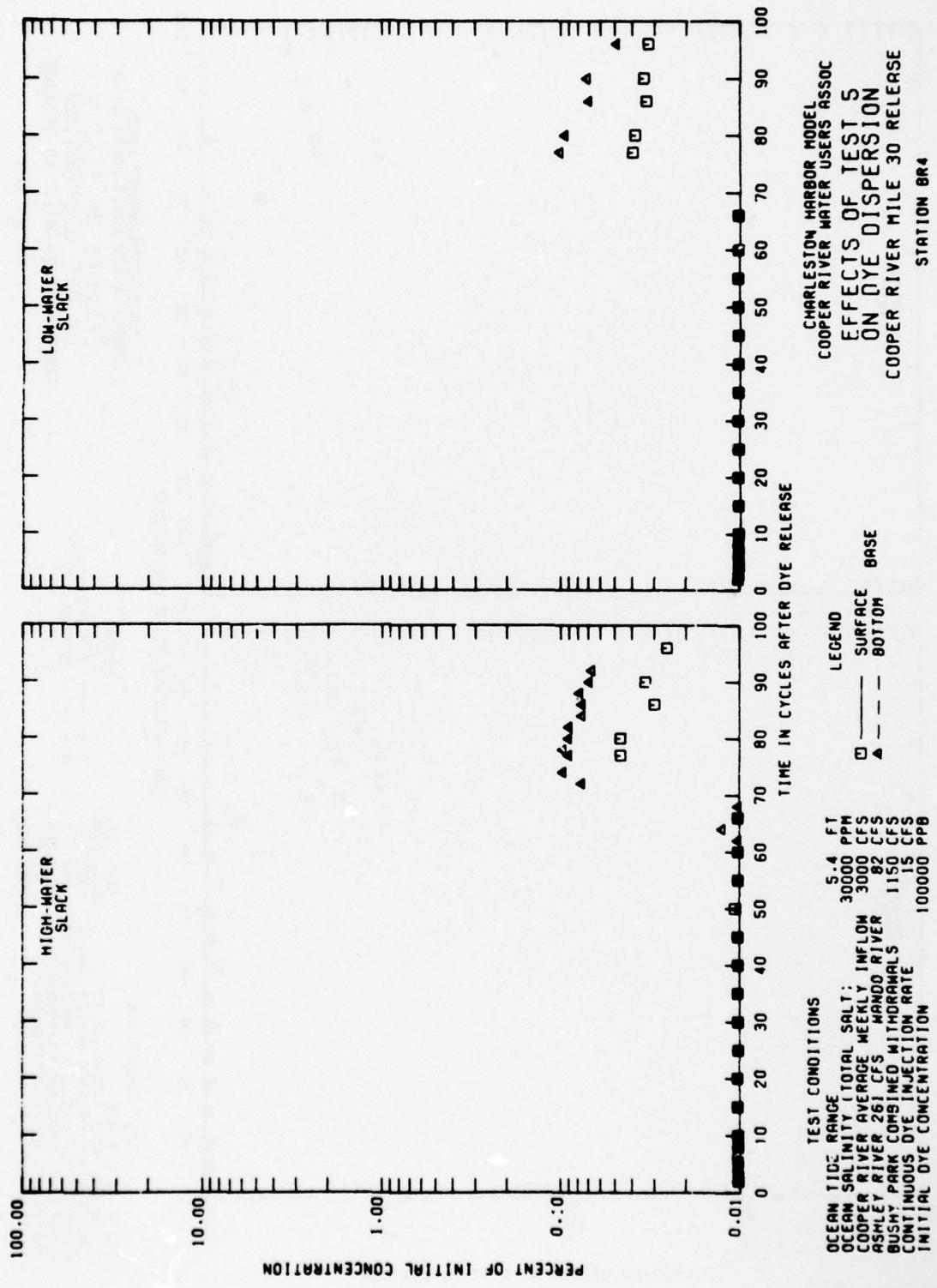
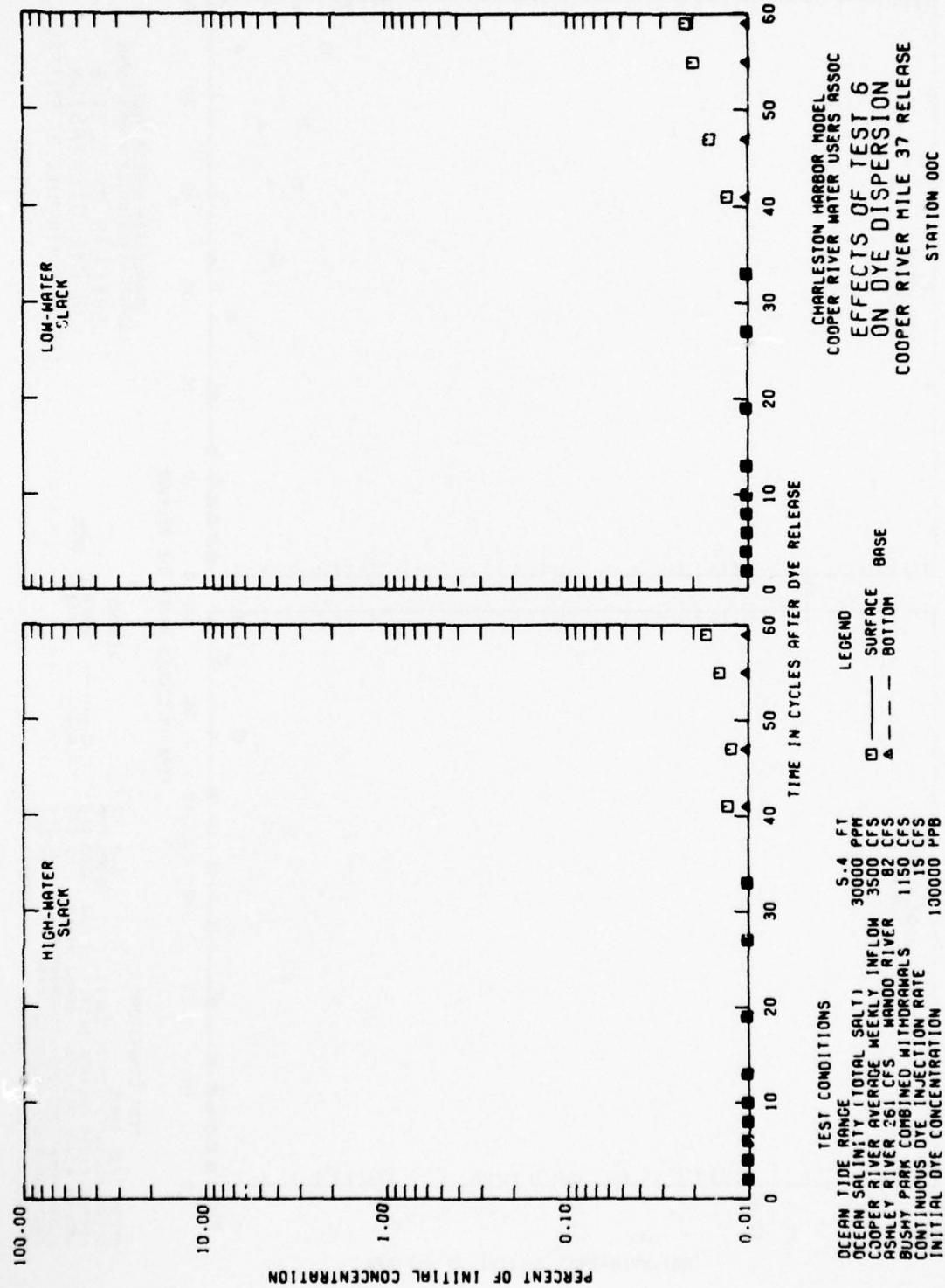
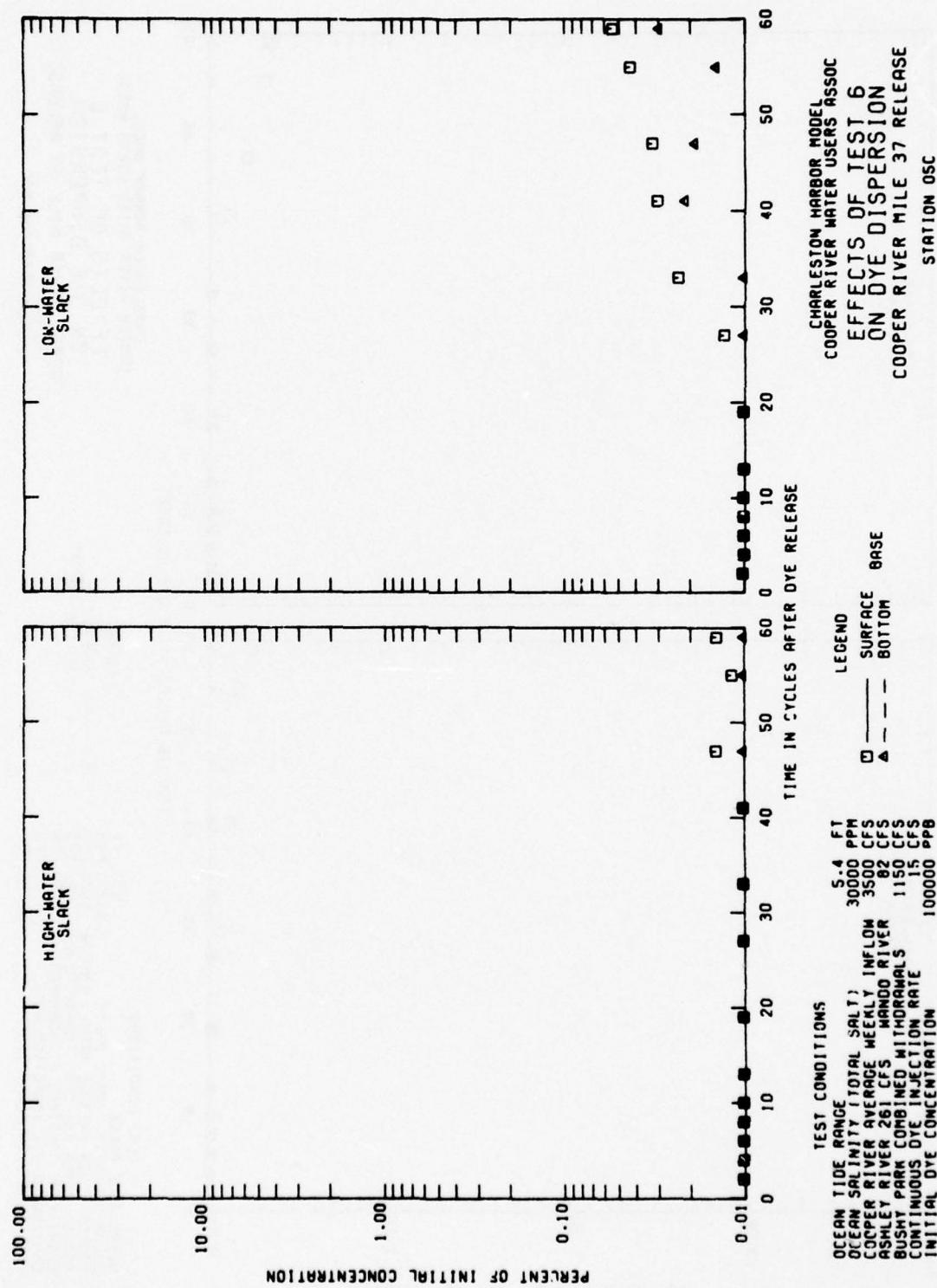


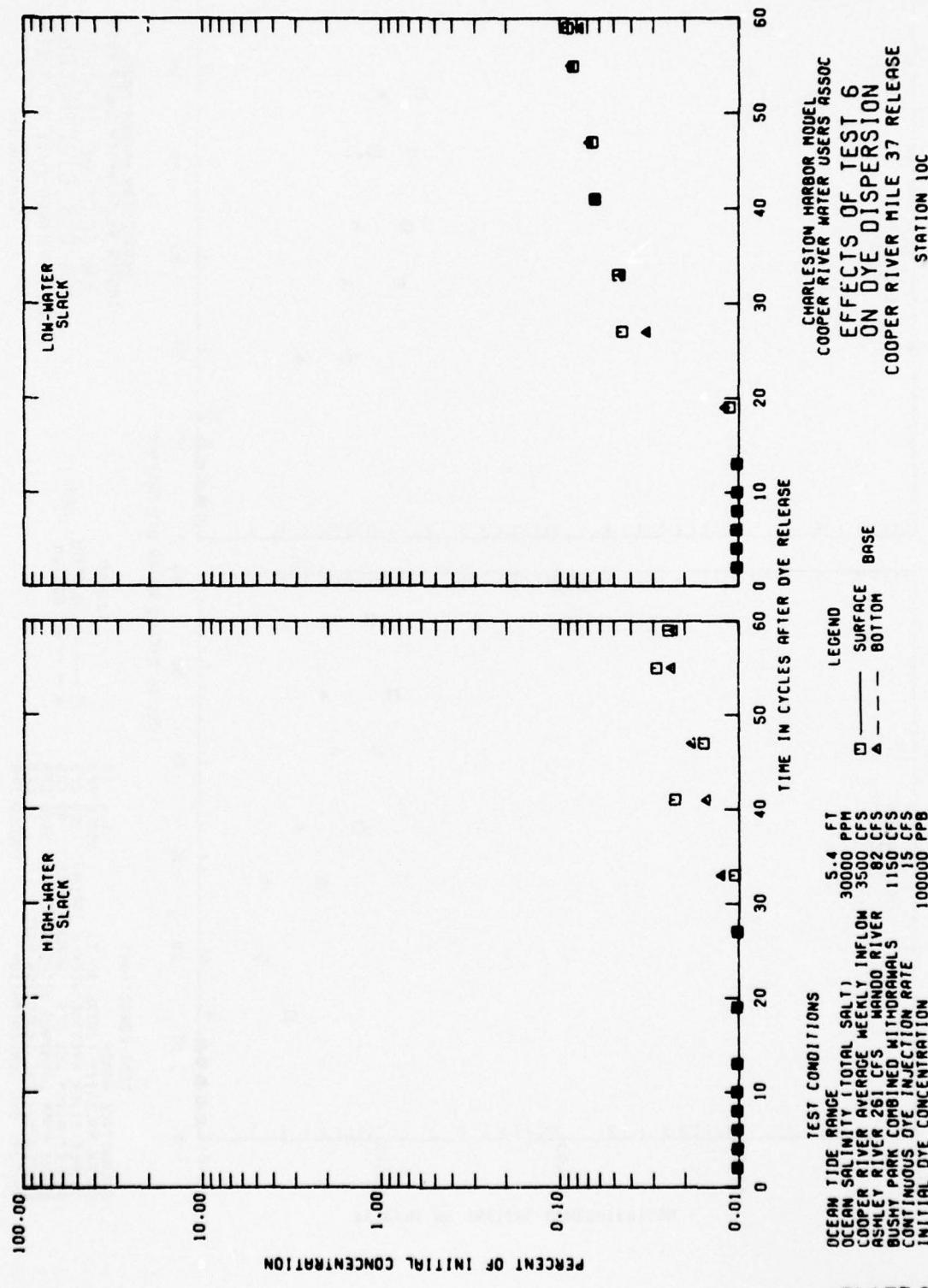
PLATE 90

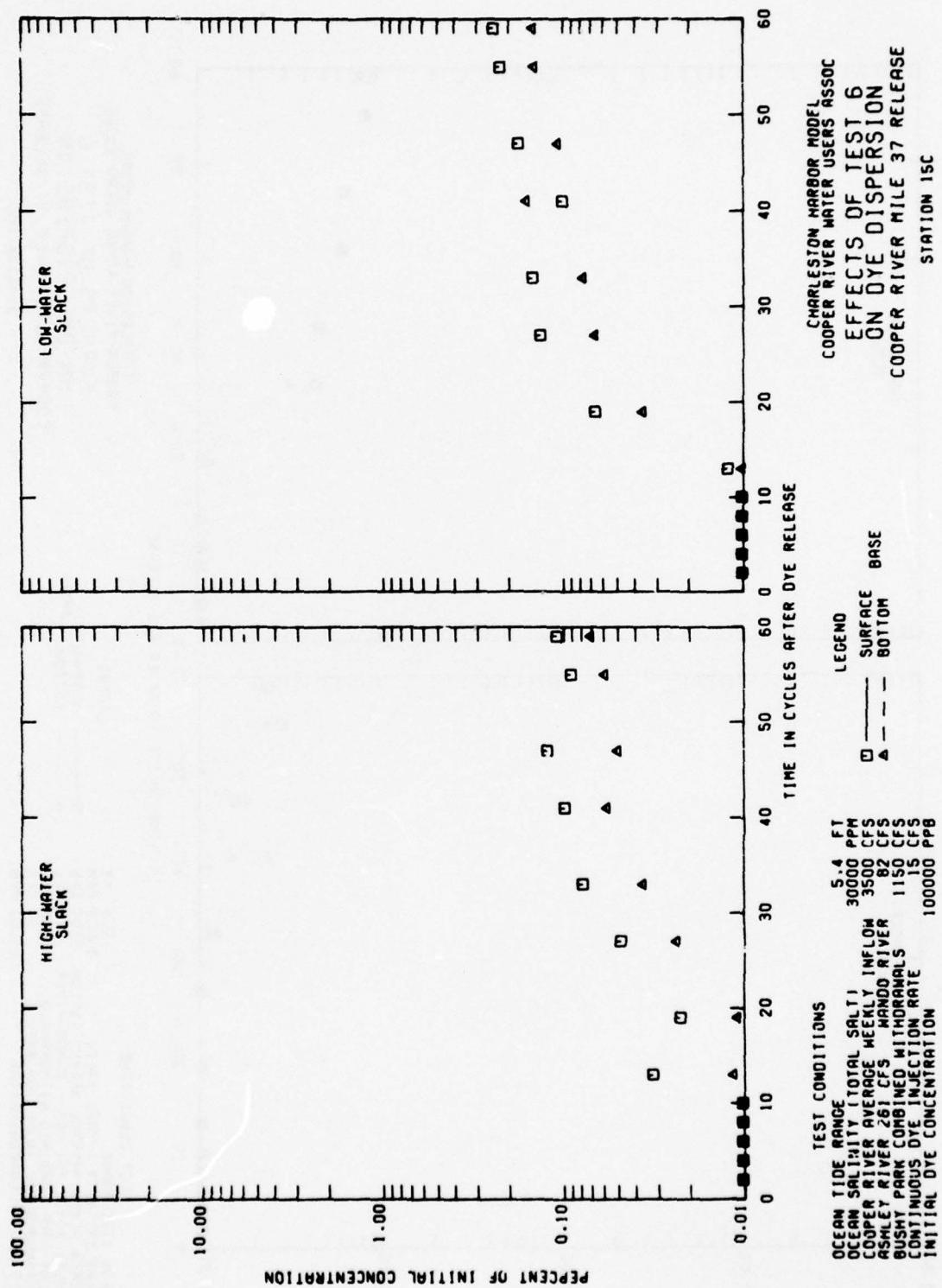


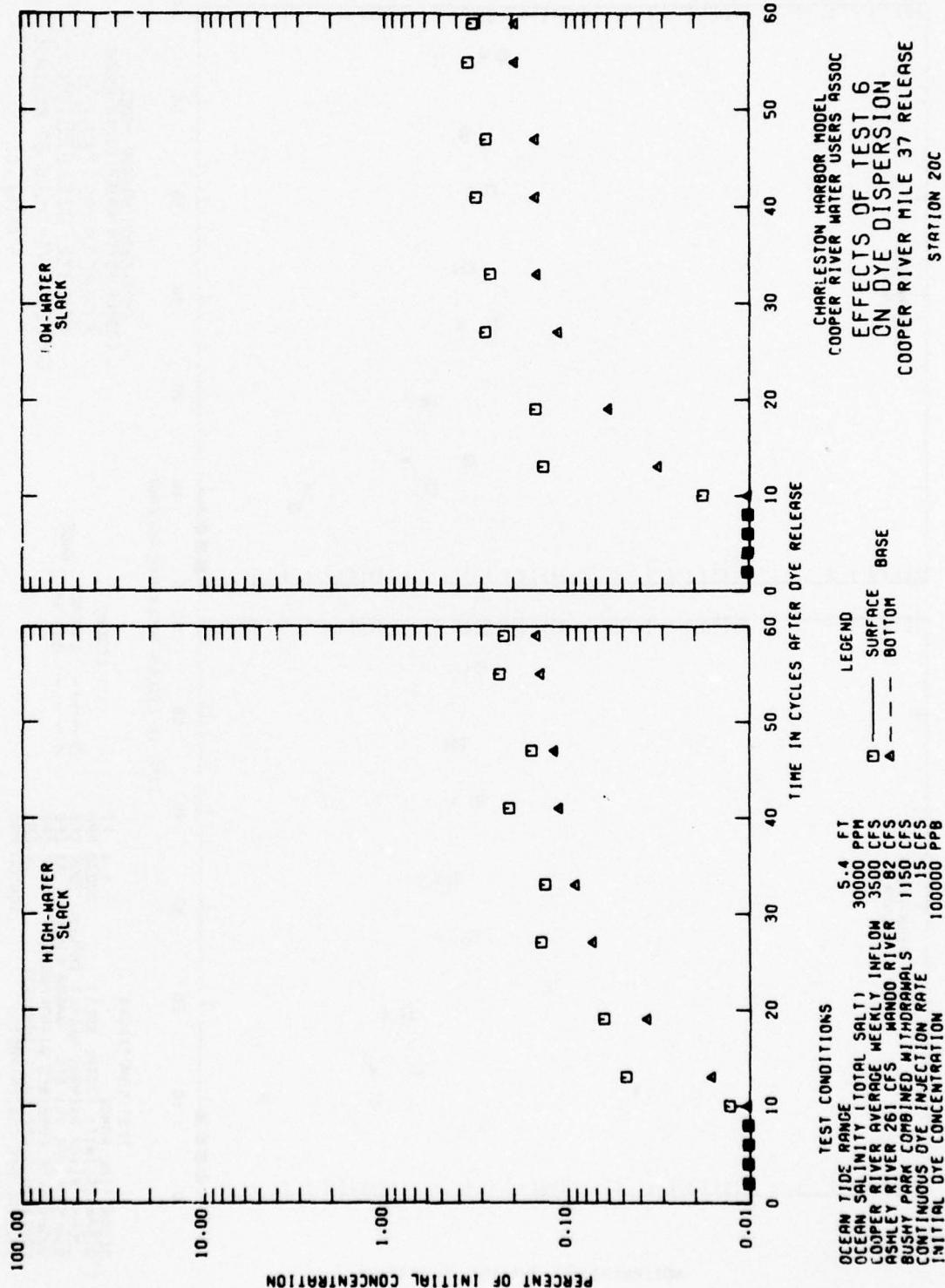


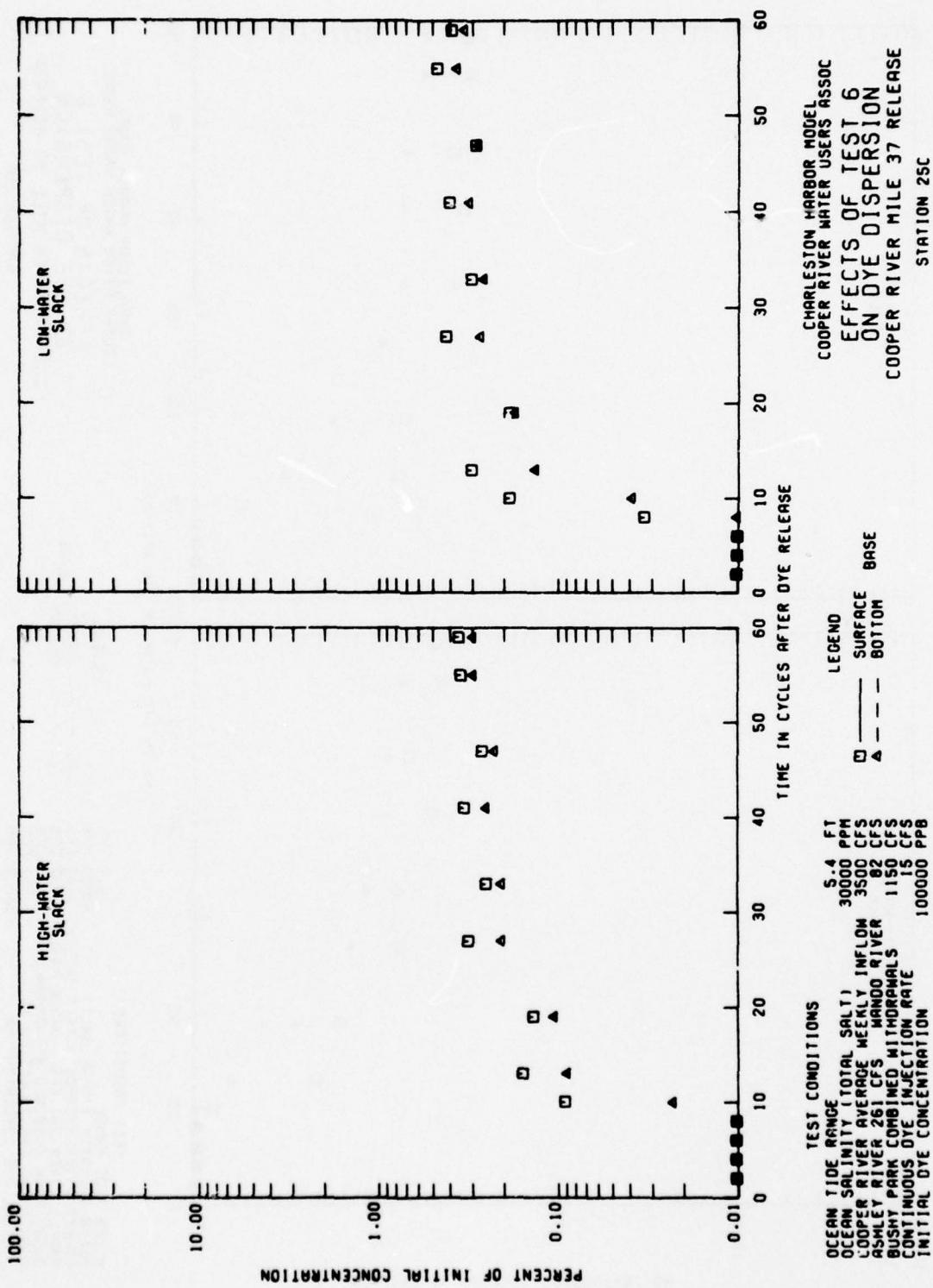


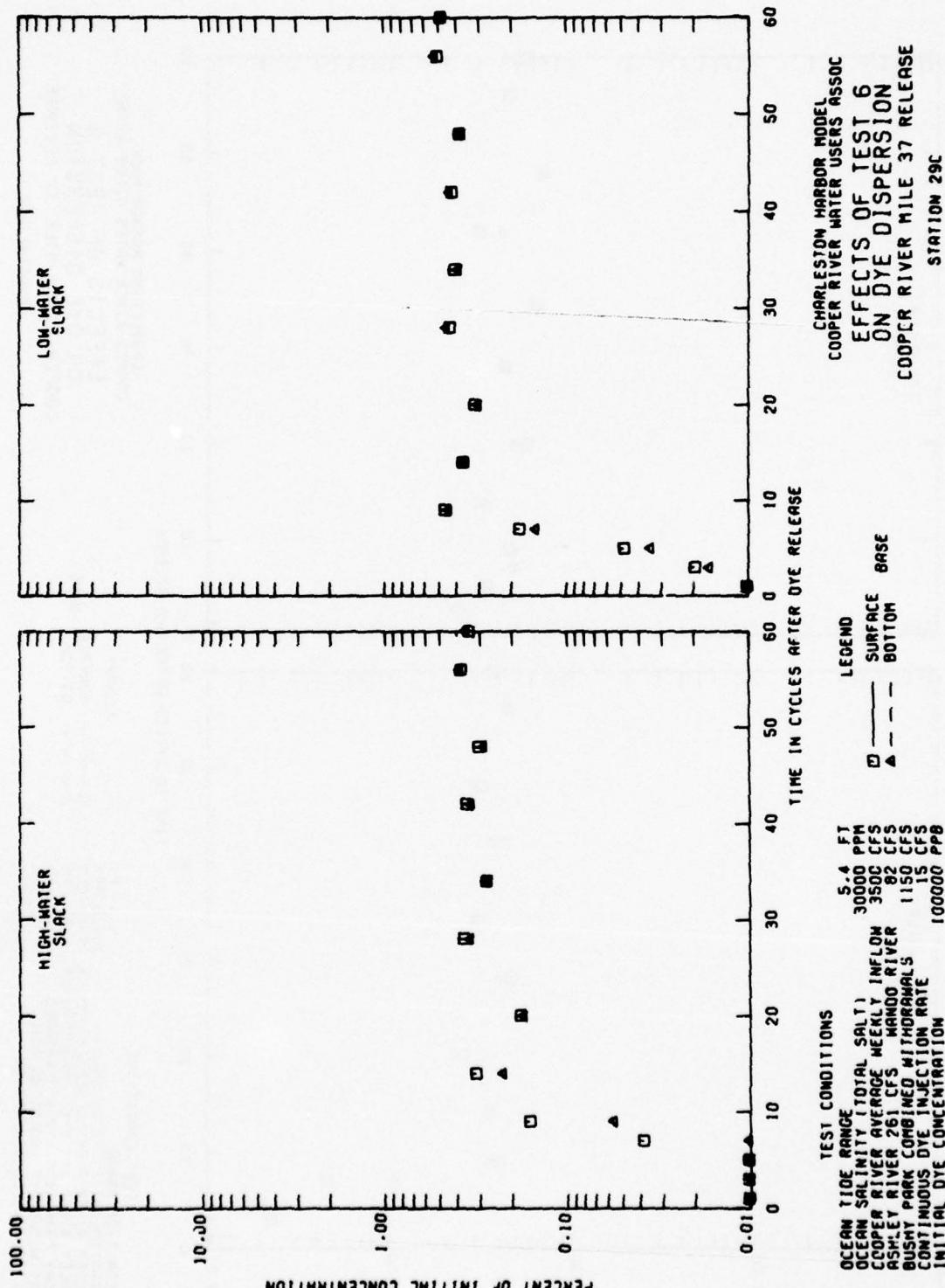


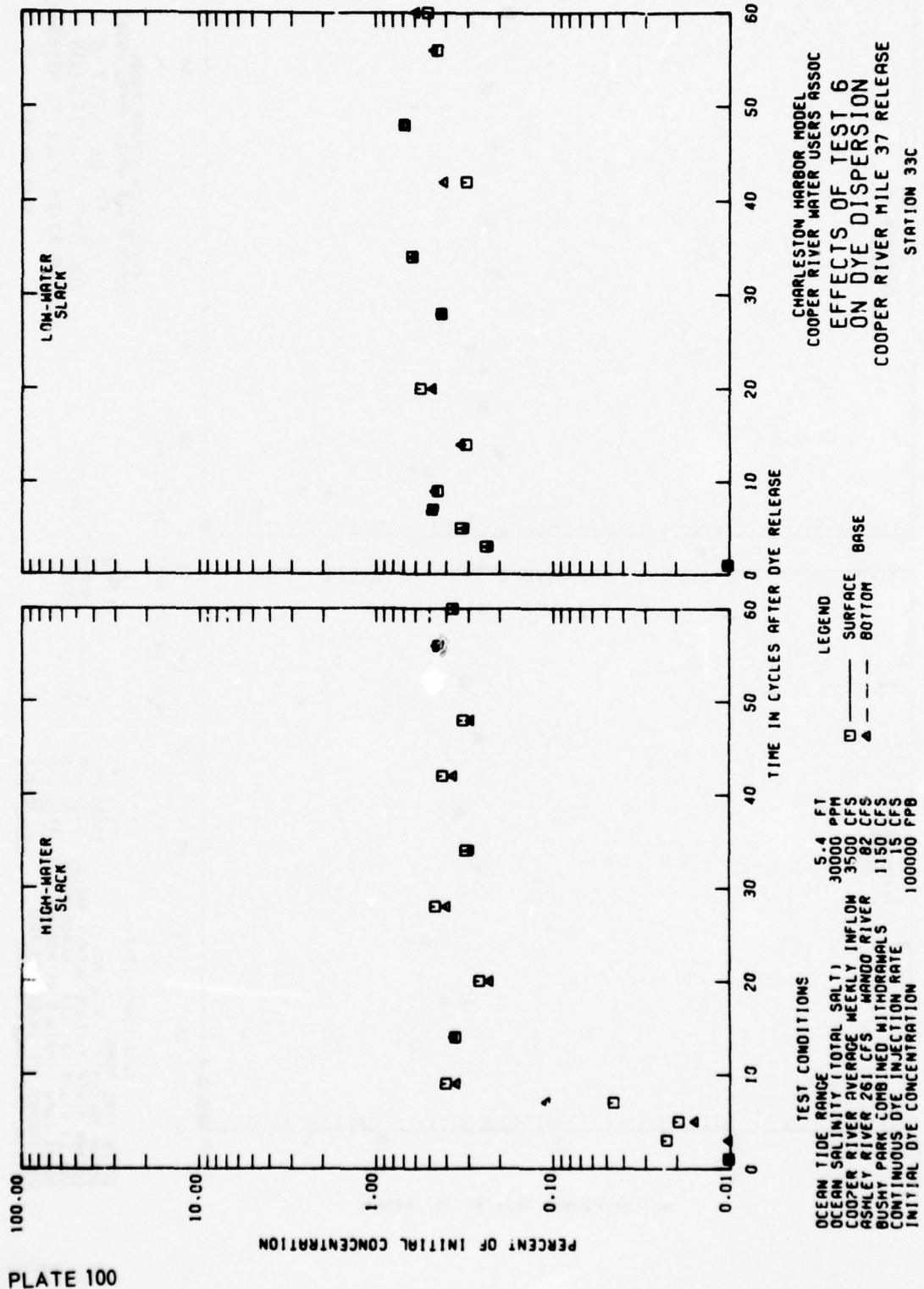


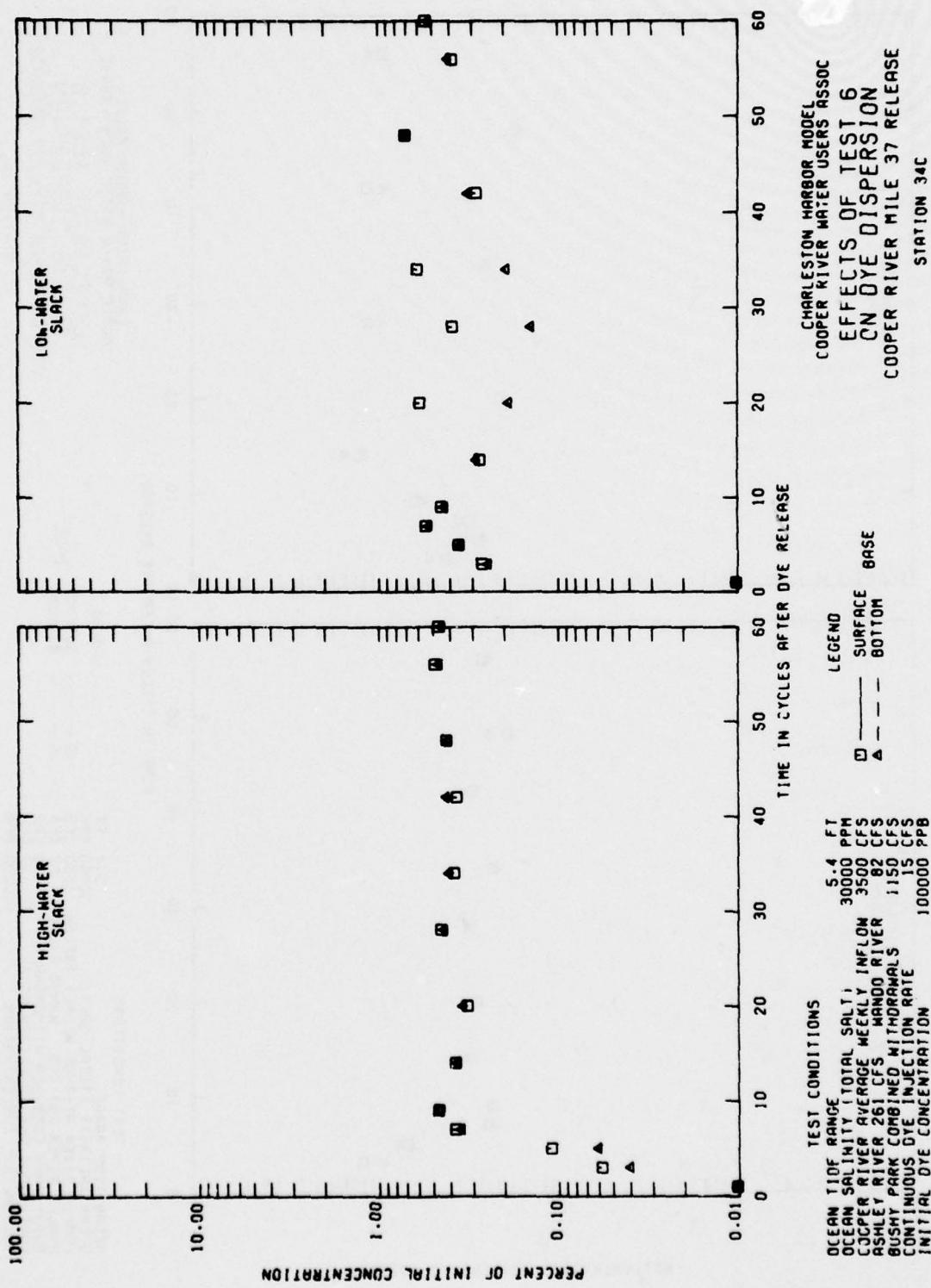


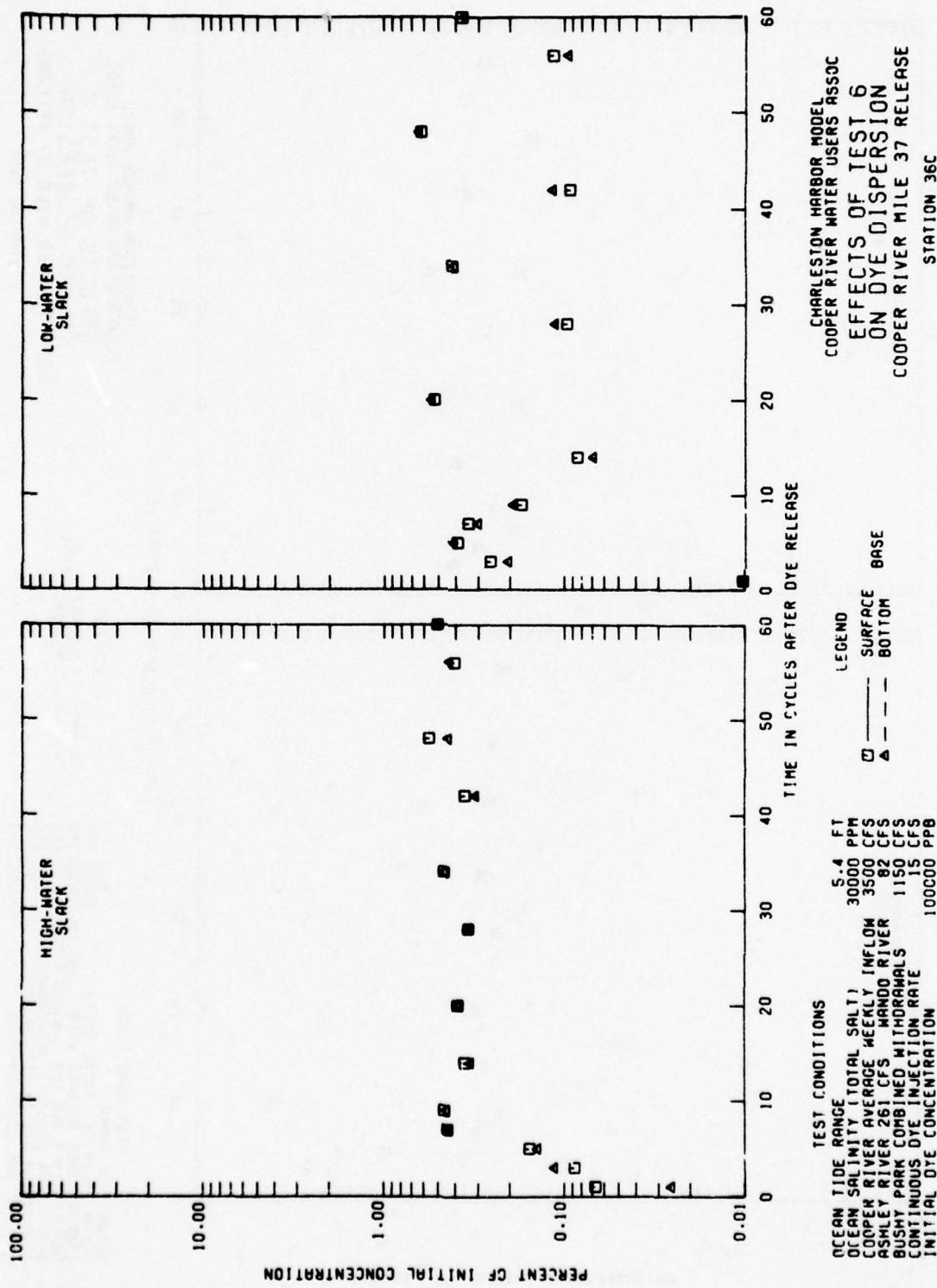


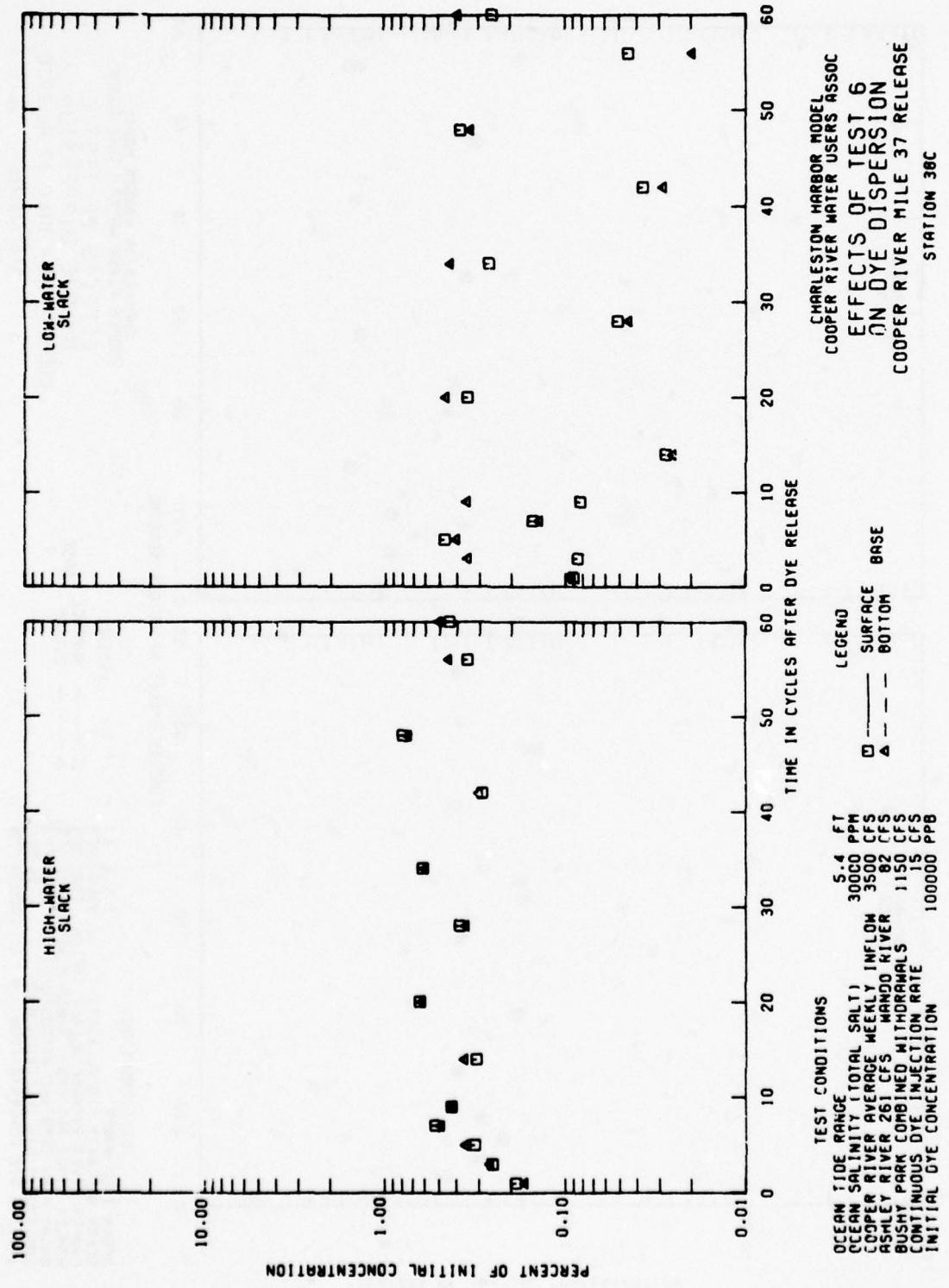












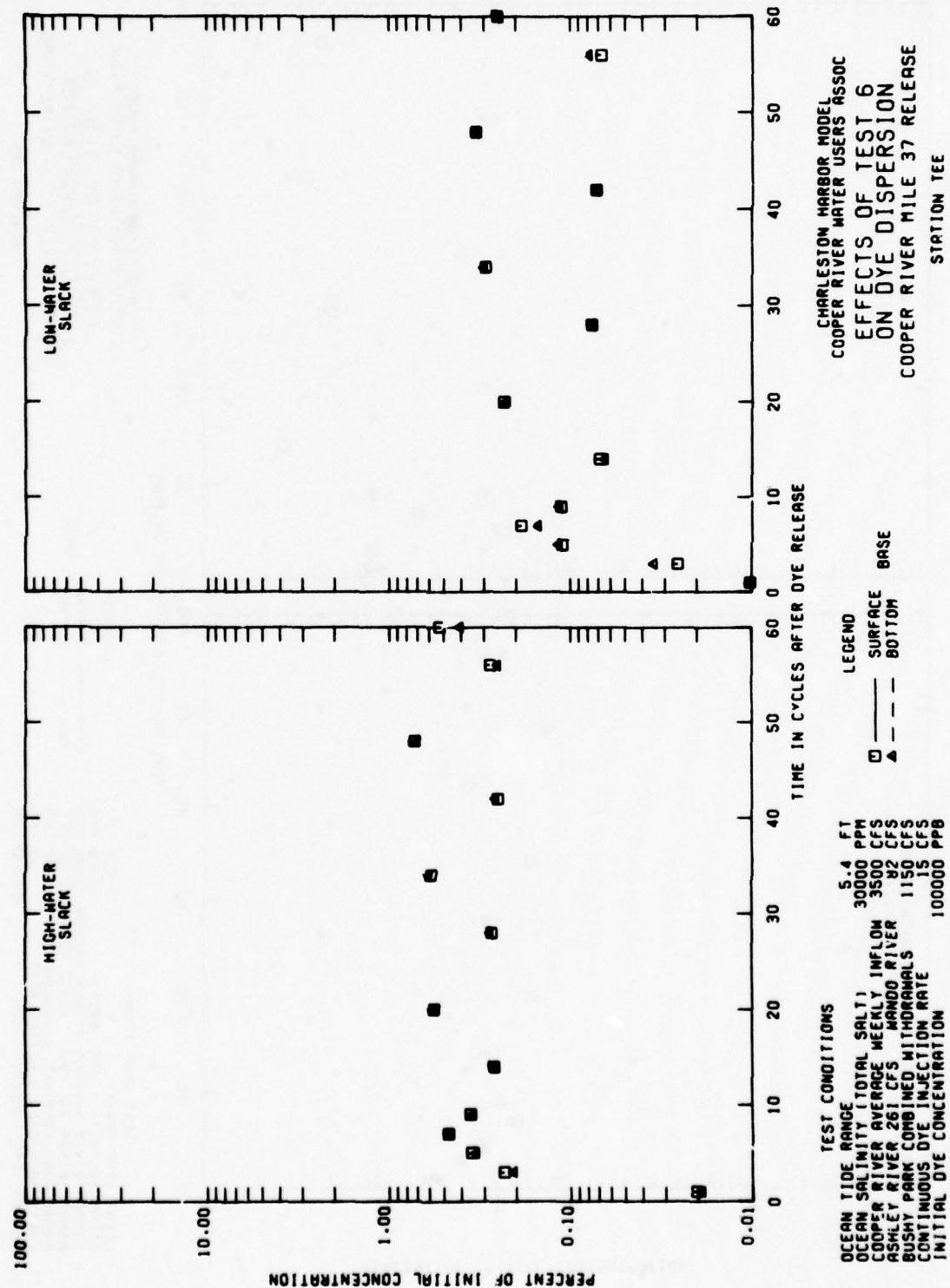
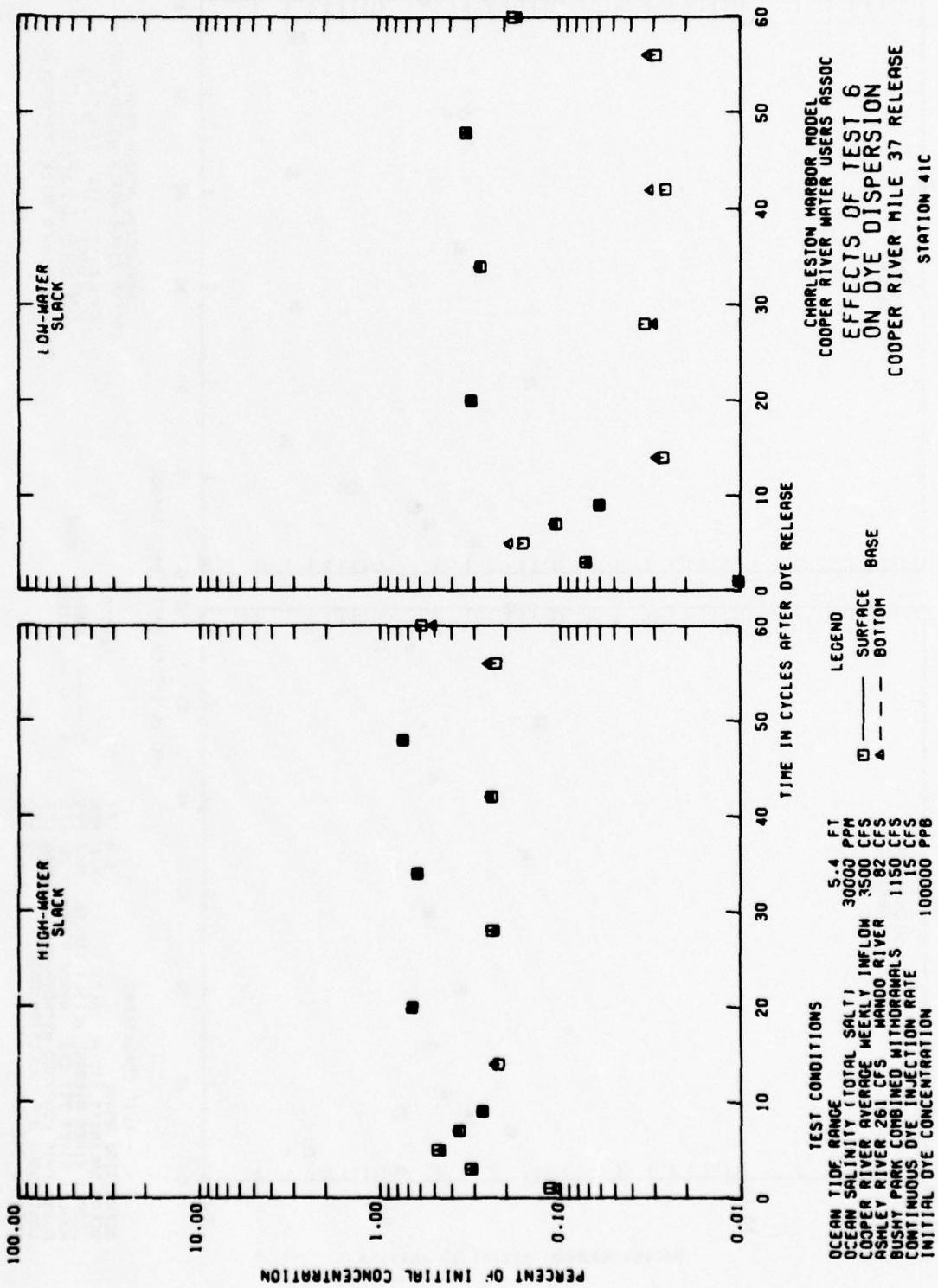
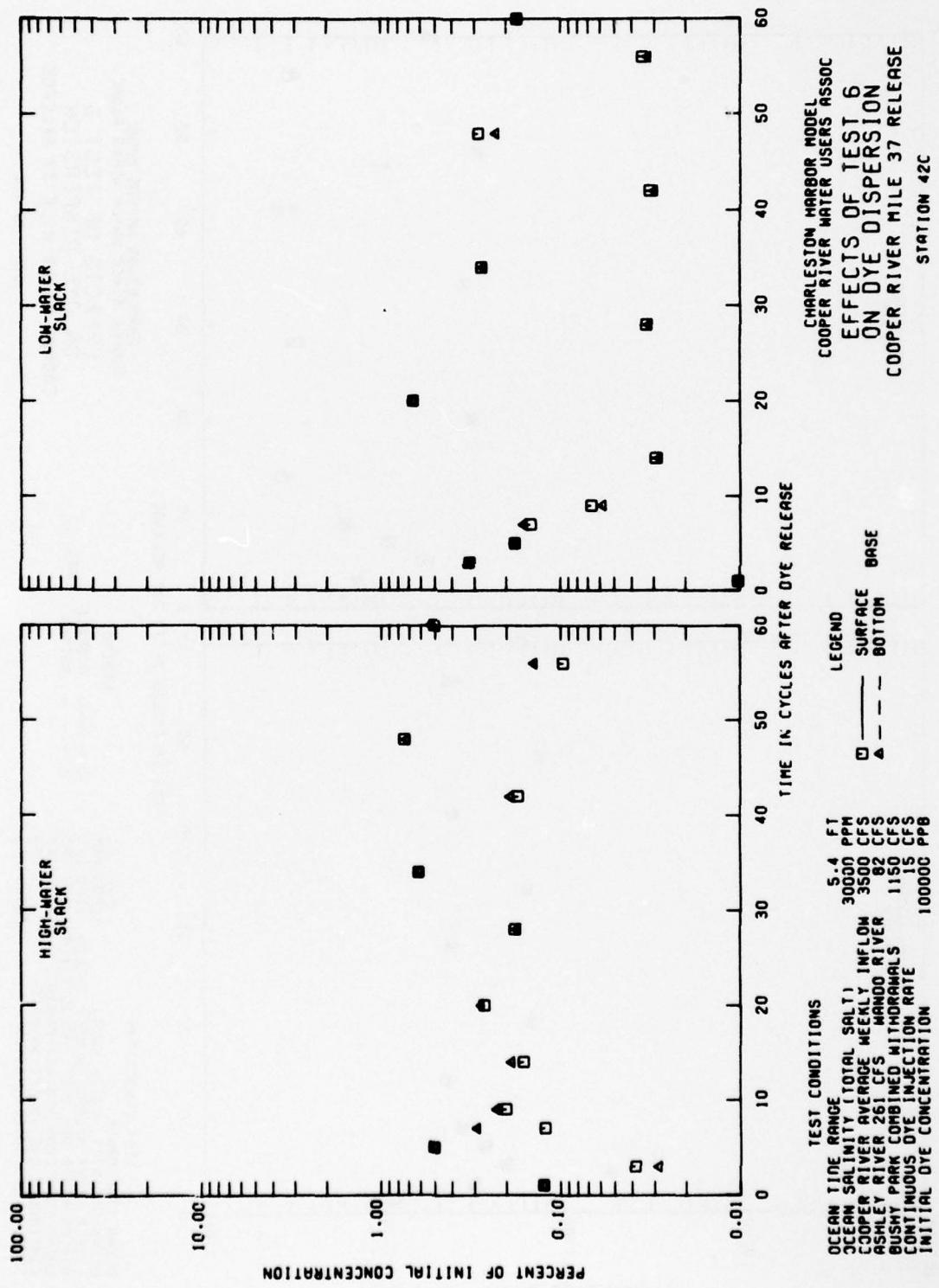
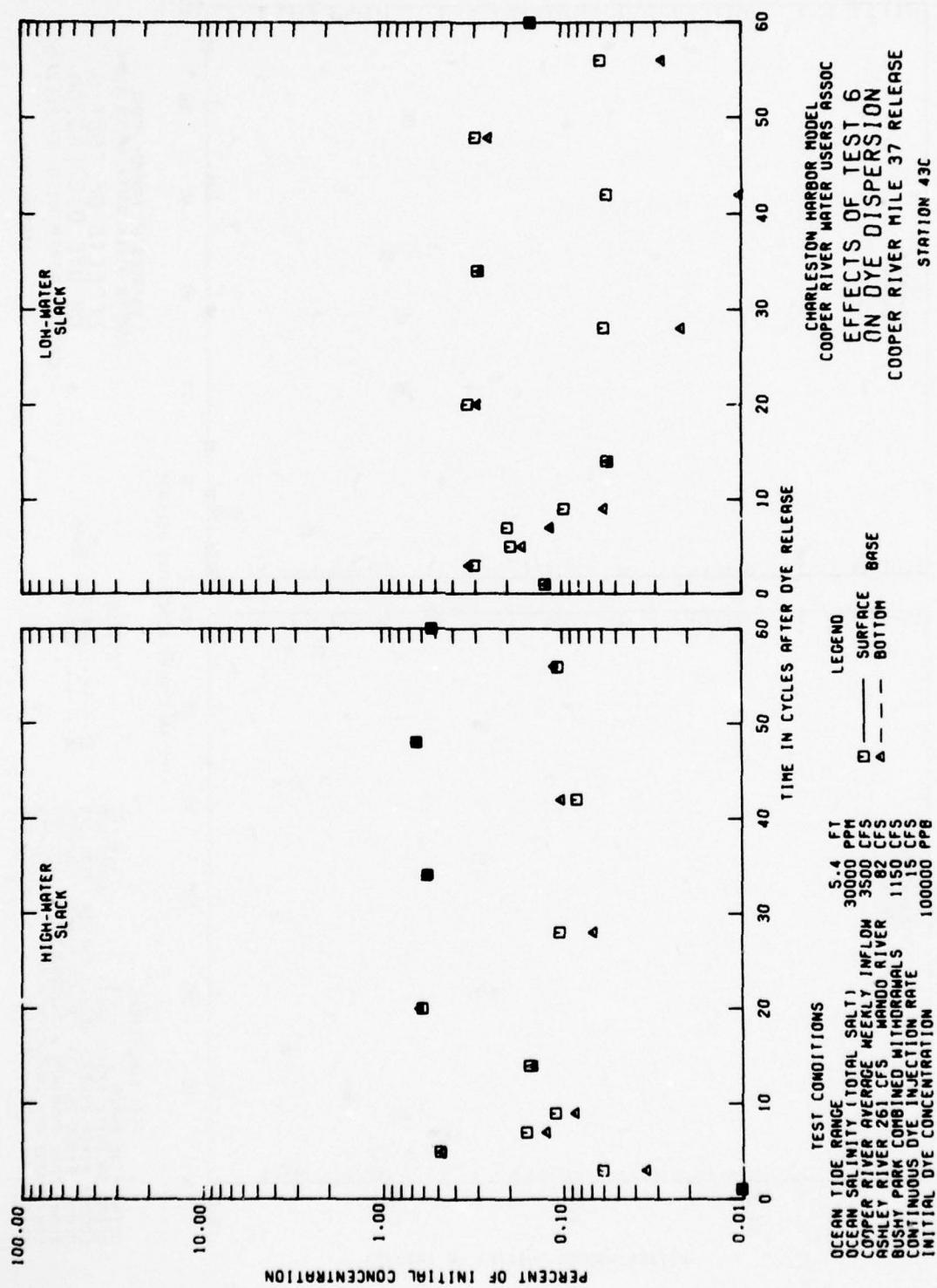
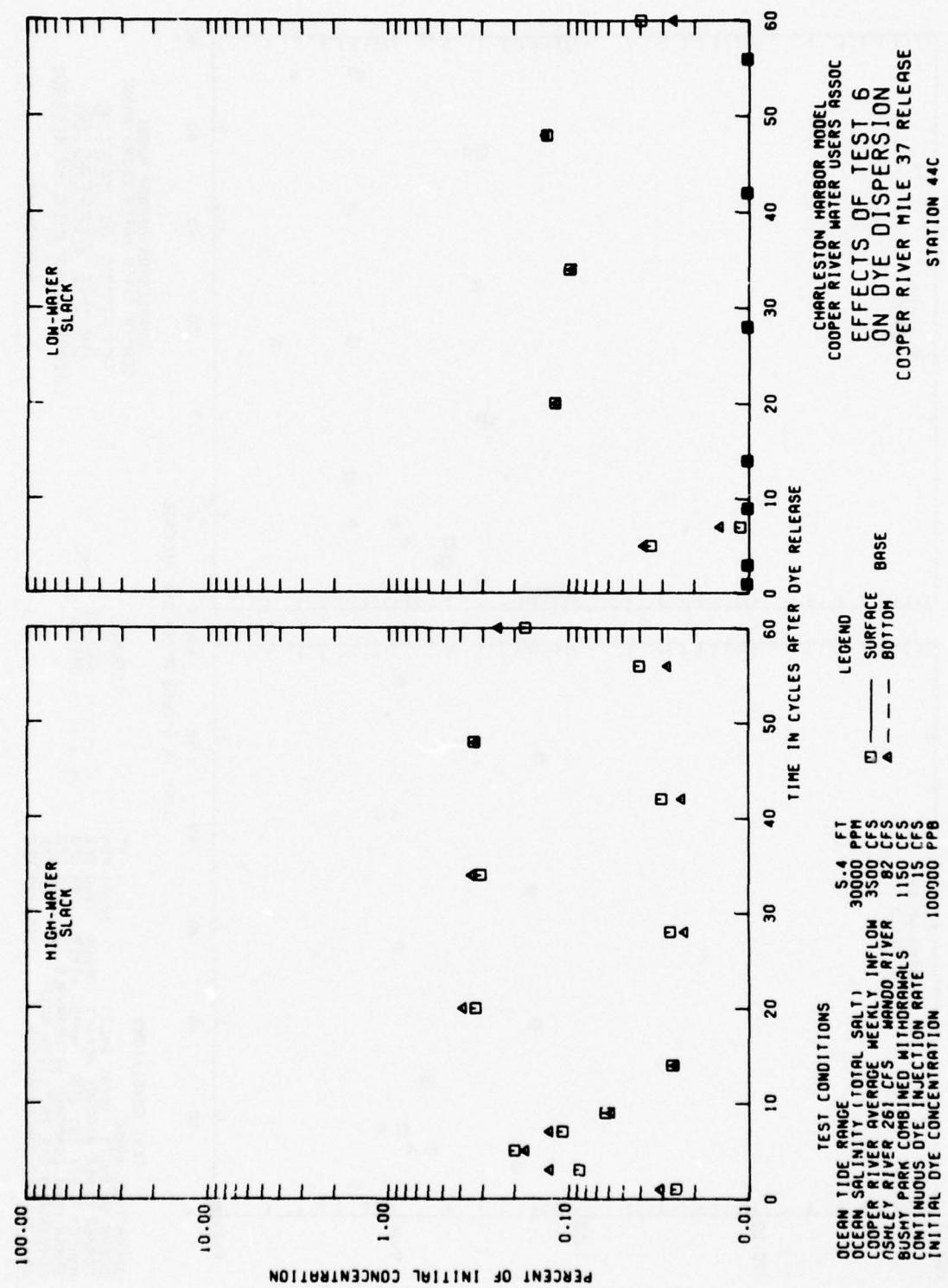


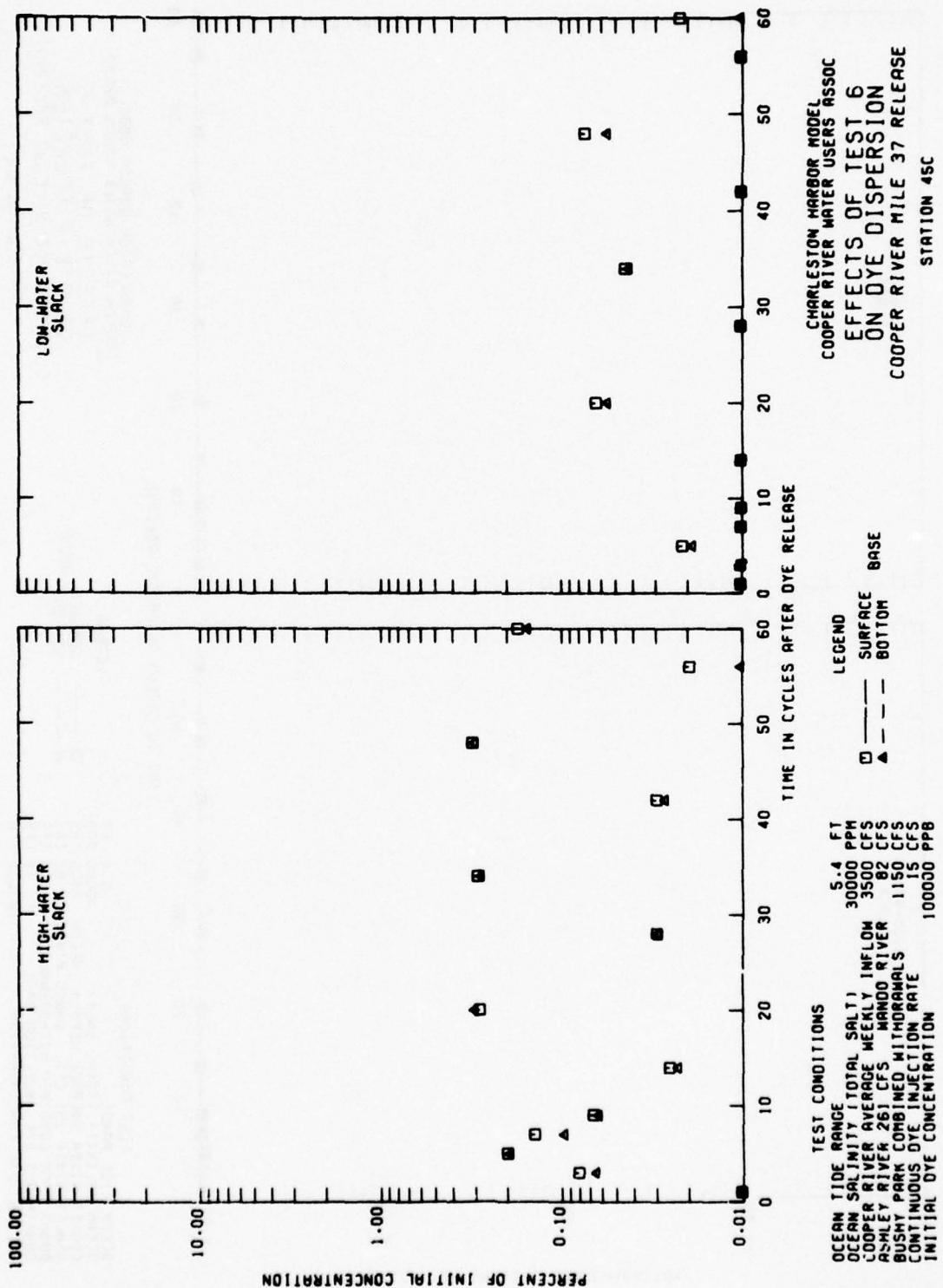
PLATE 104

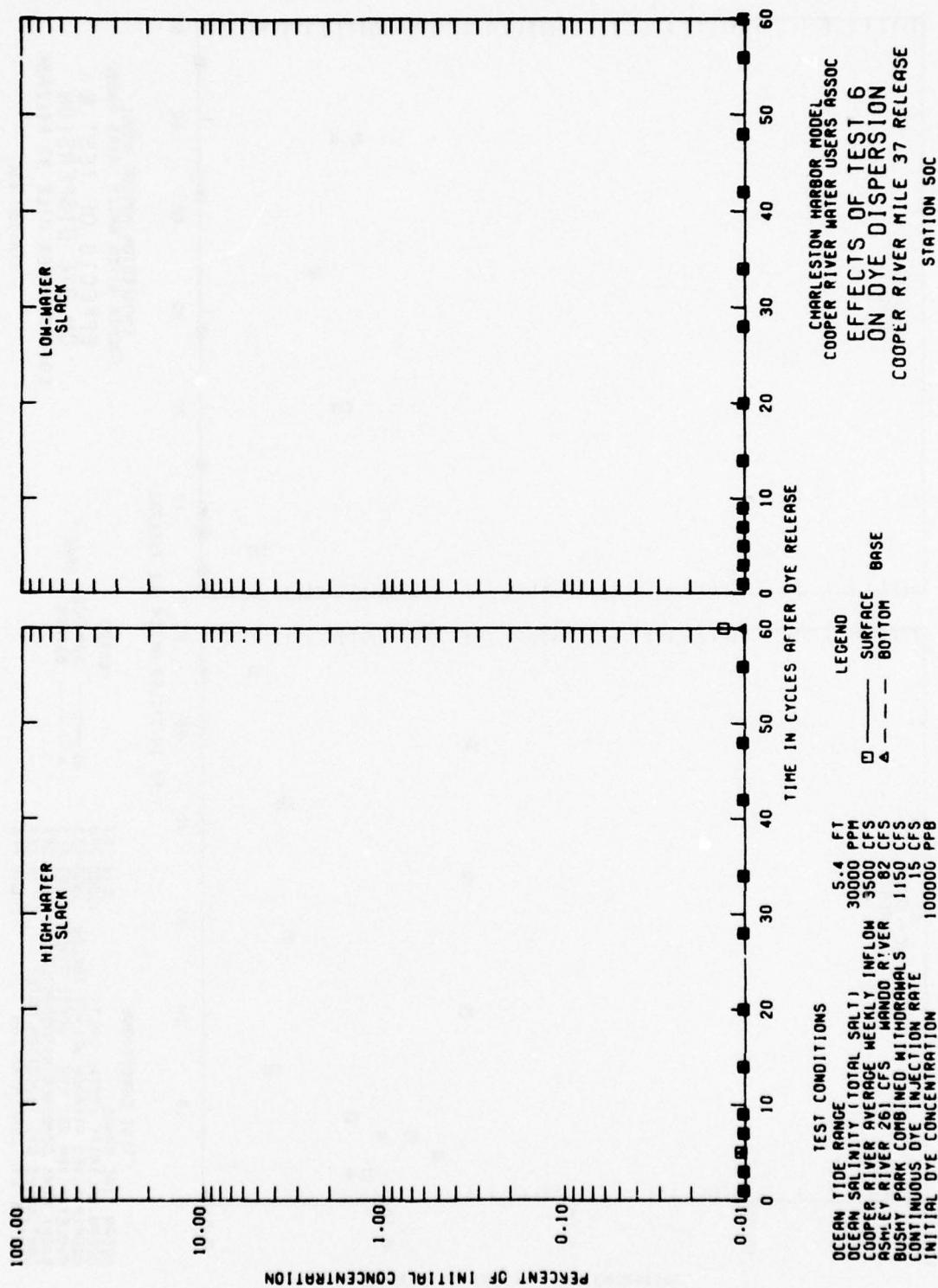


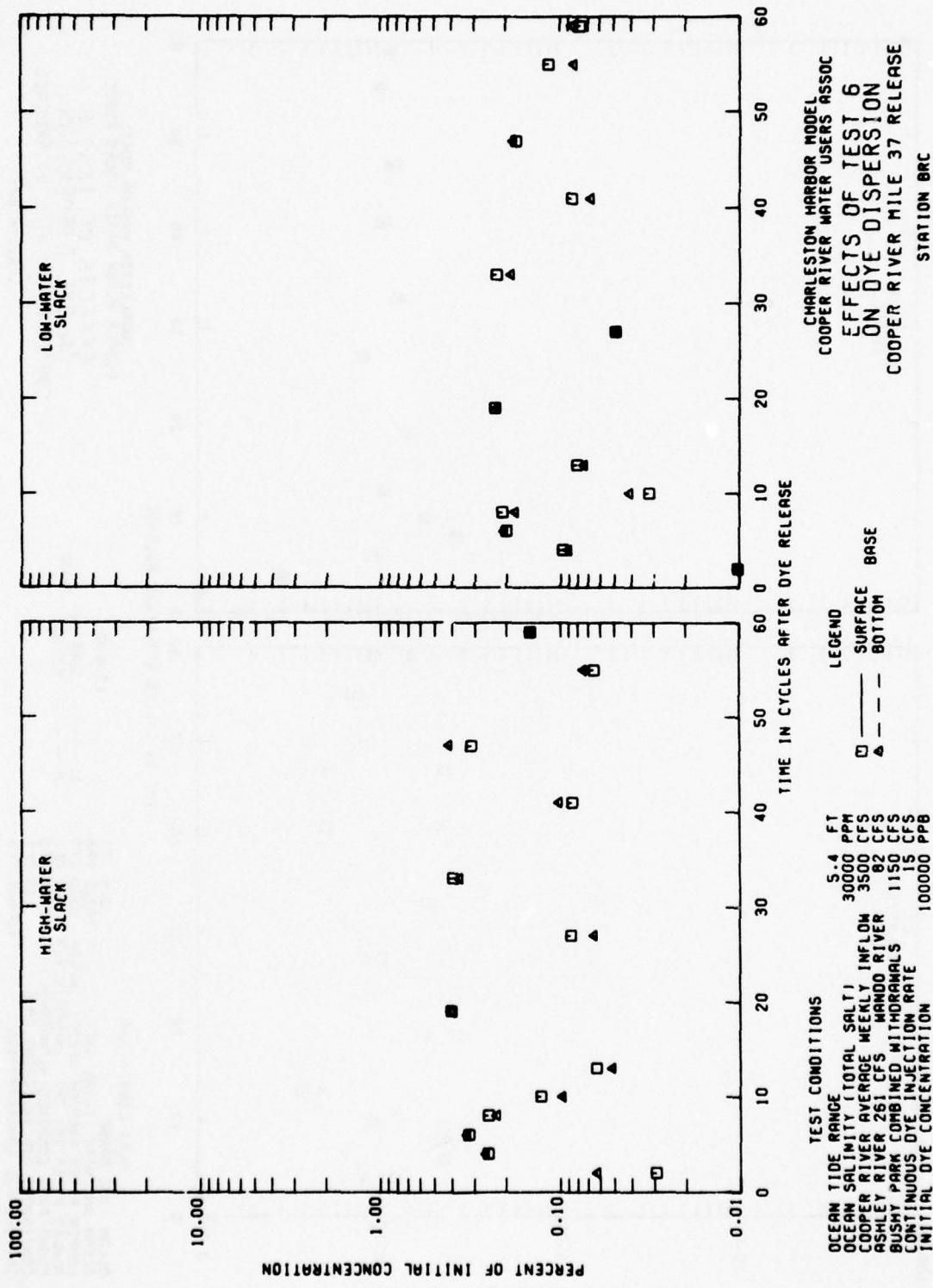


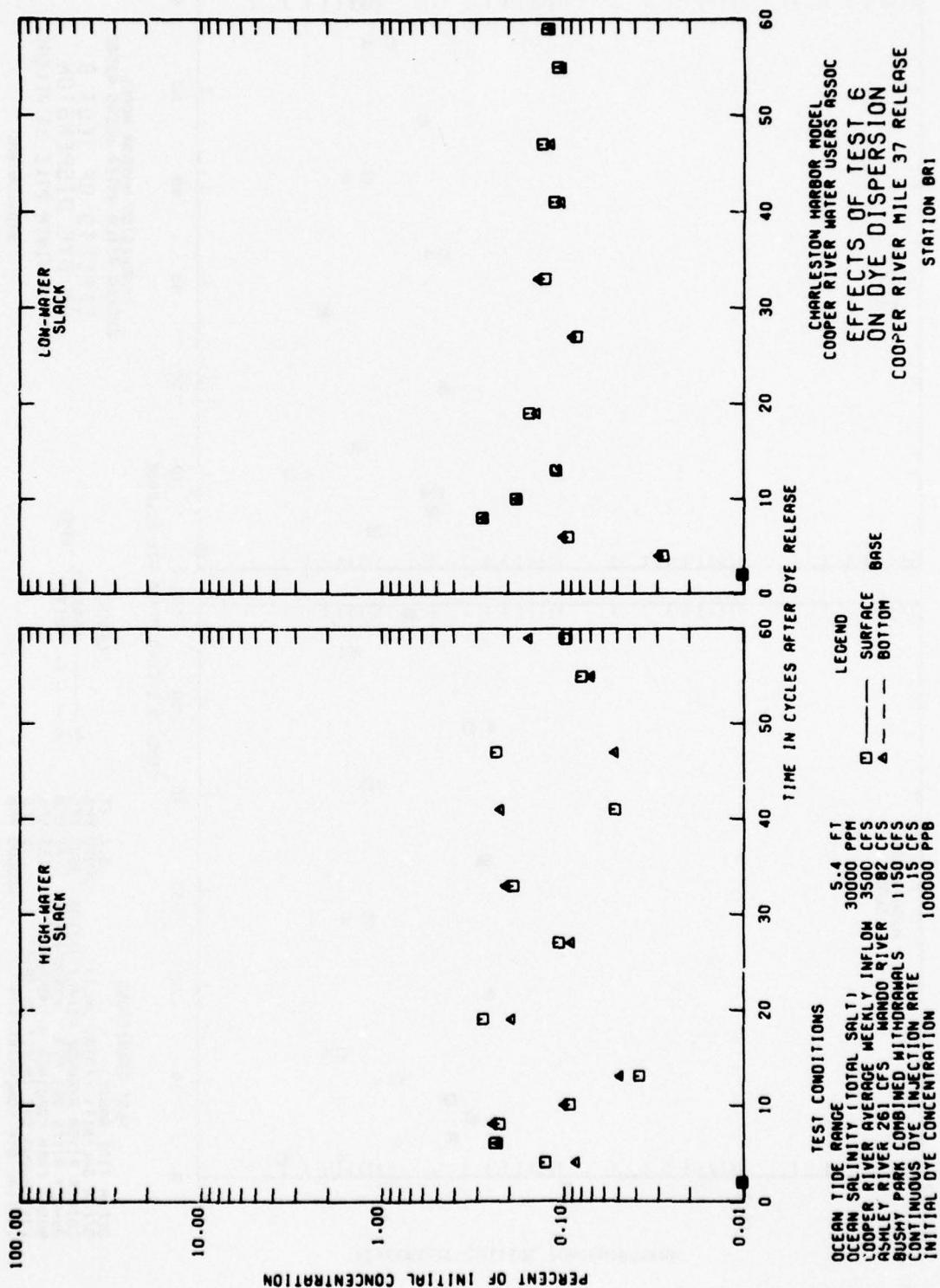


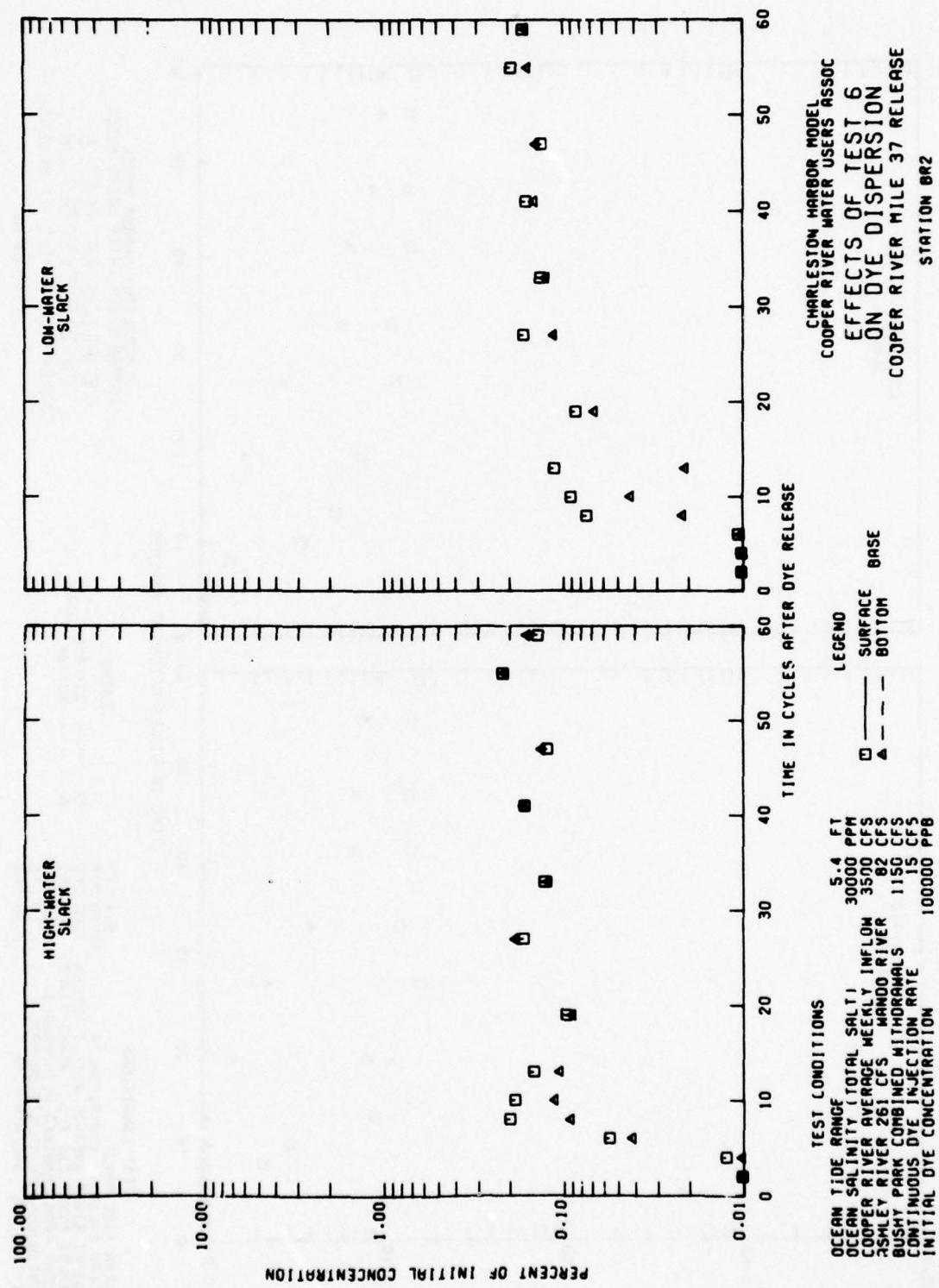












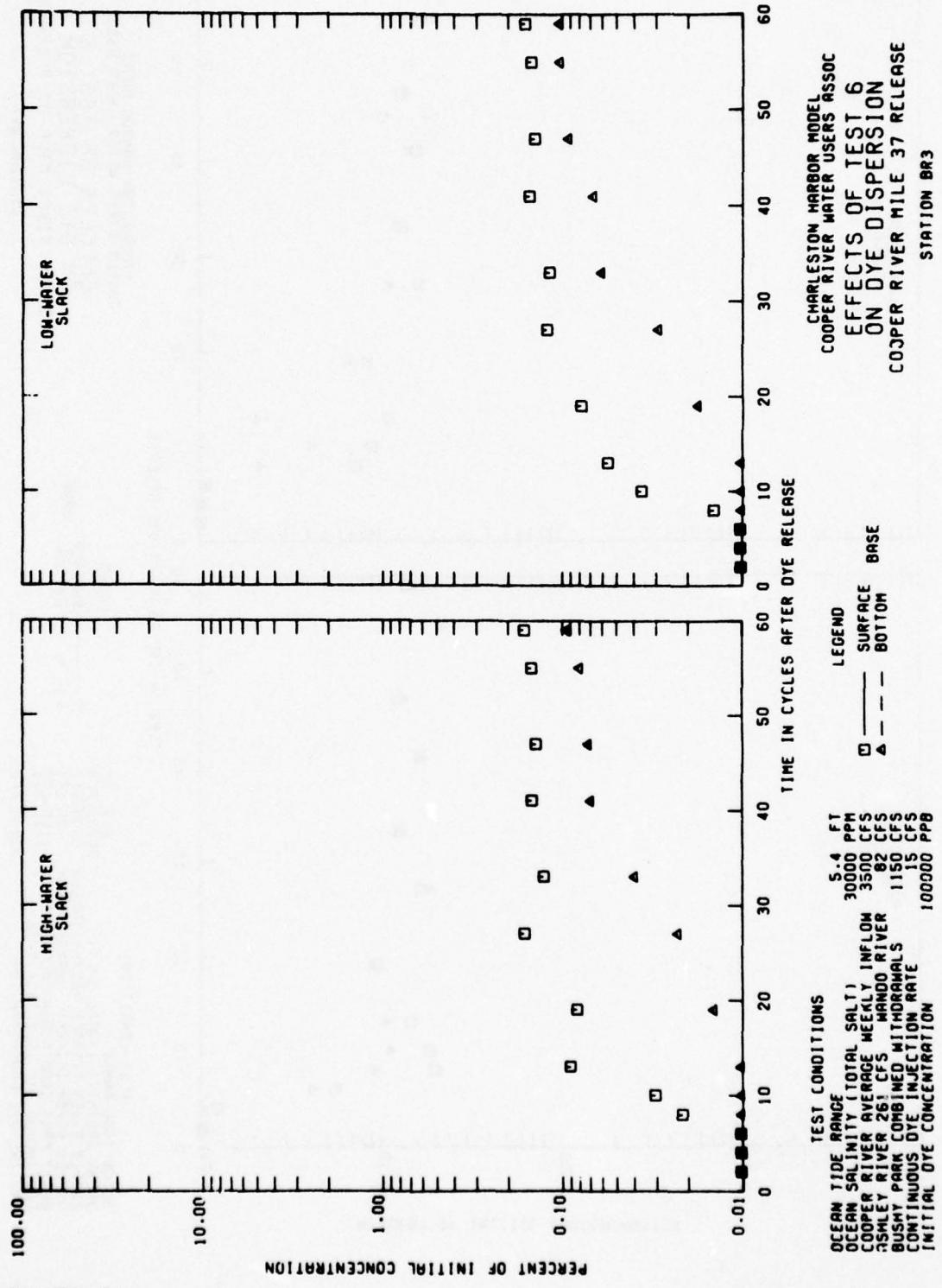
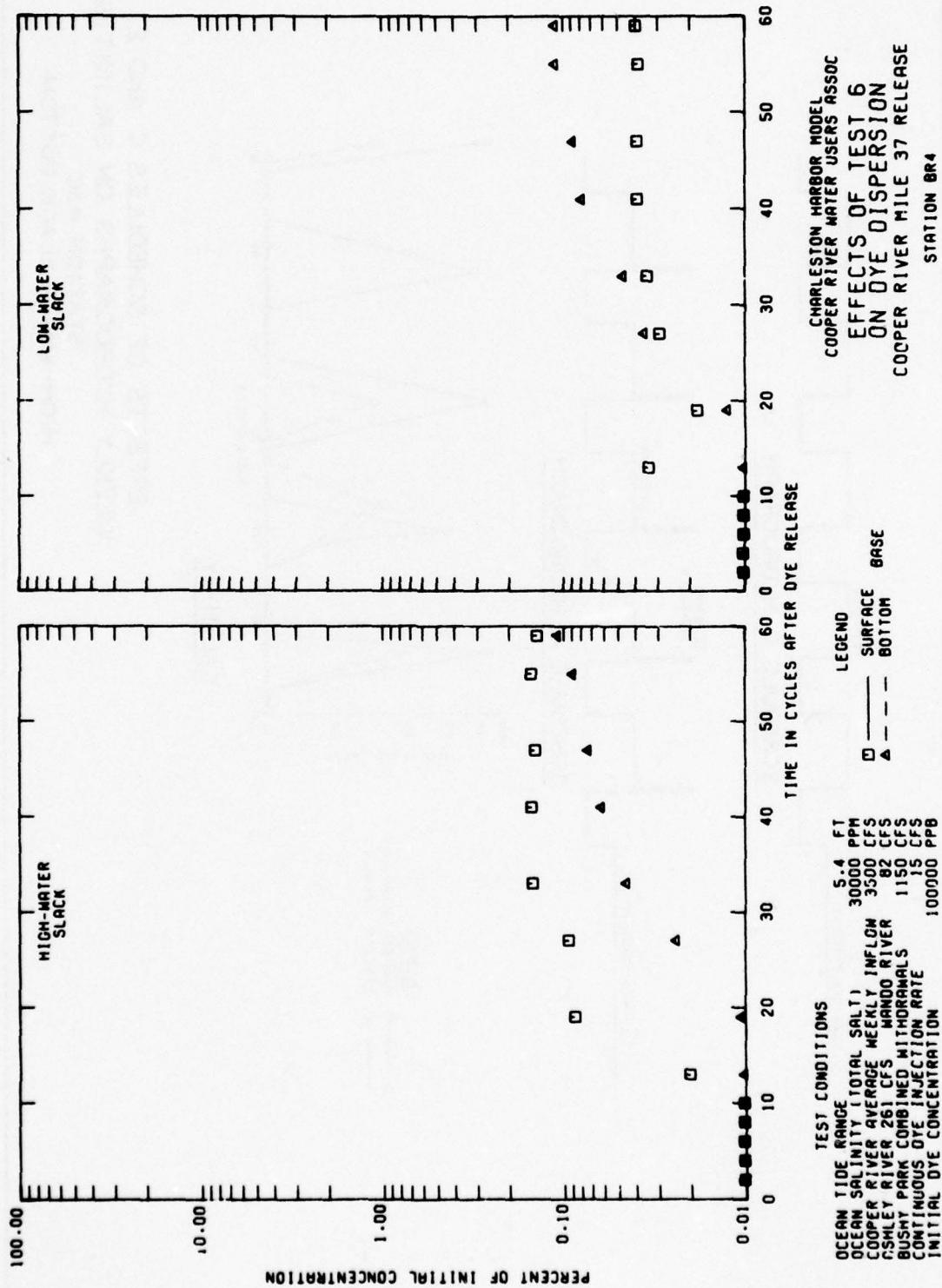
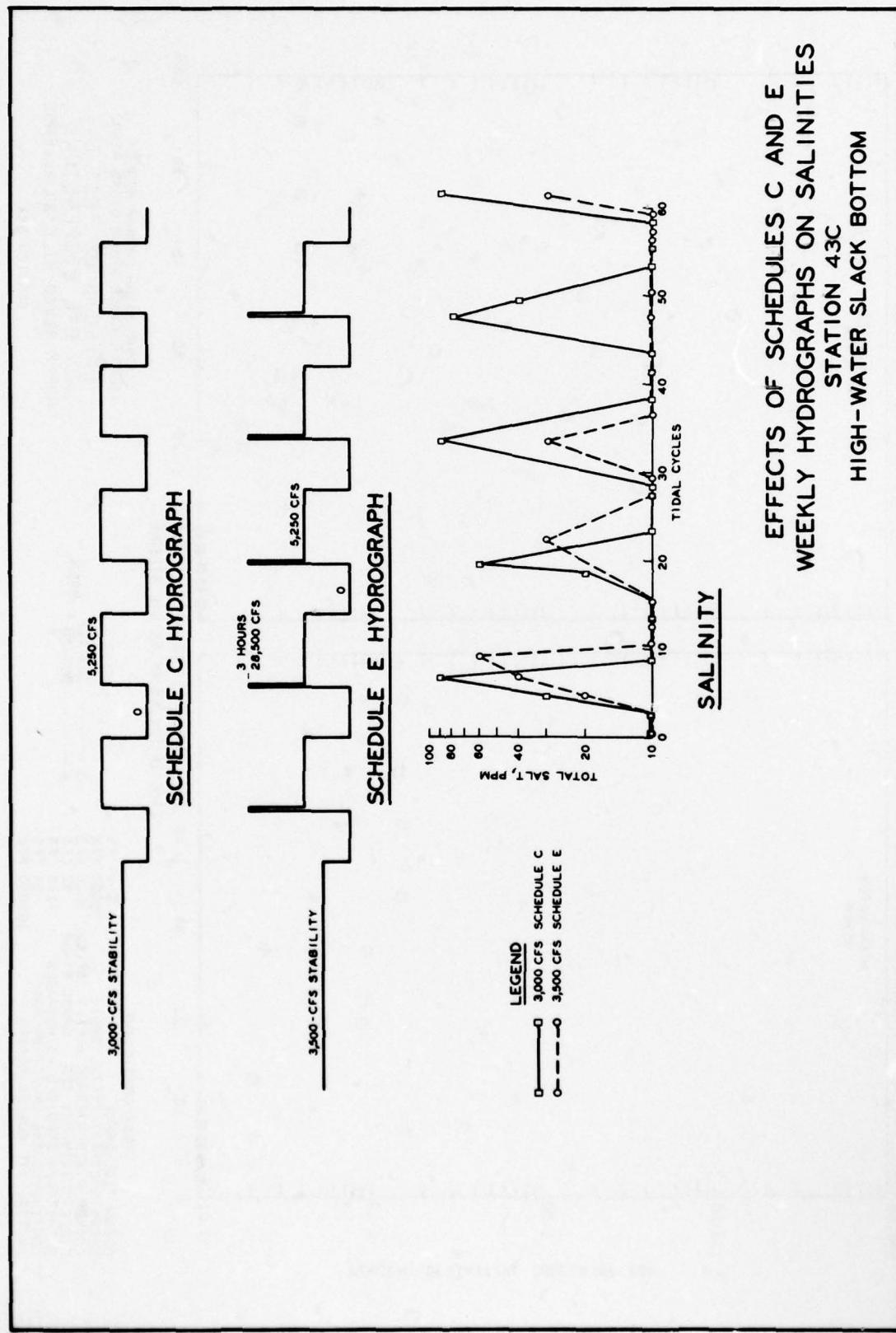
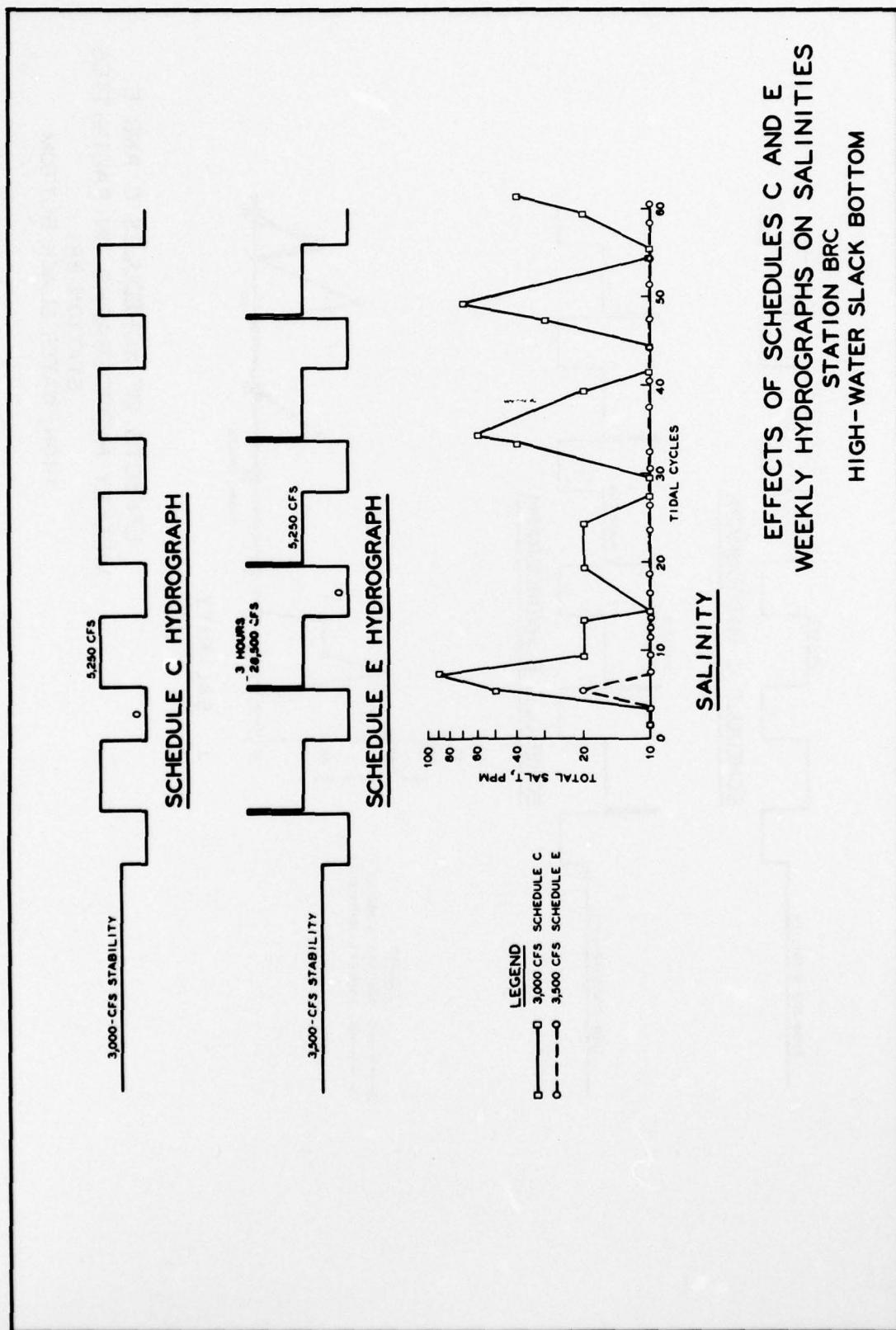
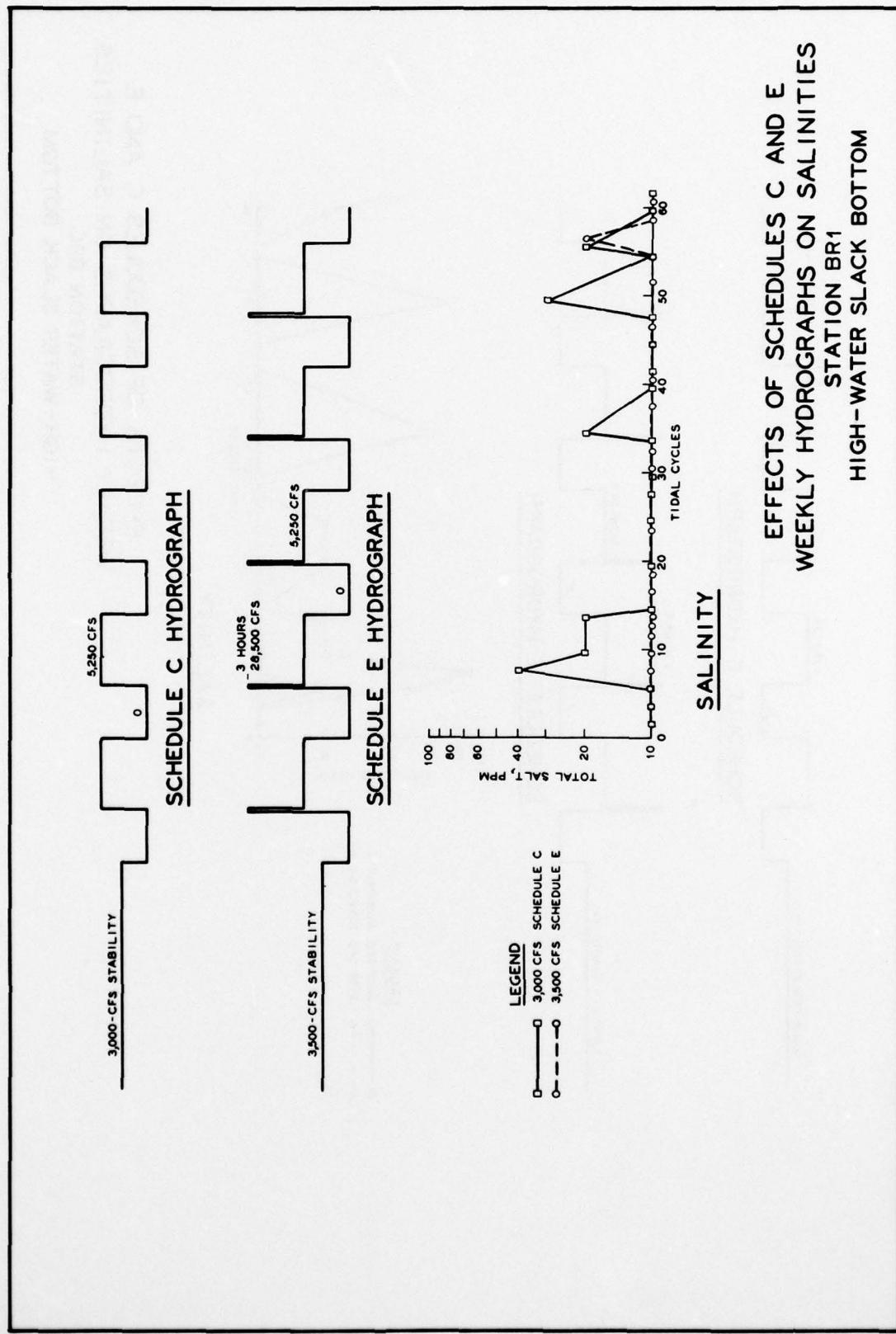


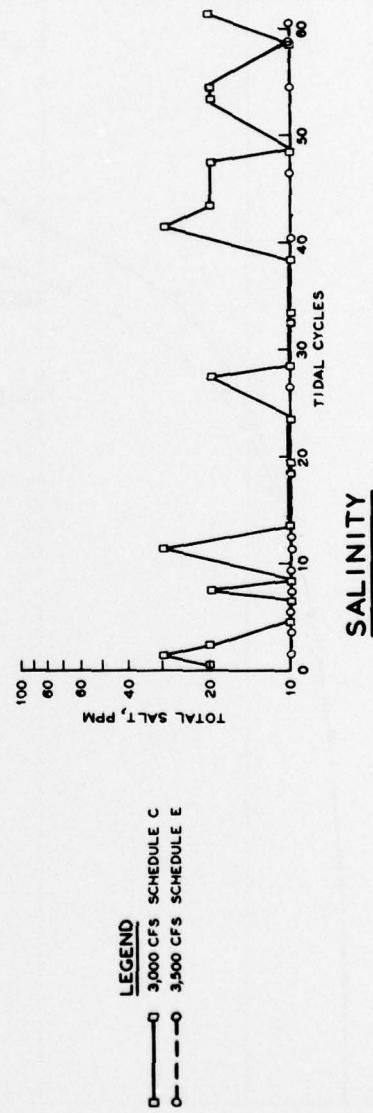
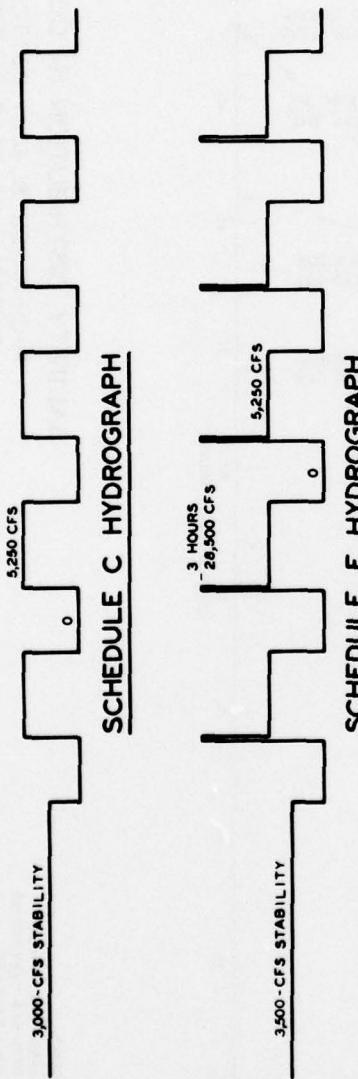
PLATE 114











EFFECTS OF SCHEDULES C AND E
WEEKLY HYDROGRAPHS ON SALINITIES
STATION BR²
HIGH-WATER SLACK BOTTOM

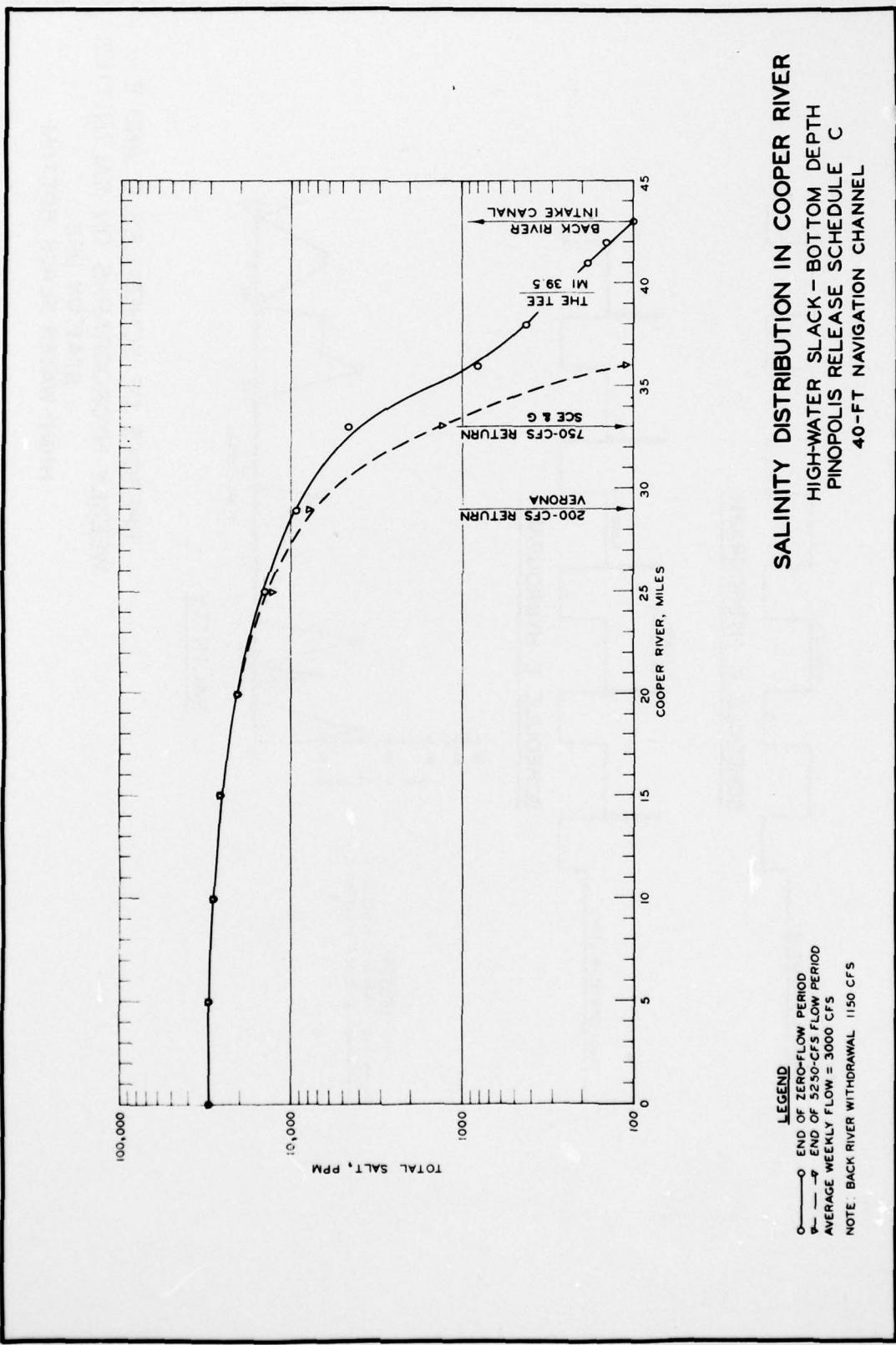
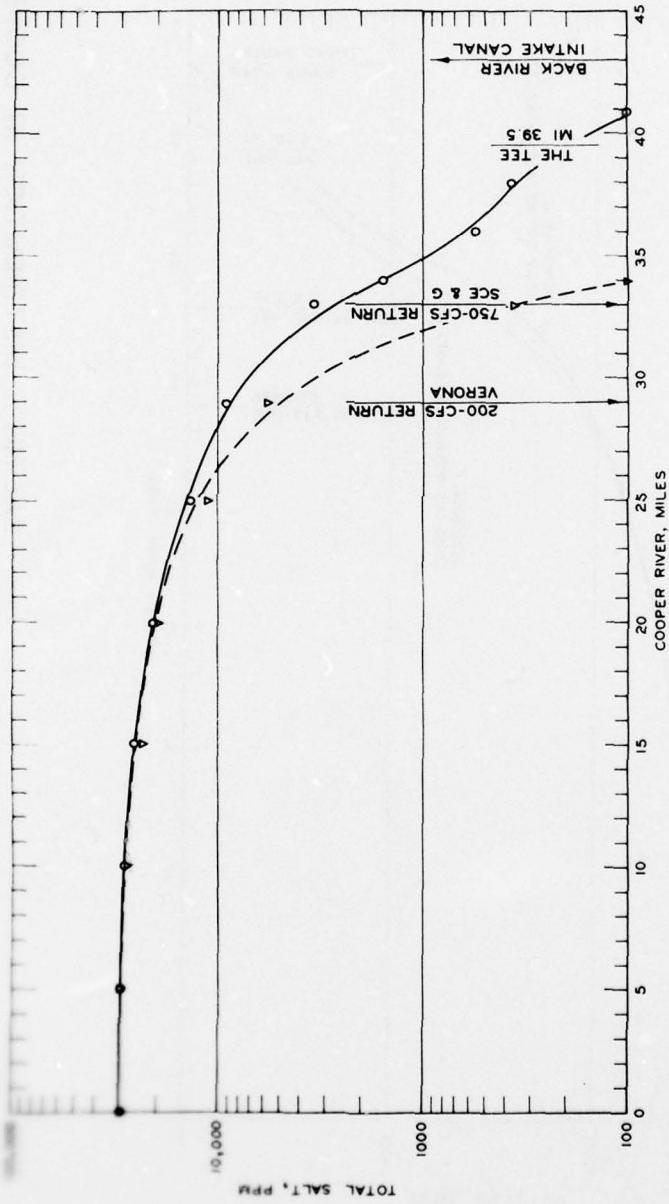


PLATE 120

SALINITY DISTRIBUTION IN COOPER RIVER
 HIGH-WATER SLACK - BOTTOM DEPTH
 PINOPOLIS RELEASE SCHEDULE E
 40-FT NAVIGATION CHANNEL



LEGEND
 ○ END OF ZERO-FLOW PERIOD
 ▲ END OF 52.50-CFS FLOW PERIOD
 AVERAGE WEEKLY FLOW = 3500 CFS
 NOTE: BACK RIVER WITHDRAWAL 150 CFS

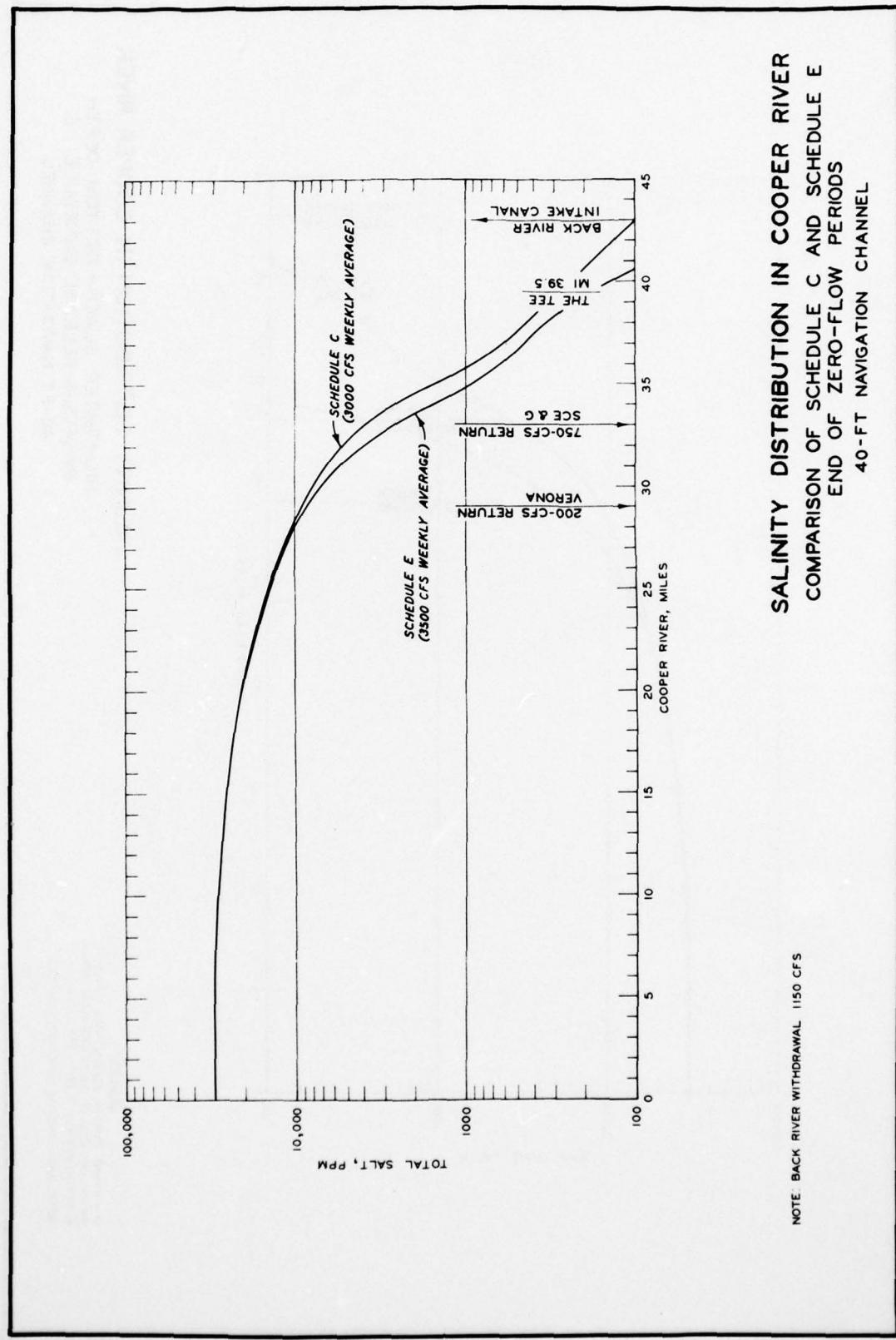


PLATE 122

SALINITY DISTRIBUTION IN COOPER RIVER
COMPARISON OF SCHEDULE C AND SCHEDULE E
END OF ZERO-FLOW PERIODS
4.0-FT NAVIGATION CHANNEL

In accordance with letter from DAEN-RDC, DAEN-ASI dated 22 July 1977, Subject: Facsimile Catalog Cards for Laboratory Technical Publications, a facsimile catalog card in Library of Congress MARC format is reproduced below.

Benson, Howard A

Dispersion of proposed effluent discharges and saltwater intrusion in Cooper River; hydraulic model investigation / by Howard A. Benson, Robert A. Boland, Jr. Vicksburg, Miss. : U. S. Waterways Experiment Station ; Springfield, Va. : available from National Technical Information Service, 1977.

27, [28] p., 122 leaves of plates : ill. ; 27 cm. (Miscellaneous paper - U. S. Army Engineer Waterways Experiment Station ; H-77-14)

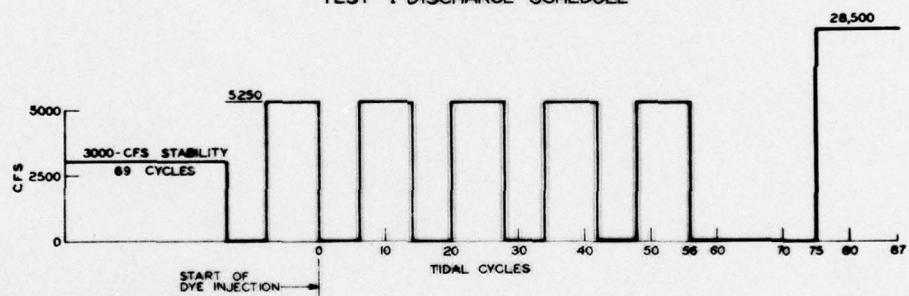
Prepared for State of South Carolina Water Resources Commission, Columbia, South Carolina.

1. Cooper River. 2. Dispersion. 3. Dye dispersion. 4. Effluents. 5. Hydraulic models. 6. Salinity. 7. Saltwater intrusion. I. Boland, Robert A., joint author. II. South Carolina. Water Resources Commission. III. Series: United States. Waterways Experiment Station, Vicksburg, Miss. Miscellaneous paper ; H-77-14.
TA7.W34m no.H-77-14

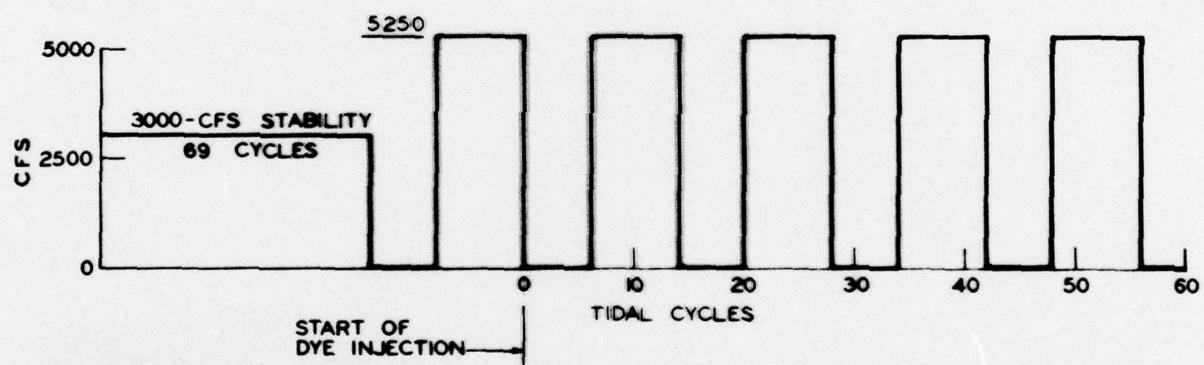
Contains:

- Test 1 Discharge Schedule - See: page 15
- Test 2 Discharge Schedule - See: page 17
- Test 3 Discharge Schedule - See: page 18
- Test 4 Discharge Schedule - See: page 19
- Test 5 Discharge Schedule - See: page 20

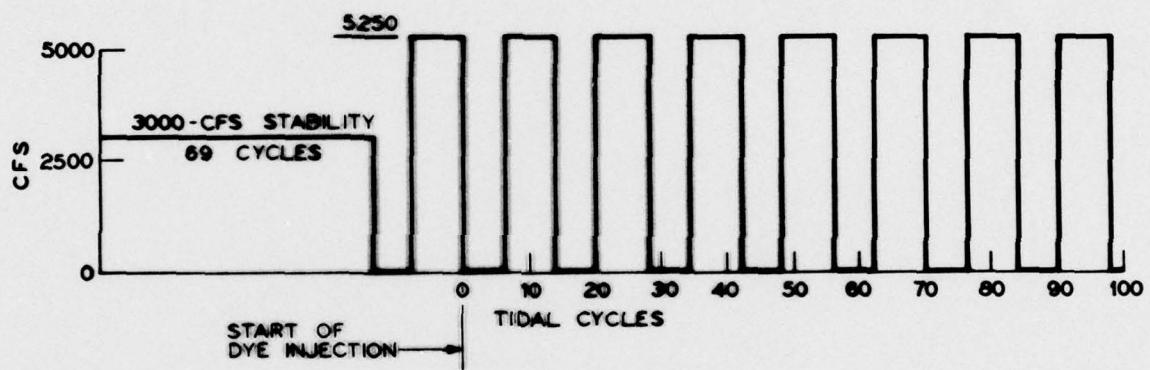
TEST 1 DISCHARGE SCHEDULE



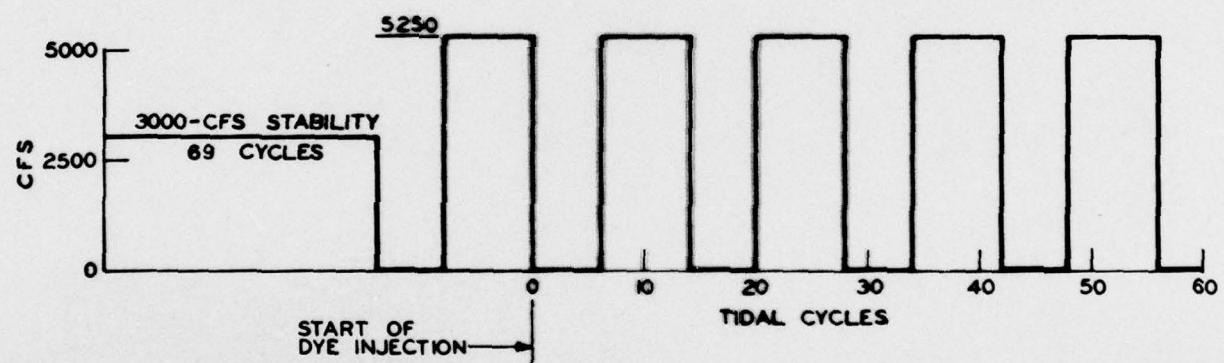
TEST 2 DISCHARGE SCHEDULE



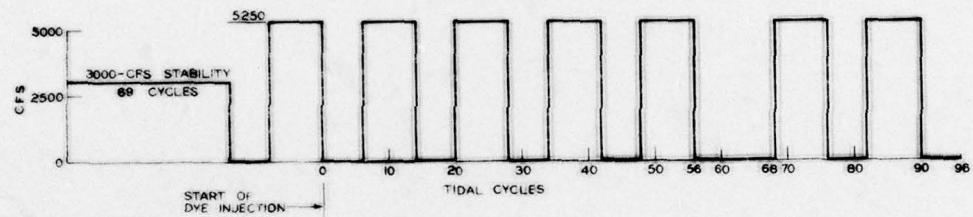
TEST 3 DISCHARGE SCHEDULE



TEST 4 DISCHARGE SCHEDULE



TEST 5 DISCHARGE SCHEDULE



TEST 6 DISCHARGE SCHEDULE

